WL-TR-94-4052 Volume 1, Chapters 1, 2, 3 and 4

DAMAGE TOLERANT DESIGN HANDBOOK



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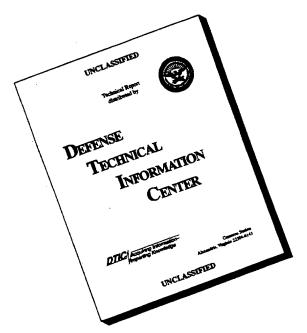
May 1994 Final Report for Period June 1991 - May 1994

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1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE MAY 1994	3. REPORT TYPE AN	D DATES SOVERED 05/19/94
4. TITLE AND SUBTITLE DAMAGE VOL 1, CHAPTERS 1 6. AUTHOR(5)D.A. SKINN, J. A.P. BERENS, P J. SMITH	P. GALLAGHER,	HANDBOOK	5. FUNDING NUMBERS C F33615-91-C-5610 PE 62102 PR 2418 TA 04 WU 91
7. PERFORMING ORGANIZATION NAME(UNIVERSITY OF DAY 300 COLLEGE PARK DAYTON OH 45469-0	TON RESEARCH INS	TITUTE	8. PERFORMING ORGANIZATION REPORT NUMBER
9. SPONSORING/MONITORING AGENCY MATERIALS DIRECTO WRIGHT LABORATORY AIR FORCE MATERIE WRIGHT PATTERSON	RATE L COMMAND	4	10. SPONSORING/MONITORING AGENCY REPORT NUMBER WL-TR-94-4052
11. SUPPLEMENTARY NOTES			
12a. DISTRIBUTION / AVAILABILITY STAT	EMENT		12b. DISTRIBUTION CODE
APPROVED FOR PUBL UNLIMITED.	IC RELEASE; DIST	RIBUTION IS	
13. ABSTRACT (Maximum 200 words)			

This report presents a compilation of mechanical property data that are useful for damage tolerant design and analyses. The data of this handbook combines the old data that were previously presented in MCIC-HB-OIR (Damage Tolerant Design Handbook, December 1983) and more recent data that were collected from various sources. The fracture toughness, crack growth, R-curve, sustained load and threshold data are for alloy and stainless steels, nickel based super alloys, titanium alloys and aluminum alloys.

14. SUBJECT TERMS FRACTURE TOUGH SUBCRITICAL CE	INESS	R-CUI SUSTA THRES	LINE	D LOAD	15. NUMBER OF PAGES 747 16. PRICE CODE
17. SECURITY CLASSIFICATION OF REPORT UNCLASSIFIED	18. SECURITY CLASSIF OF THIS PAGE UNCLASSI			SECURITY CLASSIFICATION OF ABSTRACT UNCLASSIFIED	20. LIMITATION OF ABSTRACT

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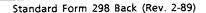


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Foreword

This report summarizes the results of a damage tolerant, material property data collection and reporting program conducted under USAF Contract F33615-91-C-5610. The work was sponsored by the Materials Directorate of Wright Laboratory with Mr. Jack Coate of the Systems Support Division serving as the project monitor. The technical effort was conducted between June 1991 and January 1994. The work was performed by the University of Dayton Research Institute under the general supervision of Dr. Joseph P. Gallagher with Dr. Alan P. Berens serving as Principal Investigator.

This final report comprises eight chapters which are presented in five volumes as follows:

VOLUME	CHAPTER	DESCRIPTION
1	1	Handbook organization and content
	2	Methods of calculation
	3	Alloy Steels
	4	Stainless Steels
2	5	Nickel Based Super Alloys
	6	Titanium Alloys
3	7	Aluminum 2000/6000 Series Alloys
4 & 5	8	Aluminum 7000/8000 Series Alloys

A detailed listing of the materials represented in the Handbook is contained in the preceding Table of Contents. In the body of the Handbook, the pages are numbered within chapters and the relevant portion of the table of contents is repeated at the beginning of each chapter.

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CHAPTER 1 HANDBOOK ORGANIZATION AND CONTENT

1.0 OVERVIEW

The format of the Damage Tolerant Design Data Handbook has been modified slightly since the previous update in 1983. Data are still presented in material chapters and sorted by alloy within the chapters. Available alloy property data are then presented in a consistent order from chapter to chapter. This organization was suggested by aerospace engineers as the format best suited for their use. Additionally, this format conforms to other aerospace structural metals handbooks such as the Military Handbook-5 and Aerospace Structural Metals Handbook.

A survey was conducted at the beginning of this handbook program. A number of aerospace design, materials, and structural engineers were canvassed for their comments relative to the handbook organization, formats, summaries and data types. It was agreed that the overall format of the 1983 edition of the handbook was generally acceptable. The page numbering scheme in the 1993 edition transitioned to sequential page numbers within chapters to facilitate looking up alloy data. The table of contents on the first page of each material chapter lists the alloys in the chapter along with their starting pages.

Mean trend fatigue crack growth and sustained crack growth data are now listed on the same page as the plots of their crack growth rate data. If available, the root mean square percent error and life prediction ratio for these data are also listed on the same page. This new format removes confusion about the relationship of crack growth data to their fitted mean trend data.

Data are presented in English units throughout the handbook, i.e., Ksivin for fracture toughness and applied stress intensity factor levels, and inches/hr or inches/cycle for crack growth rates. Metric units have been incorporated along with

the English units on the graphical presentation of the sustained load and fatigue crack growth rate data, but limited space forced the exclusion of metric units from the tabular data.

1.1 ORGANIZATION

The handbook is divided into eight chapters and consists of five volumes. The order of the chapters are as designated in Table 1.1. Following the first chapter on handbook usage and the second chapter on methods of calculations are the six material chapters. This order was selected to keep the data for a particular chapter together as much as possible while keeping the volume sizes reasonable and approximately equal.

TABLE 1.1
ORDER OF HANDBOOK CHAPTERS

Volume Number	Chapter Number	Chapter Title
1	1	Handbook Organization, Contents, and Formats
1	2	Methods of Calculation
1	3 .	Alloy Steels
1	4	Stainless Steels
2	5	Nickel Base Alloys
2	6	Titanium Alloys
3	7	2000/6000 Series Aluminum Alloys
4-5	8	7000/8000 Series Aluminum Alloys

Each material chapter contains a section of material summaries and three subsequent sections containing data pertinent to individual material alloys. Table 1.2 presents the basic organization of each material chapter and reflects the naming conventions for tables and figures found therein. The first number of any section,

TABLE 1.2 ORGANIZATION OF HANDBOOK DATA CHAPTERS

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C.0.3.1	Table	Plane Stress and Transitional Fracture Toughness K _c (Buckling Not Constrained)
C.0.3.2	Table	Plane Stress and Transitional Fracture Toughness K_c (Buckling Constrained)
C.0.4(.s)	Table	Fatigue Crack Growth Rate Comparison
C.0.5	Table	Stress Corrosion Cracking Threshold K_{Iscc}
		CIFIC ALLOY DATA
		Alloy Summaries
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CA.1.2(.s)	Table	Fatigue Crack Growth Rate Comparisons
	Alloy F	racture Toughness Data
C.A.2.1	Table	Plane Strain Fracture Toughness K_{Ic}
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CA.3.2(.s)	Figure	da/dt-vs-K _{max} Plots and Mean Trend Sustained Load Crack Growth Rate Data
C.A.3.3	Table	Stress Corrosion Cracking Threshold K_{Iscc}

C - material chapter number A - alloy sequence number (.s) - sequence number when multiple tables or figures exist for specific test conditions

subsection, table or figure number refers to the material chapter as specified in Table 1.1. A zero in the second position indicates that the data is a material summary. Consecutive sequence numbers originating at one are assigned to alloys as the second number in the numbering scheme. The alloy sequence numbers are defined on the index page of each material chapter. The material bibliography is assigned the sequence number immediately following the last alloy in the material chapter.

In the material summary section, C.0..., where C represents a material chapter number, five types of material summary tables may be listed as subsections. Tables will be listed in the order defined by Table 1.2. If, however, not enough data are available for a particular summary, this summary is not printed and its sequence number is skipped. Section 1.3 describes the formats for material summaries.

In the alloy section, CA..., where C represents material chapter number and A represents alloy number, the third number in the sequence will designate whether the data are an alloy summary $(C.A.\underline{1})$, fracture toughness data $(C.A.\underline{2})$, or crack growth resistance data $(C.A.\underline{3})$. Within each subsection, data tables and graphs are ordered consecutively. If, however, insufficient data are available to generate a table or figure, the table or figure in question does not appear and the sequence number is skipped.

Section 1.4 discusses the formats of two alloy summaries: plane strain fracture toughness and fatigue crack growth rate. Section 1.5 discusses the data formats of three types of fracture toughness data: plane-strain fracture toughness, plane stress and transitional fracture toughness, and resistance curve. Section 1.6 discusses the data formats of three types of subcritical crack growth data: fatigue crack growth rate, sustained load crack growth rate, and stress corrosion cracking threshold.

To help the handbook user locate data, examples of actual tables and figures are included in the discussions of the handbook subsections which follow. These examples are presented to familiarize the user with the formats presented in the handbook. The discussion follows the same order as that found in the handbook.

1.2 DATA ORDERING AND ABBREVIATIONS

1.2.1 Sorting Order

Data fields in the handbook database exist in one of three formats: text, numeric, or coded. The ASCII (American Standard Code for Information Interchange) collating sequence (Table 1.3) defines the sort order for text fields such as alloy, condition/heat treat, and environment. Letters are case insensitive in text fields, i.e., lower case letters are treated as their upper case equivalents. Numeric fields are presented in ascending order (most negative to most positive). Test temperature is a numeric field that has a minor exception in that temperatures from 65°F to 80°F are grouped as room temperature and are considered equal. Coded fields are ordered on their code value according to the ASCII collating sequence. Table 1.4 presents three such coded fields: product form, specimen design, and specimen orientation. Existing codes and their equivalent values are given in coded order. Note that the equivalent values are used in the presentation of material data.

1.2.2 Abbreviations

The material chapters present tables and figures summarizing material property data. Abbreviations are used throughout the tables and figures in these chapters for the following five data fields: 1) condition/heat treatment, 2) product form, 3) environment, 4) specimen design, and 5) specimen orientation. Abbreviations and expanded descriptions used in the presentation of these data types can be found in Tables 1.5 through 1.8 and Figure 1.1, respectively.

1.3 MATERIAL CHAPTER SUMMARIES

Material summaries are presented at the beginning of each chapter before alloy summaries and detailed data. These summaries are meant to aid in comparing material properties and selecting materials for design. There are five data types (see

TABLE 1.3

AMERICAN STANDARD CODE FOR INFORMATION INTERCHANGE (ASCII) CONVERSION TABLE

Decimal Value	ASCII Character	Decimal Value	ASCII Character	Decimal Value	ASCII Character
32	(space)	64	@	96	4
33	!	65	A	97	a
34	11	66	В	98	b
35	#	67	C	99	с
36	\$	68	D	100	d
37	%	69	E	101	e
38	&	70	F	102	f
39	,	71	G	103	g
40	(72	H	104	h
41)	73	I	105	i
$\frac{41}{42}$	*	74	J	106	j
43	+	75	K	107	k
44	·	76	L	108	1
45	-	77	M	109	m
46		78	N	110	n
47	/	79	0	111	0
48	0	80	P	112	р
49	1	81	Q	113	q
50	2	82	R	114	r
51	3	83	S	115	s
52	4	84	Т	116	t
53	5	85	U	117	u
54	6	86	V	118	v
55	7	87	W	119	w
56	8	88	X	120	x
57	9	89	Y	121	У
58	:	90	Z	122	Z
59	;	91]	123	{
60	<	92	١	124	
61	=	93	11	125	}
62	>	94	٨	126	~
63	?	95		127	Δ

TABLE 1.4
SORT ORDER FOR CODED HANDBOOK DATA FIELDS

	PRODU	П	1
01	Sheet	09	Welded & Stress Relieved
02	Plate	10	Weldment
03	Forging	11	Disk
04	Extrusion	12	Extruded Bar
05	Forged Bar	13	Rolled Bar
06	Billet	14	Bar
07	Casting	15	Hand Forging
08	Round Bar		
	SPECIME	N DESI	GN
01	Compact Tension (CT)	11	Charpy
02	Center Cracked Panel (CCP) (max load specified)	12	Cantilever (Side Grooved)
03	Center Cracked Panel (CCP) (max stress specified)	13	Part Through Surface Crack (PTSC) (max load specified)
04	3-point Notched Bend (3-NB)	14	Single Edge Notched Tension (SENT)
05	Center Notch Tension (CNT)	15	Old Compact Tension
06	Wedge Open Loading (WOL)	16	K _B Bar
07	Bolt Loaded WOL (BWOL)	17	4-point Notched Bend (4-NB)
08	Cantilever Beam (CB)	18	Bend Specimen - Side Grooved
09	Double CB (DCB)	19	Part Through Surface Crack (PTSC) (max stress specified)
10	Tapered DCB (TDCB)	20	Modified Compact Tension (MCT)
	SPECIMEN O	RIENTA	ATION
01	L-S	10	R-L
02	L-T	11	R-C
03	T-S	12	C-R
04	T-L	13	
05	S-T	14	L-T45
06	S-L	15	CS = C-L
07	L-C	16	SC = L-C
08	C-L	17	RS = R-L
09	L-R	18	SR = L-R

TABLE 1.5
ABBREVIATIONS FOR ALLOY CONDITION AND HEAT TREATMENT

Abbreviation	Condition/ Heat Treatment
ABQ	Aus-Bay Quench
AC	Air Cool
BA	Beta Anneal
DA	Duplex Anneal
HAZ	Heat Affected Zone
MA	Mill Anneal
OQ	Oil Quench
RA	Recrystallize Anneal
ST	Solution Treated
STA	Solution Treated and Aged
WC	Water Quench

TABLE 1.6
ABBREVIATIONS FOR PRODUCT FORM

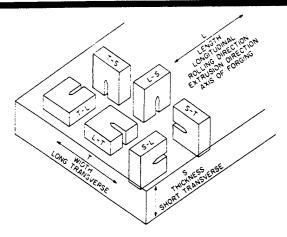
Abbreviation	Product Form
В	Bar
BR	Round Bar
BT .	Billet
C	Casting
D	Disk
E	Extrusion
EB	Extruded Bar
F	Forging
FB	Forged Bar
HF	Hand Forging
P	Plate
RB	Rolled Bar
S	Sheet
W	Weldment
WSR	Welded & Stress Relieved

TABLE 1.7
ABBREVIATIONS AND TERMS FOR TEST ENVIRONMENT

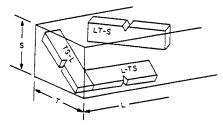
Abbreviation	Test Environment
3.5% NACL	3.5% Salt Water Solution
CCL4	Carbon Tetrachloride
DIST WATER	Distilled Water
DRY AIR	Low Humidity Air (<10% RH)
F.C.S.	Field Cleaning Solvent
H.H.A.	High Humidity Air (>80% RH)
H2O	Water
H2O(D)	Distilled Water
JP4	JP-4 Jet Fuel
L.H.A.	Low Humidity Air (<10% RH)
LAB AIR	Laboratory Air (RH unspecified)
S.C.S.	Shop Cleaning Solvent
S.S.W.	Simulated Seawater
S.T.W.	Sump Tank Water
SALT FOG	Salt Fog

TABLE 1.8
ABBREVIATIONS FOR SPECIMEN DESIGN

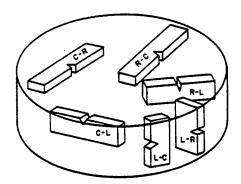
Abbreviation	Specimen Design
4-NB	4-point Notched Bend
BDCB	Bolt-loaded Double Cantilever Beam
BWOL	Bolt-loaded Wedge Open Loading
CANT	Cantilever Beam
CCP	Center Cracked Panel
CHAR	Charpy
CNT	Center Notched Tension
CT	Compact Tension
DCB	Double Cantilever Beam
K _B BAR	K _B Bar
MCT	Modified Compact Tension
NB	Notched Bend
PTSC	Part Through Surface Crack
SENT	Single Edge Notched Bend
TDCB	Tapered Double Cantilever Beam
WOL	Wedge Open Loading



(a) Crack Plane Orientation Code for Rectangular Sections



(b) Crack Plane Orientation Code for Rectangular Sections where Specimens are Tilted with Respect to the Reference Directions



(c) Crack Plane Orientation Code for Bar and Hollow Cylinder

Figure 1.1 ASTM Abbreviations Used to Describe Specimen Orientations

Material Summaries in Table 1.2) for which material summaries are possible. Each summary compares availability or properties of damage tolerant data for the given alloys, heat treatments, and product forms of a particular material.

1.3.1 Available Data Summary

Figure 1.2 presents the fourth page of the available data summary for Aluminum 7000/8000 labeled as TABLE 8.0.1. The first number in the table number is "8" which indicates that this table belongs to the eighth chapter; the second number is "0" which indicates that this is a table in the material summary section. The third number is "1" which indicates that this is the "Available Data" table for this material.

The available data summary defines the property data that are available in a chapter by alloy, condition/heat treatment, and product form. The number is each data type cell in Figure 1.2 indicates the number of test specimens recorded in the handbook database for the specific test conditions of alloy, heat treat, and product form. The six different types of data are listed across the top of the table. Alloys are listed in ASCII collating sequence which is how they appear in the handbook. Heat treatments and conditions are also sorted according to the ASCII collating sequence. Following the sort by alloy and condition/heat treatment, the property data are then sorted according to product form. Product form sort order is outlined above in Table 1.4.

1.3.2 Plane Strain Fracture Toughness Material Data Summary

Figure 1.3 presents the second page of the aluminum 7000/8000 plane-strain fracture-toughness data summary labeled as TABLE 8.0.2. This is the second type of material summary and its third table digit is "2". Data are sorted and grouped by alloy, condition/heat treatment, and product form. Data are listed only for specimens tested in laboratory air at room temperature (65°F - 80°F). Plane

TABLE 8.0.1 (CONTINUED)

AVAILABLE DATA FOR ALUMINUM 7000/8000 SERIES ALLOYS

Alloy	Condition/ Heat Treatment	Product Form	Kle	Ke	R Curve	da/dN	da/dt	Klace
		Extrusion	33			9		
	T6510	Forged Bar	36					
		Extruded Bar				2		
		Forging.				7		
	1651	Extrusion	12		9	01		
	T6511 #8	Forging				-		
		Sheet		27				
	1	Рате				3		
	1/3	Forging	20					
		Forged Bar	•			41		
7075		Sheet		35				
(Cont'd)	T7351	Plato	901	144		96	3	91
		Extrusion	32					
	17361 63.2	Plate				2		
		Extrusion	12			9		
	173510	Extruded Bar				3		
		Extrueion	27			26		
	173511	Extruded Ber						9
		Extrusion				•		
	T73511-111GH PURITY	Extruded Bar	4					
	The state of the s	Extrusion				8		
	73511-LOW PURITY	Extruded Ber	7					

Sample Table (pg 8-6): Available Data Summary for Aluminum 7000/8000 Series Alloys Figure 1.2

TABLE 8.0.2 (CONTINUED)

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF ALUMINUM 7000/8000 SERIES ALLOYS AT ROOM TEMPERATURE

			Bandoof					K) P	K_{Ic} $(Ksi\sqrt{in})$					
Allov	Condition/	Product	Product					Specimen Orientation	men	Orient	ation				
Î	Heat Treatment		Thickness		Ţ	L-T			T	T-L			3 2	S-L	
				Min Spec Thk	=	Mean	Std	Min Spec Thk	£	Mean	Std Dev	Min Spec Tuk	ч	Mean	Std
	174511	Extrusion	075-1.50	0.73	•	40.4	6.0	,	:	!	:	:	:	:	:
	17452	Forging	00:≯	99:1	2	31.1	1.2	1.00	6	23.6	9.0	1	1	i	:
7050 (Cont'd)	T7651	Plate	0.75-1.00	0.74	9	33.4	2.8	:	i	;	:	:	:	:	;
	176511	Extrusion	0.75-1.60	0.73	က	34.8	9.9	::	::	ì	÷	:	:	÷	:
	17556	Forging	6.00	:	ï	:	1	0.75	1	28.9	3.6	÷	;	:	;
	, s	Forging	0.50-0.89	0.50	2	24.3	0.1	0.25	2	20.9	1.7	0.50	-	16.8	0.4
	9	Extrusion	2.00	ï	!	ı	:	0.76	6	19.9	0.2	0.75	8	18.5	0.2
		Plate	0.37-5.00	19:0	8	26.5	2.0	0.38	26	22.5	2.0	0.50	11	17.6	2.7
	T651	Extrusion	3.00.6.00	1.56	-	31.1	9.6	1.60	9	20.2	0.2	i	::		:
		Rolled Bur	6.00	1.60	2	34.1	9.0	:	ı		i	:	i	ı	:
2000	0.300	Extrusion	0.68-3.50	09:0	12	27.5	2.1	0.50	91	23.3	1.6	0.25	3	20.0	1.3
2	01001	Forged Bar	0.68.5.00	0.62	13	29.2	3.4	09:0	13	21.4	1.8	0.25	7	18.7	6:0
	16611	Extrusion	1.26	1.22	2	27.9	7.7	1.17	7	26.9	1.8	;	i		
	173	Forging	1:00	!	!	i	i	i	i	i	1	09:0	•	19.1	9:0
	17361	Phate	1.00-4.00	1970	43	29.4	2.2	0.51	8	26.2	3.2	0.50	7	18.6	0.4
	T73510	Extrusion	0.68-3.50	ı	i	!	1	0.60	٠	24.6	2.3	1.00	3	20.3	0.8
	T73511	Extrueion	3.50	1.68	•	39.6	8.1	1.76	80	26.8	1.1	1.00	8	21.9	1.1

Figure 1.3 Sample Table (pg 8-13): Plane Strain Fracture Toughness Values (Material Summary)

strain fracture toughness values and standard deviations mean are listed for the three most frequently occurring specimen orientations; i.e., L-T, T-L and S-L. Product thickness range and minimum specimen thicknesses are listed for general information. Dashes in a particular column indicate that no mean plane strain fracture toughness data exist for the stated conditions.

1.3.3 Plane Stress and Transitional Fracture Material Data Summary

The plane stress and transitional fracture toughness data summary is presented third in the series of summaries. Two tables may be presented for a material type if sufficient data are available. The first table (Figure 1.4a) presents test data for specimens where buckling constraints were not imposed. The sequence number for this type of table is C.0.3.1, where C is the material chapter number. The second table (Figure 1.4b) presents test data for specimens where buckling constraints were applied. The sequence number of this table is C.0.3.2, where C is the material chapter number. The third digit of the table number is always "3". Observe that the fourth digit is "1" and "2" for test specimens without and with buckling constraints, respectively. The data are sorted in both table types by alloy, condition/heat treatment, test temperature, specimen orientation and specimen width. Yield strength is not a sorting field but is included for general information. Mean K_c values are listed as a function of specimen thickness which is indicated across the top of the page. Specimen thickness variations run along the top of the page and may vary from table to table to prevent overcrowding in the tables while still accommodating all of the data. Individual K_c data values are listed only if useful in determining a trend in the data.

1.3.4 Fatigue Crack Growth Rate Material Data Summary

Figure 1.5 presents a sample fatigue crack growth rate (FCGR) summary taken from the Aluminum 7000/8000 Chapter. The data are from Table 8.0.4.2, a four number sequenced designation. The first two numbers again indicate

TABLE 8.0.3.1

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PLANE STRESS AND TRANSITIONAL FRACTURE TOUGHNESS

				1								*	K, (Ksk/in)	/in)						
Con Heat T	Condition/ Heat Treatment	Test Temp	uallinada a		Yield Strength			=	S.	Sp. Sample size	Spe	ecime	Specimen Thickness (in.) ze μ·Mean σ·Standı	knes o - E	s (in.	kness (in.) σ - Standard Deviation	eviat	ion		
		}	Oriont	Width	(Igy)	٦	0.063			0.125			0.250			0.200		-	1.000	
			Circus	(in.)		=	=	o	6	=	0	•	_	0	E	=	ь	=	=	ъ
			LT	20.0	70.6-72.2			::	i	i	1	1	ı	:	;		:	2	33.0	6.9
	T75	R.T.	1 4	3.0	67.7-68.6	ï	:	i	12	39.5	2.6	1	;	1	:	:	!	!	:	i
			3	20.0	69.6-71.3	:		-	;;	:	:	!	ı	-	;	1	!	2	286	3.2
			£	15.0	73.6	:	::	::	: :				i	;	2	64.0	12.7		;	;
			:	16.0	75.7-80.1	9	9.99	6.0	စ	2.09	1.3	2	6.69	7	!	;		1		:
				3.0	72.9.77.0	:	i.		9	919	2.6	1	i	i	:	:	:	1	,	;
	J.	R.T.		6.0	75.5	8	6.83	4.0	ï	i	:	;	i	i	:	:	;	-	1	;
			Ţ.Ľ	15.0	73.3-76.0	-				:	:	2	57.2	3.7	~	49.3	6	,	:	:
				16.0	72.9	9	62.1	3.4		ı	!	;	i	1	1	;	1	1	;	1
				24.0	69.0-75.6	7	46.2	6.8		ı	-	:-		1	:	:	!	i	;	;
				3.0	17.3.79.1		i	:	8	62.6	5.9	2	46.2	0.	i	;	ı	!	1	i
			2	4.0	77.3		i	÷	-	i	ı	2	61.3	4.6	i	:	1	1	ŀ	;
				20.0	76.6-80.3	-:	ï	:	:	i	!	ł	i	1	i	i	1	2	16.4	=
	T651	R.T.		3.0	13.4.77.7		:	ï	•	48.6	1.2	18	43.9	3.2	ī		:	!	1	1
			Ē	4.0	72.0-75.4		i	-	ij	ì	!	12	50.2	4.6	2	94.9	1.5	· i	1	i
			2	16.0	11.2		i	-;	ı	i	ī	ï		1	8	47.8	3.6	1	;	i
				20.0	13.6.77.4	ï	ï	-	-	ı	:	-	I		1	: .	1	13	1.98	82
	£7T	98	LT	16.0	60.0	2	82.9	3.6	-	i	1	-		1	i	:	j	1	1	ı
	17361	R.T.	LT	8.0	61.1-62.1	i	i	i	1	i	i	1		i	8	61.4	10.4	8	46.8	63
				16.0	61.1-62.1	i	ì	ı	!	•	!	I	1	i	i	ı	1	7	62.7	6.3
				20.0	60.8-64.6	ì	i	i	1	-	-	1	ı	i	I	1	-	12	9.96	9.0
				36.0	61.1-62.1	i	ï	i	i	1	i	ŧ			_	1		8	9.99	8
			T:F	20.0	63.6	i		:	1	i	:	1	1	1	i	ï	:	-	1.81	2
																	ĺ			

Figure 1.4a Sample Table (pg 8-16): Plane Stress and Transitional Fracture Toughness without Buckling Constraints (Material Summary)

l of l

TABLE 8.0.3.2

ALUMINUM 7000/8000 SERIES ALLOYS (WITH BUCKLING CONSTRAINTS) PLANE STRESS AND TRANSITIONAL FRACTURE TOUGHNESS

									ļ ļ			X	K, (Ksl√ln)	E						
Allov	Condition/	Test Temp	apecimen	# # # # # # # # # # # # # # # # # # #	Yield Strength				,		Spe	cime	Specimen Thickness (in.)	knes	g (in.)					
•	Heat Treatment	(e.F.)			(Kai)			=	Sat	nple (ezi.	- I	n · Sample size	30	tand	ard De	viati	no		
		<u>;</u>	Orient	Width			0.058			0.080			0.090		٦	0.100			0.280	
				(jn.)		c	ュ	D	5	1	Đ	E	1	ь	-	=	ь	=	=	٥
7050 (ALCLAD)	176	R.T.	LT	20.0	67.2	64	114.0	7.6	!	ı	-	ı	,	1	;		i	-	i	1
				12.0	16.9	::	!	!	:	i	ı	8	8.17	2.8	1	1	:	i	ı	!
				15.0	16.2	1	:			i	ï	i	i	1	1	;	1	~	76.6	~
	22	R.T.		24.0	75.9	i	÷	:: :		:	ï	i	i	:	~	71.6	64	i	i	:
7075				36.0	75.9	::	i	::	i	:	-1	1	1	i	20	72.8	9	1	1	!
				24.0	76.5	01	73.3	8.1	:	i	1	ï	i	!	i	ł	;	1	ļ :	!
	T651	R.T.	LT	0.8	78.9	9	63.4	9.9	:	ï	-	i	i	ı		į	1	ï	;	:
	17361	R.T.	LT	36.0	60.6	ï	ï	-:	::	:	i	;	:	ļ	:	1	1	2	119.8	23.9
				6.0	73.1	i	;		9	60.1	6.0	ı	ì	1	1	1	1	1	;	;
7076 (ALCLAD)	J.	R.T.	LT	12.0	13.1	:	÷	::	11	10.1	7.1	i	ı	ł	1	,	i	;	ï	1
				24.0	13.1	i	ŧ	!	20	69.3	10.4	į	i	;		1	;	1	ï	:

Sample Table (pg 8-19): Plane Stress and Transitional Fracture Figure 1.4b Toughness with Buckling Constraints (Material Summary)

TABLE 8.0.4.2 (CONTINUED)

100.0 FREQUENCY: 0.08 - 40. Hz 80.0 FATIGUE CRACK GROWTH RATE (FCGR) COMPARISON AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK FOR ALUMINUM 7000/8000 SERIES ALLOYS IN LAB AIR AT ROOM TEMPERATURE ΔK Level (Kai√in) PCGR (10.º tr/grale) 68.19 63.88 657.63 63.63 59.24 65.66 80.15 49.44 20.0 20.0 61.61 13.04 14.84 17.11 13.77 24.33 20.79 14.89 14.98 3.04 10.0 17.34 7.7 8.02 0.78 0.99 1.01 1.18 0.72 3.05 0.74 0.68 1.67 **0** 1.69 9 90.0 0.0 0.19 0.09 0.1 #2 #4 FREG 0.1.30 0.1-30 0.1-30 2.9 1-30 5.5 2 \$ ಜ 2-5 7.6 2 2-6 5.5 2 STRESS RATIO: -1.0 - 0.8 33 0.33 9.0 0.01 ē 9.0 0.05 0.33 9.0 0.1 0.5 0.1 0.05 0.02 0.02 9.0 0.02 0.02 ***** EXTRUDED BAR UNSPECIFIED EXTRUSION PRODUCT FORM EXTRUSION FORGING PLATE CONDITION/ HEAT TREATMENT T6611 1861 ORIENTATION: L-T 7076 (Cont'd) ALLOY

Figure 1.5 Sample Table (pg 8-26): Fatigue Crack Growth Rate Comparison (Material Summary)

the chapter (8) and the summary section (0). The third number in the sequence (4) indicates that this is an FCGR summary table. The fourth number in the sequence (2) indicates that this is the second ordered table in the fatigue crack growth rate summary for a given material. When only a single FCGR summary table is available for a material, the fourth number in the sequence is dropped. Readers will find one table for each specimen orientation for which there are enough data for the table to have meaning.

All data in a particular summary table were collected under conditions where the environment is laboratory air at room temperature. The stress ratio and loading frequencies vary slightly depending on the individual tests. The range of test conditions are listed at the top of each table. Beneath the general description of test conditions are the data fields of alloy, condition/heat treatment and product form for which the FCGR data comparisons can be made. Predefined ΔK levels are listed across the top of the table and are a subset of the levels associated with the tabular format of the mean trend FCGR data. See Section 1.6 for a list of all predefined mean trend ΔK levels. Fatigue crack growth rates expressed in 10^{-6} inches/cycles are listed in the applicable columns and rows according to the alloy, condition/heat treatment, and product form. With this format, it is easy to determine which materials, heat treatments, or product forms have the lowest growth rate at a particular ΔK level.

1.3.5 Stress Corrosion Cracking Threshold Material Data Summary

Figure 1.6 illustrates the stress corrosion cracking threshold material data summary - the fifth possible material data summary. The sequence number assigned to this table type is C.0.5, where C is the material chapter number. Because of the small number of specimens (typically one or two) that are used to generate these data, individual results are presented here rather than means and standard deviations. The data are sorted by alloy, condition/heat treatment, product form and specimen orientation. Possible environments for which $K_{\rm Iscc}$ data exist are listed

TABLE 8.0.5 (CONTINUED)

	STRESS CORROSION CRACKING THESHOLD DATA FOR ALUMINUM 7000/8000 SERIES ALLOYS AT ROOM TEMPERATURE	ON CRACK ERIES AL	ING THES LOYS AT I	SHOLD SOOM	DATA	ERATUR	9	
						K _{loc} Ksi√in	Į.	
Alloy	Condition/ Heat Treatment	Product Form	Specimen Orientation			Environment	nt	
				3.5% NaCl	Shop Cleaning Solvent	Sump Tank Water	JP-4 Jet Fuel	Simulated Seawater
			L-T		26.6(2)	21		
7049 (Cont'd)	T7352	Forging	T-T			20(4)		
			T-S			18.6(4)		
	OPPE		L-T	28.2				
	1730	rorging	T.L	24.5				
7050	T73651	Plate	T-L	29.1		27.8(2)		
	ואטנהו	ā	L-T				22.5(2)	22.(2)
	1,051	Flate	T-L				22.5	22.3(2)
	Т6	Plate	S-L	19				
	100E	ā	L-T	28.3				
	1001	Flate	S-L	11				
7075	T73	Forging	T-L			22		
			L-T				28.7(4)	28.6(4)
	T7351	Plate	T-L	23.9				
			S-L	21		14.1(2)		

Figure 1.6 Sample Table (pg 8-42): Stress Corrosion Cracking Threshold (Material Summary)

across the top of the table. K_{Iscc} data values for each particular environment are listed in the appropriate row and column. This table summary allows for comparisons of K_{Iscc} values of various materials in a particular environment as well as a quick assessment of how various environments affect a particular material.

1.4 ALLOY SECTION SUMMARIES

Following the material summaries, the data are divided into sections by alloy. Each alloy section is further divided into three subsections: a data summary subsection, a fracture toughness subsection, and a crack growth resistance subsection. The data content and format for these three subsections are described in this and the following two subsections, respectively.

There are two possible alloy summaries: a plane strain fracture toughness summary and a fatigue crack growth rate data summary. Tables in these summaries are labeled C.A.1..., where C is the material chapter number, A is the alloy section number, and "1" identifies the alloy summary section. A fourth number appears on each table in this section. The numbers "1" and "2" in the fourth position indicate plane strain fracture toughness and fatigue crack growth rate, respectively. A fifth number is appended to the fatigue crack growth rate table number when multiple tables exist for an alloy.

Figure 1.7 presents the tabular format for the K_{Ic} alloy summary. It is similar to the K_{Ic} material summary in that the mean and standard deviation for a particular condition/heat treatment, product form, and specimen orientation is given for each alloy. However, the number of specimens used to generate the data has been added. The data are sorted by product form, condition/heat treatment, and specimen orientation. This summary groups K_{Ic} data by condition and product form for easy comparison. It also allows for quick assessment of the effect that orientation has on fracture toughness.

1 of 2

TABLE 8.9.1.1

FOR ALUMINUM 7000/8000 SERIES ALLOY 7075 AT ROOM TEMPERATURE MEAN PLANE STRAIN FRACTURE TOUGHNESS

Droduct					K_{Ic}	$K_{Ic}~(ksi\sqrt{in})$	<u>(u</u>			
Form	Condition/Heat Treatment			32	pecime	Specimen Orientation	itation			
			L-T			T·L			S-L	
		Mean K _{ie}	Std Dev	E	Mean K _i	Std Dev	u	Mean K _{is}	Std Dev	a
	T651	26.5	2.	63	22.5	2.	15	17.6	2.7	11
Plate	T7351	29.4	2.2	47	26.2	3.2	98	18.5	0.4	7
	T7651	28.5	1.5	26	23.1	2.	46	17.8	1.6	16
	T6	24.3	0.1	2	20.9	1.7	2	16.8	0.4	4
	T73	:	:	ï	:	:	:	19.1	0.6	4
Forging	T7352	33.6	3.1	14	26.6	2.8	13	21.7	3.2	89
	T73652	35.	1.8	8	26.6	2.7	8	;		i
	176	:	i	ì	19.9	0.2	8	18.5	0.2	3
	T651	31.1	0.5	4	20.2	0.2	æ	1		i
ا ا	T6510	27.6	2.1	12	23.3	1.6	16	20.	1.3	က
Extrusion	T6511	27.9	1.4	2	28.9	1.8	4	÷	:	i
di - op	T73510	:	:	i	24.6	2.3	6	20.3	9.0	87
	T73511	39.6	3.1	4	26.8	1.1	8	21.9	1.1	2
	T76511	35.7	4.4	9	23.6	2.8	4	ij	i	;

Sample Table (pg 8-452): Mean Plane Strain Fracture Toughness at Figure 1.7 Room Temperature (Alloy Summary)

The FCGR alloy data summaries shown in Figure 1.8 are similar to the FCGR material data summaries described previously. Note that for a particular alloy, the data are separated by the test variables of specimen orientation and environment which are listed at the top of each page. The sort order of specimen orientation is shown in Table 1.4 and environment is sorted alphabetically. Other test variables such as condition/heat treatment, product form, stress ratio and frequency are then listed for the data as noted. Typically, a number of FCGR data summaries are produced to describe the effects of specimen orientation and environments. The condition/heat treatment and product form yielding the lowest crack growth rate in a given environment for a given specimen orientation may be determined from these summary tables. Discrepancies in data sets can also be noted as well as a quick determination of how stress ratio and frequency affect the crack growth in a particular environment.

1.5 ALLOY FRACTURE TOUGHNESS SUBSECTION FORMATS

Within each alloy section following the alloy summaries is the fracture toughness type data. Fracture toughness data consist of plane strain data (K_{Ic}), plane stress and transitional fracture toughness data (K_c), and resistance curve data (R-curves). Each of these has a different and yet somewhat similar ordering scheme which is particularly suited to that type of data. Tables and figures in these sections are labeled C.A.2..., where C is the material chapter number, A is the alloy section number, and "2" indicates the fracture toughness section. A fourth number appears on each table and figure. The numbers "1", "2", and "3" in the fourth position indicate K_{Ic} , K_c , and R-curve, respectively. K_{Ic} and K_c tables may have multiple pages. Page sequence numbers are given to the upper right of each table. A fifth number is assigned to R-curve plots when multiple plots are available for an alloy.

1 of 2

TABLE 8.9.1.2.4

100.0 FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 60.0 PCGR (10⁻⁸ in/cycle) ΔK Lovel (Ksi√in) 20.0 ENVIRONMENT: H.H.A. 23.98 28.69 70.23 10.0 17.22 16.9 6.36 1.45 1.01 4.19 0.48 9.6 0.05 0.42 0.13 7075 AT ROOM TEMPERATURE 1Q 04 FREQ (Hz) 13.3 20 25 26 6 6 6 0.33 0.33 0.05 0.33 8 9.0 0.7 2 ö PRODUCT FORM SHEET PLATE ORIENTATION: L-T CONDITION/ HEAT TREATMENT 7651 2

52.37 176.08

3.07

1.81

13.85

0.05

EXTRUSION

T6511

9.0

0.0 0.0

FORGED BAR

T73

27.3

14.55

Figure 1.8 Sample Table (pg 8-457): Fatigue Crack Growth Rate at Defined Levels of Stress Intensity (Alloy Summary)

1.5.1 Plane Strain Fracture Toughness Data

The format for the plane-strain fracture toughness data is shown in Figure 1.9. This particular example is taken from the aluminum 7000/8000 chapter for alloy 7075. The data are sorted by condition/heat treatment, product form, test temperature, orientation and yield strength using the primary sort order identified in Section 1.2.1. K_{Ic} data collected for similar test conditions are grouped together with the mean and standard deviation listed in a column near the right of the page. Product thickness is listed after product form, but is not a sorting parameter. Specimen dimensions (thickness and width) and crack length are also listed, but not sorted in any particular order. The $2.5(K_{Ic}/\sigma_{ys})^2$ criterion value is included for information purposes only. Two additional columns list the date of the reference and the reference number so that when and where the data were collected can be assessed, and where additional information might be obtained should it be desired. Footnotes may be given as a number enclosed in parentheses behind the reference number. Footnotes are used to indicate out-of-range conditions, average data values, and other important identifying features.

Reference numbers from the earlier versions of the handbook have been retained and new data have been assigned a new reference number with the first two or three characters identifying the organization or journal from which the data was obtained. Table 1.9 lists the general format for later reference numbers.

1.5.2 Plane Stress Fracture Toughness Data

The format for presenting plane stress fracture toughness (K_c) data is presented in Figure 1.10. Plane stress fracture toughness data within a particular alloy section are ordered by condition/heat treatment, buckling of crack edges (restrained, unrestrained, or unknown), product form, test temperature, specimen orientation, specimen thickness and specimen width. Additionally, initial and final crack lengths are given as a function of the total crack length (2a) for center-cracked

						ALUMINUM		7075 K _{lo}	_						
	PRODUCT	ucr					SPECIMEN	N.S.	CRACK			K _{lo}			
CONDITION	КОКМ	THICK (In.)	TEST TEMP (*P.)	SPEC OR	YIELD STR (Kul)	WII) (le.) W	THICK (In.)	DESIGN	(in.)	8.6 (K_TYB)* (In.)	(£ 7.	H. MKAN	BFAN	DATE	нялян
9.5	Porsing	0.50	÷	÷	79.0	1.000	0.500	CT	0.634	0.23	24.20			1973	86213
		93.0		5	79.0	1.000	0.500	ಕ	0.623	0.24	24.40	24.3	7.	1973	86213
	Parana	0.89	=		67.2	0.500	0.249	NB	0.265	0.21	19.70			1973	86213
		0.69		:	70.0	0.500	0.249	INB	0.273	0.25	22.10	20.9	1.7	1973	86213
		0.50			65.4	000 1	0.499	cr	0.493	0.17	17.00			1973	86213
318	Parent	050	<u>:</u>	5	65.4	1.000	0.500	£	0.510	0.16	16.70			1973	86213
		03:0		<u>.</u>	65.4	1.000	0 500	ະວ	0.496	0.16	16.40	8:91	. U.4	1973	86213
		0.50			65.4	1.000	0.500	£	0.505	0.17	17.20			1973	86213
76	Porging	0.75	82	1.1	6.69	2.000	0.500	cr	1.025	0.44	29.20	:	:	1973	86213
		0.89			57.4	1.600	0.749	cr	0.785	0.32	20.40			1973	86213
3.1.0	Forging	0.89	85	7:1	57.4	1.600	0.749	ст	0.762	0.32	20.40	19.4	7.1	1973	86213
		0.76			67.6	1.000	0.500	C.	0.511	0.17	17.50			1973	86213
9,1	Poemiou	0.89	78	£	0.89	1.500	0.750	5	0.792	0.24	21.20			1973	86213
2		0.89	5		0.89	1.600	0.760	r.	0.798	0.22	20.00	50.6	9.0	1973	86213
		2.00			72.0	1.500	0.750	ct	0.797	0.19	20.00			1973	86213
22	Extrusion	2.00	H.T.	7:	73.6	1.500	0.749	ಕ	0.798	0.18	19.70	16.0	0.2	1973	86213
		2.00			73.6	1.500	0.748	៦	0.791	0.19	20.10			1973	86213
		2.00			67.0	1.500	0.748	5	0.791	0.19	18.50			1973	86213
21	Extrusion	2.00	II.T.	3.5	67.0	1.600	0.750	៦	0.798	0.18	16.30	18.6	0.3	1973	86213
		2.00			67.2	1.600	0.749	СŢ	0.608	0.19	18.70			1973	86213
21.	Forged	;	Ē	5	9.89	1.600	0.750	ដ	0.750	0.20	19.60			1972	62879
-	Bar	;		5	9:89	1.600	0.750	СŢ	0.750	0.20	19.30	19.6	0.3	1972	82879

Figure 1.9 Sample Table (pg 8-487): Plane Strain Fracture Toughness Data by Alloy

TABLE 1.9

REFERENCE NUMBER EQUATES TO ORGANIZATIONS AND JOURNALS

Reference Number	Organization or Journal Equate
ALxxx	Alcoa Laboratories - Alcoa Center, PA
ALLxx	Allison Gas Turbine Division, GM, Indianapolis, IN
AMxxx	Airesearch Manufacturing, Los Angeles, CA
BLxxx	Battelle Columbus Laboratories, Columbus, OH
BWxxx	Boeing Military Airplane Co., Wichita, KA
DAxxx	Douglas Aircraft, Long Beach, CA
EFMxx	Journal of Engineering Fracture Mechanics
FRxxx	Fairchild Republic, Farmingdale, NY
GDxxx	General Dynamics, Fort Worth, TX
GExxx	General Electric, Evendale, OH
HDxxx	Westinghouse Hanford Development Lab, Richland, WA
JEMxx	Journal of Engineering Materials and Technology
LGxxx	Lockheed Georgia, Marietta, GA
MAxxx	McDonnell Aircraft Co., St. Louis, MO
MDxxx	McDonnell Douglas Astronautics Corp, Huntington Beach, CA
MRxxx	Materials Research Laboratory, Glenwood, IL
NCxxx	Northrop Corporation, Hawthorne, CA
NHxxx	NASA Houston, Houston, TX
NLxxx	NASA Langley Research Center, Hampton, VA
NRxxx	Naval Research Laboratories, Washington, DC
PWxxx	Pratt & Whitney Aircraft Group, Government Products Division, West Palm Beach, FL
RAxxx	Reynolds Metals Co., Richmond, VA
RIxxx	Rockwell International, North American Division and Shuttle Orbiter Divsion, Los Angeles, CA
SAxxx	Sikorsky Aircraft, Stratford, CN
SWxxx	Southwest Research, San Antonio, TX
UCxxx	University of Cincinnati, Cincinnati, OH
UDxxx	University of Dayton Research Institute, Dayton, OH
UMxxx	University of Missouri, Rolle, MO
UVxxx	University of Virginia
WAxxx	Wright Aeronautical Laboratories, WPAFB, OH
WLxxx	Wright Patterson Materials Laboratory, WPAFB, OH

TABLE 8.9.2.2 (CONTINUED)

							AI	AI.UMINUM	NOW	7075	К _с								
	PROI	PRODUCT				SPECIMEN	MEN	CRACK LENGTH	СК	GROSS STRESS	88		K.pp			К _с			
CONDITION HEAT THEAT	РОКМ	THICK (in.)	TRMP (°F)	SPEC		WIDTH 1	THICK (In.) B	INIT (in.)	FINAL (in.) 2e,	ONBRT (Kal)	MAX (Kai)	K. (Kei Vin)	MBAN	BTAN DRV	K _o (Katvita)	K, MBAN	BTAN	DATE	нялян
							SUCKLIN	IG OF CI	BUCKLING OF CRACE EDGES NOT RESTRAINED	GES NOT	HESTRA	LINED							
		90:0			71.8	3.000	0.061	1.060	;	::	36.50	60.76			-			1973	86213
		90:0			71.8	3.000	0.061	1.120	ï		34.30	49.86			!			1973	86213
i		90.0			71.8	3.000	0.061	1.080		- 1	34.80	49.33						1973	86213
2	ta Short	90.0	X.		71.8	3.000	0.061	1.050	;	;	35.50	49.37	1.03	9.0	i	1	:	1973	86213
		90.0			71.8	3.000	0.061	1.060	:	:	35.70	49.97			***			1973	86213
		90.0			76.6	3.030	0.063	0.750	0.770	ï	46.50	61.34			62.13			1966	86734
		0.12			72.9	3.000	0.123	1.060	1.350	:	31.30	43.63			62.27			1973	86213
		0.12			72.9	3.000	0.123	1.050	1.380	i	33.90	47.15			67.63			1973	86213
		0.12			72.9	3.000	0.123	1.110	1.410	:	32.90	47.52			£6.93•			1973	86213
		0.12			72.9	3.000	0.123	1.070	1.320	:	32.50	46.78			63.31			1973	86213
		0.12			72.9	3.000	0.123	1.100	1.450	i	34.00	48.80			60.25			1973	86213
		0.12			72.9	3.000	0.123	1.090	1.380	:	32.60	46.50			56.42			1973	86213
T6	Sheet	0.12	H.T.	Ţ:Ľ	72.9	3.000	0.123	1.130	1.420	1	32.50	47.63	46.8	58	66.57*	919	2.6	1973	86213
		0.12			74.1	3.000	0.123	1.000	1.380	- 1	35.40	47.68	,		60.18			1973	86213
		0.12			74.1	3.000	0.123	1.000	1.250	į	34.50	46.46	,		64.28			1973	66213
		0.12			74.1	3.000	0.123	1.000	1.240	i	34.10	45.92			63.32			1973	86213
		0.12			74.1	3.000	0.123	1.000	1.360	1	36.70	49.43			61.66			1973	86213
		0.12			72.9	3.000	0.124	81.1	1.240	!	31.00	44.50	-		48.48			1973	66213
		0.12			72.9	3.000	0.124	1.120	1.340	1	31.80	46.22			62.79			1873	96213

• NOTE: NET BECTION STREBS EXCEEDS 80% OF YIELD STRENGTH. VALUE NOT INCLUDED IN MEAN OR STANDARD DEVIATION.

Figure 1.10 Sample Table (pg 8-532): Plane Stress and Transitional Fracture Toughness Data by Alloy

panel specimens. Also, the onset and maximum gross stress values are listed when available. The fracture toughness parameters K_c and K_{app} are calculated as described in Chapter 2 and the individual as well as the mean and standard deviation values are listed for both K_c and K_{app} . The final two columns present the date of the reference and the reference number.

1.5.3 R-Curve Data

The format for resistance curve (R-Curve) data is shown in Figure 1.11. The information listed at the top of the page includes alloy, condition/heat treatment, product form, product thickness (if known), specimen design, specimen orientation, specimen dimensions (thickness and width), K_c value (if known), and reference number. Unless otherwise specified, the data were tested at room temperature in laboratory air environments. Only one specimen is illustrated per figure, and the figures are sorted by alloy, condition/heat treatment, test temperature and environment, specimen orientation, specimen thickness, and specimen width. Resistance curve data are plotted on linear axes with applied stress intensity K_R (Ksi \sqrt{in}) as a function of change in effective crack length $\Delta a_{\rm eff}$ (in.). Section 2.4 contains details associated with the R-curve calculation.

1.6 SUBCRITICAL CRACK GROWTH SUBSECTION FORMATS

The subcritical crack growth data follow the fracture toughness data within each alloy section. The subcritical crack growth data includes: fatigue crack growth rate data, sustained load crack growth rate data, and stress corrosion cracking threshold data. Figures and tables in these sections are labeled C.A.3..., where C is the material chapter number, A is the alloy section number, and "3" indicates subcritical crack growth sections. A fourth number appears on each figure and table. The numbers "1", "2", and "3" in the fourth position indicate fatigue crack growth rate, sustained load crack growth rate, and stress corrosion cracking threshold data, respectively. Both the fatigue and sustained load crack growth rate figures have a fifth number when multiple plot sets exist for an alloy.

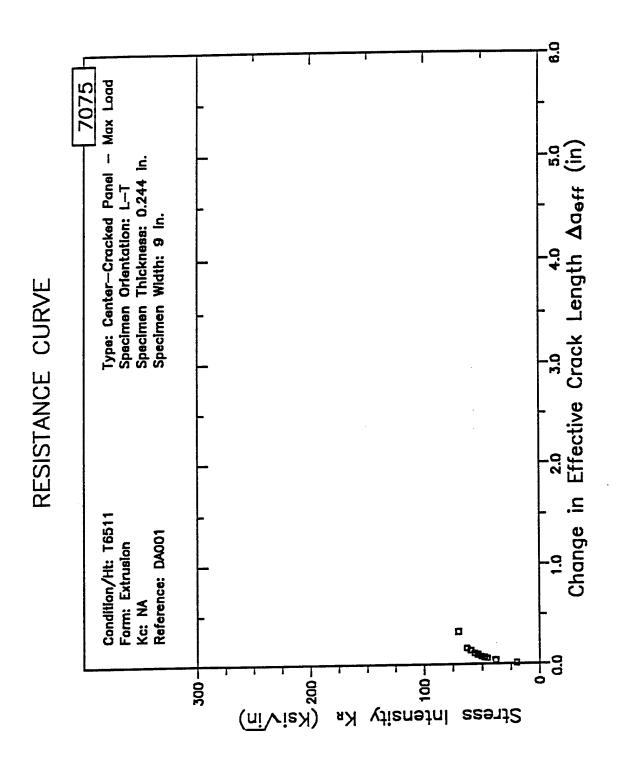


Figure 1.11 Sample Figure (pg 8-554): R-Curve Data by Alloy

1.6.1 Fatigue Crack Growth Rate Data

Fatigue crack growth rate data are presented in two complementary formats: graphical (data points overlaid with a mean trend curve) and tabular (listing of mean trend data points). The data on a page describe the effects of one of three varying parameters - stress ratio, environment/test temperature, or frequency. A header window lists parameter values which are considered constant for all test data being presented. Plots for two values of the varying parameter can be presented on a given page. Multiple pages are used to present plots for three or more values of the varying parameter. In addition to the da/dN- Δ K plots and mean trend tables, minimum and maximum Δ K, root mean square percent error, and life prediction ratio of the mean trend curve are given when available. All plots having similar header data are subsequently referred to as a plot set.

Figure 1.12 shows an actual page of fatigue crack growth rate data from the handbook. Each page consists of five data block types: 1) header block, 2) FCGR plot block, 3) mean trend block, 4) root mean square (RMS) block, and 5) life prediction ratio (LPR) block. The header block is common to the plot set. Data block types 2 through 5 are specific to one value of the varying parameter.

The header block identifies the alloy, the varying parameter, and constant values for all plots in the current plot set. The alloy is identified in the upper outside corner of the plot page. The varying parameter is also identified in the upper outside corner by the presence of the capital letters "R" (stress ratio), "E" (environment), "F" (frequency), or "EF" (combination of environment and frequency). Environment is the varying parameter in Figure 1.12. Condition/heat treat, product form/thickness, specimen type, specimen orientation, tensile yield and ultimate strengths, specimen thickness, specimen width, and references always appear in the header block if available. Stress ratio, environment, and frequency are also listed in the header block when they are not the varying parameter. Values of certain constant parameters are given as ranges when the values are close enough to be considered similar.

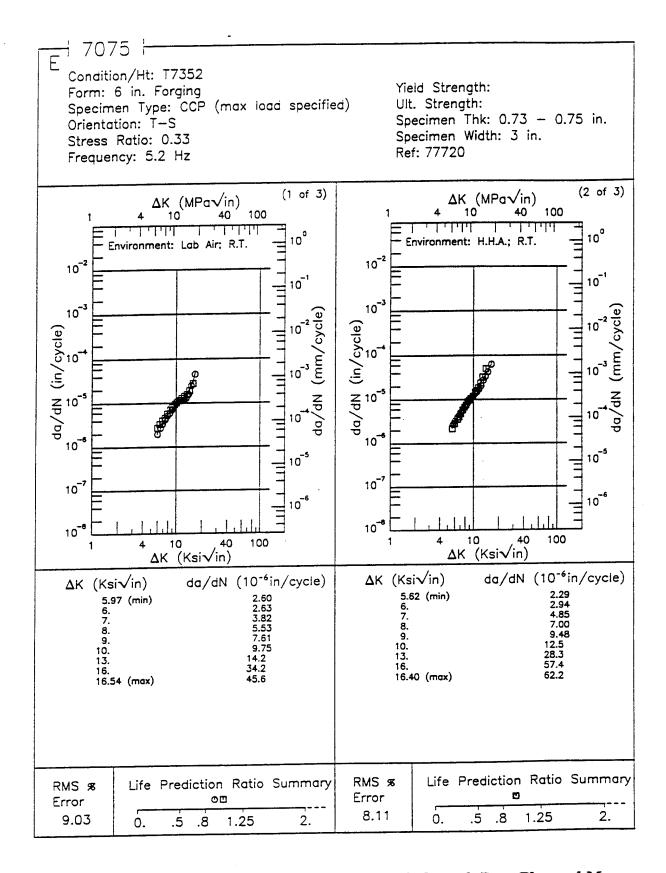


Figure 1.12 Sample Figure (pg 8-698): Fatigue Crack Growth Rate Plot and Mean Trend Fit

The FCGR plot block consists of the following four items: 1) a trend plot of da/dN- Δ K data, 2) the value of the varying parameter, 3) a mean trend curve (if available), and 4) the plot set sequence number. Fatigue crack growth rate (da/dN) is plotted as a function of the range of stress intensity (Δ K). The definition of Δ K according to ASTM Standard E647, i.e., Δ K = K_{max} if stress ratio is negative, was chosen for data presentation throughout the handbook. The logarithmic x-axis represents Δ K and spans from 1 to 200 Ksi \sqrt{i} n. The logarithmic y-axis represents da/dN and spans 7 decades from 10^{-8} to 10^{-1} inches/cycles. English units, i.e., inches/cycle for da/dN and Ksi \sqrt{i} n for Δ K, are listed to the left and bottom of each plot respectively. The corresponding metric units for da/dN and Δ K, i.e., mm/cycle and MPa \sqrt{i} m, respectively, are placed on the opposite side of the plot as their English counterparts.

The trend plots in Figure 1.12 indicate that multiple plot symbols may be used. Each symbol represents a unique set of test data. Up to eight different tests can be accommodated in a single plot. If more than eight tests have common header data, then additional plots are generated. Each plot uses the same plot symbols; however, the data they represent are independent from plot to plot. If eight or more data points exist, a mean trend curve is fit to the plotted data using a cubic spline polynomial. The cubic spline polynomial fit method is described in Section 2.5.4.

The sort order in which fatigue crack growth rate data are presented is as follows: alloy, condition/heat treat, product form, product thickness, specimen design, and specimen orientation. The ordering by product form has been revised so that similar product forms such as extruded bars/extrusions and forged bars/forgings can be presented next to each other. Table 1.10 presents the revised sort order of product form. Table 1.4 above presents the sort order of specimen design and specimen orientation.

TABLE 1.10

ALTERNATE PRODUCT FORM SORTING ORDER FOR CRACK PROPAGATION DATA

Product Form
Product Form
Sheet
Plate
Bar
Billet
Disk
Extrusion
Extruded Bar
Forging
Hand Forging
Forged Bar
Rolled Bar
Round Bar
Casting
${\bf Weldment}$

Given that certain test data have similar values for the above mentioned parameters, individual plots in a plot set are presented in order by varying parameter. Plot sets varying stress ratio are placed before plot sets varying environment which in turn are placed before plot sets varying frequency. For varying stress ratio, plots are presented in ascending stress ratio order. When environment is the varying parameter, plots are presented in alphabetical order on environment and ascending test temperature. For varying frequency, plots are presented in ascending frequency order.

The mean trend window presents fatigue crack growth rate values calculated at predefined ΔK levels based on the cubic spline polynomial curve fit to

the test data. Table 1.11 lists the 30 possible ΔK levels for which corresponding da/dN crack growth rates may be calculated. The minimum and maximum ΔK values observed in the test data are included and delimit the range of predefined ΔK levels to be included in a mean trend table. If less than eight data points are available, the mean trend window is empty.

TABLE 1.11
PREDEFINED AK LEVELS

1.0	1.3	1.6	2.0	2.5	3.0	3.5	4.0	5.0	6.0	7.0	8.0	9.0
10.	13.	16.	20.	25.	30.	35.	40.	50.	60.	70.	80.	90.
100.	130.	160.	200.									

The RMS data block presents root mean square percent error (RMS % Error) which is a description of scatter about the mean trend line; i.e., a smaller value indicates less scatter than a larger value. The RMS block is empty if a mean trend cannot be generated. The calculation of the root mean square percent error is described in Section 2.5.4.

The LPR data block reports the life prediction ratio for specimen test data plotted in the plot block. The LPR is the number of cycles predicted using the mean trend curve divided by the actual number of cycles taken from the experimental crack length versus cycle (a-vs-N) data for a predefined interval. Plot symbols are placed along a scale ranging from zero to two with intermediate tic marks at 0.5, 0.8, and 1.25. The plot symbol placed along the scale is the same plot symbol used to represent a specimen test in the trend plot above. LPR values which fall between 0.8 and 1.25 indicate an adequate mean trend fit. For threshold type tests and for tests in which the loads were varied frequently during the test, LPR values tended to be well outside this range. Some test data shown on the trend plot do not have a calculated LPR value because the data were received in reduced form, i.e., da/dN-vs- Δ K rather than a-vs-N, and therefore had no actual cycle count for comparison. If a mean trend fit cannot be generated, no plot symbols appear in the LPR data block.

1.6.2 Sustained Load Crack Growth Rate

The sustained load crack growth rate data are presented after the fatigue crack growth rate data and are plotted on log-log scales in a manner similar to the FCGR data (See Figure 1.13). The data are plotted to present time based crack growth rate as a function of maximum stress-intensity factor on pages with header blocks and two graphs of equal size with both English and Metric units lining opposite sides of the plot. The alloy is identified in the upper outside corner of the plot page. The condition/heat treatment is listed at the very top of the header block and the remaining parameters are listed in two columns beneath the condition. The first column contains the parameters of product form and thickness, specimen type, specimen orientation, tensile yield strength, and tensile ultimate strength. The second column contains specimen thickness and width, initial crack length (a₀), stress corrosion cracking threshold value $K_{\mbox{\tiny Iscc}}$, and reference numbers. There are also three variations on these plots, that is, variations on product form and product thickness, tensile yield strength, and test temperature/environment. There are also some data sets in which condition/heat treatment for a given alloy is varied. In addition to the three basic plot variations noted, the sustained load crack growth rate data have two possible growth rate axes in order to accommodate the data. Both axes span six decades. The first axis ranges from 10⁻⁶ to 1 inches/hour, the second 10⁻⁴ to 10² inches/hour (English units). Both have maximum stress-intensity (K_{max}) values that range from 1 to 200 Ksi√in. The corresponding metric units for da/dt and K_{max}, i.e., mm/hour and MPa/m, respectively, are placed on the opposite side of the plot as their English counterparts.

Some of these data also have mean trend curves and mean trend tables associated with them. The mean trend tables are presented directly beneath the graphical presentation of the data in a manner similar to the fatigue crack growth rate data. The format of the table in Figure 1.13 is nearly identical to that of the fatigue crack growth rate data. Since all sustained crack growth data were received in reduced form, the LPR cannot be calculated. Therefore, LPR has been omitted

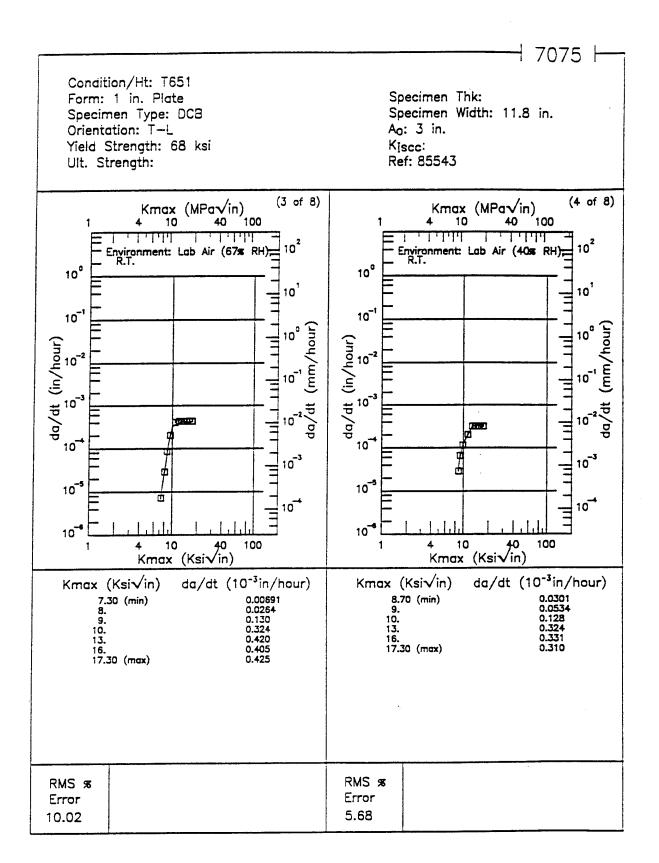


Figure 1.13 Sample Figure (pg 8-731): Sustained Load Growth Rate Plot and Mean Trend Fit

from the plot page. Due to the nature of the data, the values of the RMSPE are usually larger than those of the FCGR data. Additionally, mean trend curves representative of the data are not always created. For these cases, no mean trend curve or table is presented.

1.6.3 Stress Corrosion Cracking Threshold

Following the sustained load crack growth rate data is the tabular stress corrosion cracking threshold data. An example of this data format is presented in Figure 1.14, which is similar to the fracture toughness data format. The material, alloy and data type are listed in the table title. Condition/heat treatment, product form, product thickness, test temperature, specimen orientation, yield strength, and environment are listed in the table from left to right. Following these parameters are the specimen design, width and thickness as well as product thickness, crack length, K_Q fracture toughness, K_{Iscc} individual values, test times, dates and reference numbers. The data are sorted by alloy, condition/heat treatment, product form, test temperature, specimen orientation and environment.

The fracture toughness value K_Q indicates the level of crack toughness of the material. These values were obtained from threshold tests and are not valid plane-strain fracture toughness values. The K_Q values, however, should provide an engineer with an indication of stress-corrosion cracking sensitivity relative to fracture.

In the K_{Iscc} tabular data, the specimen design column and/or the K_{Iscc} column may be footnoted. An asterisk appearing in the specimen design column indicates that the specimen has been side-grooved along the path of the crack. A plus sign appearing in the K_{Iscc} column behind the individual K_{Iscc} values indicates that the crack length and/or specimen thickness were not greater than the required minimum value of $2.5(K_{Iscc}/\sigma_{ys})^2$.

K_{Irce} SUMMARY FOR ALLOY STEEL 18Ni(250)(MAR)

			1	Vield		Š	Specimen						Teat		
Condition/ Heat Treat	Prod Form	Temp (°F)	Spec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)	Thk (in)	Crack (in)	Ko (Ksivin)	Kırı (Ksivin)	Time (min)	Test Date	Reference
				252	Synth. Suaweter	CANT	1	1	1		72.6	49	30000	9961	65166
						CANT.	3	1	1.25	1.05	93	35	00009	1968	73829
Unspecified	a,	R.T.	i		<u> </u>	CANT.	0.6	1	1.25	0.17	68	21	00009	1968	73829
				529	Synth.	CANT.	-	1	1.25	0.35	78	37	00009	1968	73829
						CANT.	5	1	1.25	1.75	95	38	00009	1968	73829
								•		•••		36.5	•••	1969	74232
						CANT	8	1	1.25	i	88	35	ï	1970	78065
1650F 1.25hr WQ; 1525F 1.25hr WQ;	Δ,	R.T.	i	259	Synth.	CANT	-		1.25	1	78	87	1	1970	78065
900F 3hr AC						CANT	9	1	1.25	-	98	38	I	1970	78065
		I			3.5% NaCl	CNT	2	0.05	0.08	•••	:	110*	20000	1968	72283
900F 2hr AC	တ	R.T.		228	Dist. Water	CNT	2	0.05	0.08	i		110	30000	1968	72283
Age 900F 3hr	ď	R.T.	L-T	249	3.5% NaCl	NB	1.5	0.48	0.48	:	92	45		1971	84351
						CANT	0.5	0.375	0.5			60	Į	1971	80824
Aged 900F 3hr AC	ŀ	K.T.	L-S	:	3.5% NACI	CANT	0.482	0.375	0.5	i	i	31	1	1971	80824
TYS=250Ksi	Ь	R.T.	:	250	3.5% NaCl	CANT.	i	-	1	i	70	50	į	1972	83613
TYS=260Ksi	P	R.T.		260	3.6% NaCl	CANT	i	-	1	i	98	70	1	1972	83613

* specimen thickness does not meet minimum requirements of $2.5~(rac{K_{loo}}{\sigma_{rr}})^2$

* asterisk in specimen design column indicates that specimens are side-grooved

Sample Table (pg 3-66): Stress Corrosion Cracking Threshold Data by Alloy Figure 1.14

Greater than (>) and less than (<) signs before the $K_{\rm Iscc}$ value indicate that the actual value is either greater than or less than the value stated, respectively. Data containing these signs were considered to be informative since little data exists and so were included.

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CHAPTER 2 METHODS OF CALCULATIONS

2.0 OVERVIEW

This chapter briefly describes the methods used to calculate the damage tolerant properties reported in the Handbook. The properties reported for characterizing fracture resistance include:

- K_{Ic}, the plane-strain fracture toughness
- K, the critical plane-stress (or transitional) fracture toughness
- K_{App} , the apparent plane-stress fracture toughness
- K_R, the tearing resistance

and, the properties reported for characterizing subcritical crack growth resistance include:

- $\frac{da}{dN}$, the constant amplitude fatigue crack growth rate
- $\frac{da}{dt}$, the sustained-load crack growth rate
- K_{Iscc} , the threshold for sustained load cracking

Sections 2.1 through 2.7 describe these properties and the specific methods of calculations utilized to convert laboratory (specimen) data into the properties reported.

2.0.1 Data Review and Acceptance Criteria

Newly acquired data and data available from previous revisions of the Handbook were systematically reviewed and analyzed. The principal data acceptance criteria were based on criteria established by the American Society for Testing and Materials (ASTM); these criteria are embedded within ASTM standards for test methods and practices. Table 2.1 lists those standards used to provide criteria for plane-strain fracture toughness (K_{Ic}) data, for R-curve data, and for fatigue crack growth rate (da/dN) data. ASTM literature was also reviewed to establish criteria based on typical engineering practice for the other types of data collected and reported.

TABLE 2.1

APPLICABLE LIST OF STANDARDS FOUND IN

THE ASTM BOOK OF STANDARDS

ASTM STD	Title
E616-81	Standard Terminology Relating to Fracture Testing
E399-90	Test Method for Plane-Strain Fracture Toughness of Metallic Materials
E561-86	Practice for R-Curve Determination
E647-91	Test Method for Constant-Load-Amplitude Fatigue Crack Growth Rates Above 10 ⁻⁸ m/Cycle

Newly acquired data was substantially easier to process than the data available from previous revisions since the data suppliers screened their data according to ASTM criteria before it was released to the data processing organization (UDRI). Also, when questions concerning newly acquired data developed, the suppliers could be called and the questions resolved.

The final step in the review process was the determination of whether the data were a "true" representation of the behavior they described. This step was implemented for both newly acquired data as well as for the available Handbook data in order to eliminate suspect data through subjective criteria. Unfortunately, it is not possible to detail the subjective criteria that were employed to exclude questionable data. It can be stated that the principal mode of operation here was by way of comparison between behaviors that were expected to be somewhat similar.

2.0.2 Fracture Mechanics Basis

The damage tolerant data reported in this Handbook utilize the technology of linear elastic fracture mechanics. This technology is widely applied throughout the aerospace industry to relate structural calculations for cracked structures to material behavior in the presence of cracks. In essence, fracture mechanics provides a structural parameter, the stress-intensity factor (symbol K) which characterizes the magnitude of stresses and strains in the crack tip region of essentially elastic structures. It was postulated that the stress-intensity factor represents a similitude parameter that describes crack tip behavior under various loading conditions (monotonically increasing load, fatigue loading, etc.); the hypothesis has been verified for a wide number of materials, loading conditions, and failure type mechanisms. For a more thorough review of linear elastic fracture mechanics and its applications to the aerospace industry, see AFWAL-TR-82-3073, USAF Damage Tolerant Design Handbook: Guidelines for the Analysis and Design of Damage Tolerant Aircraft Structures.

Currently, there are developments that are extending the technology of fracture mechanics to aid in the solution of crack problems for which the assumptions of linear elastic fracture mechanics are invalid. This technology is referred to as nonlinear fracture mechanics and its similitude parameter is the J-integral (J), or alternately the crack tip opening displacement (δ). To date, nonlinear fracture mechanics has been successfully utilized to characterize tearing type fractures and fractures occurring in the presence of large-scale yielding. Some evidence has been presented suggesting that J may provide a similitude parameter for non-monotonically increasing type loadings, i.e., for fatigue loadings; but, questions still exist here. It is expected that subsequent revisions of this Handbook will include nonlinear fracture mechanics type data such as J_{Ic} , a plane-strain fracture toughness property, and J_{R} -curves, (tearing resistance curves).

2.0.3 Test Specimen Geometries

As described above, the stress-intensity factor provides a parameter that can be used to establish similitude between two cracked structures. This means that if the stress intensity factor in structure A equals the stress-intensity factor in structure B and if other conditions (loading, material, environment, etc.) are the same, then the cracks in both structures will behave the same way. This concept provides the justification for conducting material behavior studies on small laboratory test specimens (coupons) which contain cracks. If the resistance to cracking in the laboratory can be optimized by a choice of material, then improved resistance can also be obtained for structural hardware (given that the material can be fabricated into the hardware without processing degradation taking place).

The types of test specimen geometries that have been employed to generate damage tolerance (fracture mechanics) type data for this Handbook are summarized in Table 2.2. Table 2.2 also guides the reader to individual figures (Figures 2.1 through 2.14) which describe the geometries associated with individual specimen names and symbols.

TABLE 2.2

CORRELATION LISTING OF TEST SPECIMEN SYMBOL,
TEST SPECIMEN GEOMETRY, AND REFERENCE FIGURE NUMBER

Symbol	Test Specimen	Geometry Described in Figure Number
CCP	Center Crack Panel	2.1
CT	Compact (Tension)	2.2
NB	Three Point Notched Bend	2.3
4-NB	Four Point Notched Bend	2.4
CANT	Cantilever Beam	2.5
WOL	Wedge Opening Load	2.6
BWOL	Bolt Loaded WOL	2.7
SENT	Single Edge Notch Tension	2.8
PTSC	Part-Through Surface Crack	2.9
KB-BAR	K _B BAR	2.10
DCB	Double Cantilever Beam	2.11
BDCB	Bolt Loaded DCB	2.12
TDCB	Tapered Double Cantilever Beam	2.13
CNT	Center Notch Tension	2.14

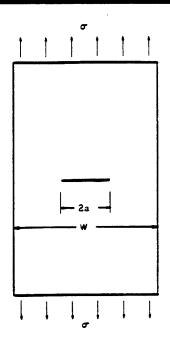


Figure 2.1 Center Cracked Panel (CCP) Specimen.

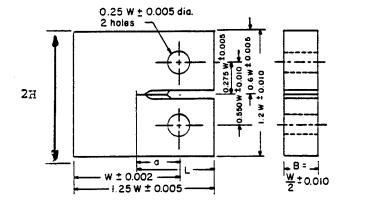


Figure 2.2 Compact Tension (CT) Specimen.

 $\frac{H}{W} = 0.6$

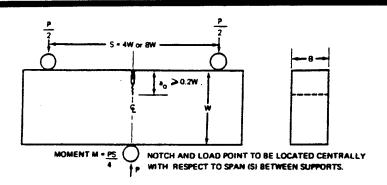
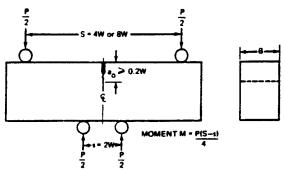


Figure 2.3 Three Point Notched Bend (NB) Specimen.



NOTCH TO BE LOCATED CENTRALLY WITH RESPECT TO MAJOR (S) AND MINOR (s) SPAN

Figure 2.4 Four Point Notched Bend (4-NB) Specimen.

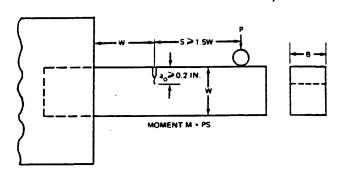


Figure 2.5 Cantilever Beam (CANT) Specimen.

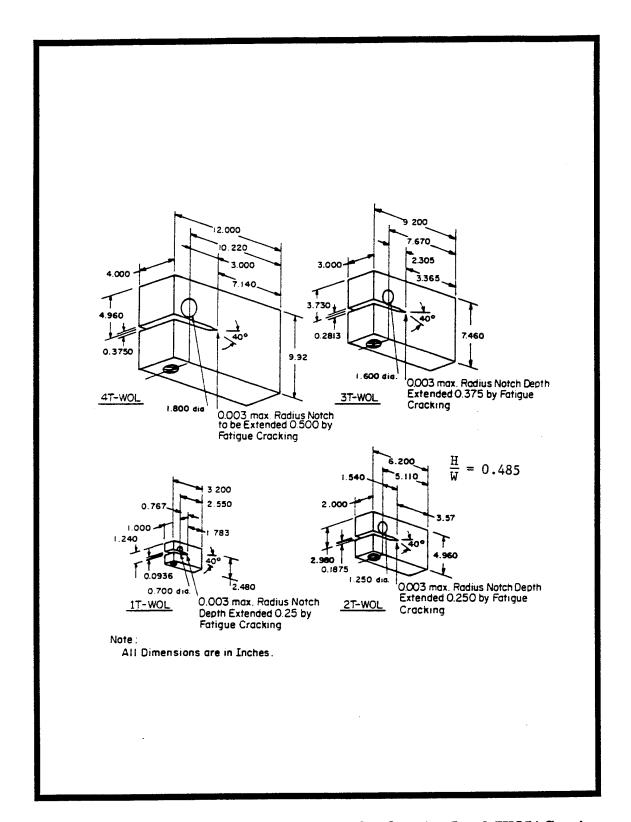


Figure 2.6 Dimensions of Several T Type Wedge Opening Load (WOL) Specimens.

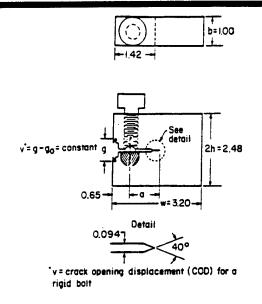


Figure 2.7 Modified 1-T WOL (BWOL) Specimen used to Determine $K_{\mbox{\tiny Iscc}}$ by Bolt Loading.

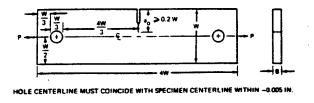


Figure 2.8 Single Edge Notch Tensile (SENT) Specimen.

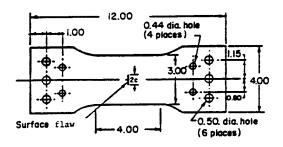
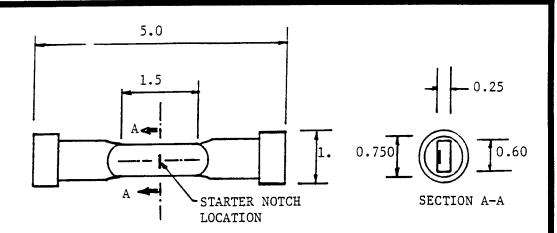
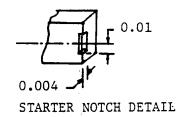


Figure 2.9 Typical Design for Part-Through-Surface-Crack (PTSC) Specimen.



ALL DIMENSIONS IN INCHES



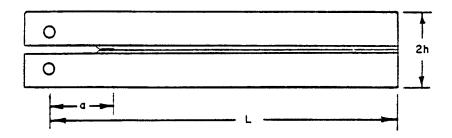


Figure 2.11 Double Cantilever Beam (DCB) Specimen with Side Grooves.

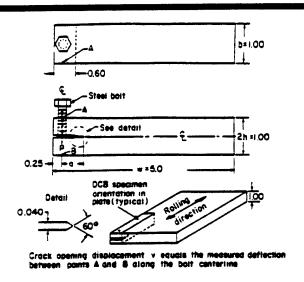


Figure 2.12 Bolt-Loaded Double Cantilever Beam (BDCB) Specimen.

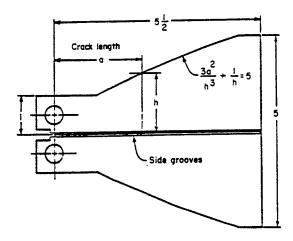


Figure 2.13 Typical Tapered Double Cantilever Beam (TDCB) Specimen with Side Grooves.

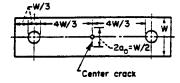


Figure 2.14 Center-Notched Tensile (CNT) Specimen.

To relate the crack type data collected in a cracked test specimen to other cracked structures, it is necessary to have a description of the stress-intensity factor (K) as a function of crack length (a) for the test specimen geometry. A great deal of attention has been given to generating accurate stress-intensity factor equations for laboratory test specimen geometries, due to their importance to standard methods of test and to reporting data. The stress-intensity factor equations are typically presented in either of the following two forms:

$$K = \sigma \sqrt{\pi a} \cdot \beta \tag{2.1}$$

where

 $\sigma = \text{remote stress (load } \div \text{ area)}$

a =crack length measure

 β = function of crack length and global geometry

or

$$K = \frac{P}{B\sqrt{W}} \quad Y \tag{2.2}$$

where

P = load

B =thickness of specimen

W =width of specimen

Y = function of crack length (a) and global geometry

Equation 2.1 is used when the loading is applied remotely from the crack, whereas Equation 2.2 is more typically used for point loading or localized loading conditions. One should note that K is a linear function of loading (σ in Equation 2.1 and P in Equation 2.2) and that the loading and geometric components of the equations are independent of each other. Thus, if one wishes to describe a stress-intensity factor relationship for a given geometry, they might formulate the equations in the following forms:

$$\frac{K}{\sigma} = \sqrt{\pi a} \cdot \beta \tag{2.3}$$

or

$$\frac{K}{P} = Y \tag{2.4}$$

Equations 2.3 and 2.4 are referred to as stress-intensity factor coefficients; the right hand side of these equations only describes the effect of the crack in the given geometry.

Table 2.3 provides a listing of stress-intensity factor coefficients which were used to generate data for this Handbook. Each equation is given a stress-intensity factor equation number, e.g., SIF.7 refers to the stress-intensity factor coefficient for the WOL (Wedge Opening Load) specimen geometry illustrated in Figure 2.6. Also note that Table 2.3 has a remarks section which describes the conditions under which individual equations were used.

2.1 PLANE-STRAIN FRACTURE TOUGHNESS (K_{Ic})

The plane-strain fracture toughness $(K_{\rm Ic})$ property was initially established to characterize the fracture resistance of materials that exhibited rather abrupt fractures in the presence of cracks. Early observations showed that thickness had a pronounced effect on the critical levels of stress-intensity factor associated with fracture; a schematic illustrating this behavior is presented in Figure 2.15. As noted in the schematic, for thicknesses greater than the experimentally determined lower-bound, the critical stress-intensity factor level was found to be relatively constant.

The reasons for the independence of toughness with further increases in thickness were related to the amount and type of yielding which could occur at the crack tip under what has been referred to as plane-strain conditions. Because the thickness-independent toughness property was useful for comparing a large variety of metals for fracture resistance, ASTM (American Society for Testing and Materials)

TABLE 2.3

STRESS-INTENSITY FACTOR COEFFICIENTS FOR TEST SPECIMEN GEOMETRIES USED TO GENERATE DAMAGE TOLERANT DATA	t Specimen Stress-Intensity Factor Equation Coefficient Number Remarks	CCP $\frac{K}{\sigma} = \sqrt{\pi a} \cdot (\sec \pi \alpha)^{1/2}$ SIF.1 This equation was used whenever K was calculated for the CCP specimen.	CT $\frac{K}{\left(\frac{P}{BW^{1/2}}\right)} = \frac{(2+\alpha)}{(1-\alpha)^{3/2}} \cdot \begin{bmatrix} 0.866 + 4.64\alpha - 13.32\alpha^2 \\ +14.72\alpha^3 - 5.6\alpha^4 \end{bmatrix}$ SIF.2 This equation was used whenever K was calculated for the CT specimen; the equation is considered to be accurate for $a/W > 0.2$.	CT $\frac{K}{\left(\frac{P}{BW^{1/2}}\right)} = \alpha^{1/2} \left[\frac{29.6 - 185.5\alpha + 655.7\alpha^2}{-1017\alpha^3 + 638.9\alpha^4}\right]$ SIF.3 This equation was only used to calculate K for data directly incorporated into pre-1983 $\alpha = a/W$ $\frac{H}{W} = 0.600$	NB $\frac{K}{\left(\frac{P}{BW^{3/2}}\right)} = S3\alpha^{1/2} \left[\frac{1.99 - \alpha(1-\alpha)(2.15 - 3.93\alpha + 2.7\alpha^2)}{2(1+2\alpha)(1-\alpha)^{3/2}}\right]$ SIF.4 This equation was used to process all new and pre-1993 revision data for NB specimens. $\alpha = a / W$ S = span length
<u> </u>	Test Specimen Geometry	CCP (See Figure 2.1)	CT (See Figure 2.2)	CT (See Figure 2.2)	NB (3 PT BEND) (See Figure 2.3)

TABLE 2.3 (Cont'd)

STRESS-INTENSITY FACTOR COEFFICIENTS FOR TEST SPECIMEN GEOMETRIES USED TO GENERATE DAMAGE TOLERANT DATA

Equation Remarks	No new data were processed from 4-NB specimens. Data incorporated into pre-1983 handbook revisions utilized this equation. s/W must be greater than 2.	SIF.6 No new data were processed from CANT specimens. Data incorporated into pre-1983 handbook revisions utilized this equation.	This equation was used to process all new and pre-1983 revision data for WOL specimens with H/W=0.485. WOL specimens with H/W=0.6 utilized equation SIF.2.	SIF.8 This equation was used to calculate stress-intensity factors for both WOL and BWOL in pre-1983 revisions. No new BWOL raw data were received for processing.
	$\frac{K}{\left(\frac{6M}{BW^{3/2}}\right)} = \alpha^{1/2} \left[\frac{1.99 - 2.47\alpha + 12.97\alpha^2}{-23.17\alpha^3 + 24.80\alpha^4} \right]$ SI $\alpha = a/W$ $M = P(S - s)/4, \text{ moment}$ $S, s = \text{major and minor span}$	$\frac{K}{\left(\frac{M}{BW^{3/2}}\right)} = 4.12 \left[(1-\alpha)^{1/3} - (1-\alpha)^3 \right]^{1/2}$ SI $\alpha = a/W$ $M = P \cdot S$, moment	$\frac{K}{t^{W/12}} = \frac{(2+\alpha)}{(1-\alpha)^{3/2}} \left[\frac{0.8072 + 8.858\alpha - 30.23\alpha^2}{+41.088\alpha^3 - 24.15\alpha^4 + 4.951\alpha^5} \right]$ $= a / W$ $= 0.485$	$\frac{K}{\left(\frac{P}{BW^{1/2}}\right)} = \alpha^{3/2} \begin{bmatrix} 30.96 - 195.8\alpha + 730.6\alpha^2 \\ -1186.3\alpha^3 + 754.6\alpha^4 \end{bmatrix}$ $\alpha = a / W$ $B = \sqrt{B \cdot B_N}$ $B_N = \text{Net Thickness at Side Groove}$
Test Specimen Geometry	4-NB (4 PT BEND) (See Figure 2.4)	CANT (See Figure 2.5)	WOL $ \frac{\left(\frac{-}{\overline{L}}\right)}{\left(\frac{-}{\overline{L}}\right)} $ (See Figure 2.6) $ \frac{\alpha}{\overline{W}} $	BWOL (See Figure 2.7)

TABLE 2.3 (Cont'd)

STRESS-INTENSITY FACTOR COEFFICIENTS FOR TEST SPECIMEN GEOMETRIES USED TO GENERATE DAMAGE TOLERANT DATA

Equation Remarks	SIF.12 This specimen was used for generating da/dN, da/dt, and K _{isc} data in pre-1983 revisions. The function Y was specified for given H/W. Data collected with DCB specimens were not reprocessed and no new data were received.	SIF.13 This equation was used for K _{lscc} testing. Data previously calculated using this equation were directly incorporated into the 1993 revision; no new data were received.	SIF.14 This equation was used by McDonnell Aircraft Company to reduce data referenced in Ref. No. 84360 (Equation is based on Plane- Strain Assumptions). Data were incorporated without change into the 1993 revision and no new data were received.
Stress-Intensity Factor Coefficient	$\frac{K}{\left(\frac{P}{BW^{1/2}}\right)} = \alpha^{1/2} Y$ $\alpha = a / W$ $Y = Y(a / W, H / W)$ $B = \sqrt{B \cdot B_N}$ $B_N = \text{Net Thickness at Side Groove}$	$K = \frac{VEh \left[3h(a+0.6h)^2 + h^3 \right]^{1/2}}{4 \left[(a+0.6h)^3 + h^2 a \right]}$ $V = \text{displacement}$ $h = \text{height}$ $E = \text{Elastic Modulus}$	$\frac{K}{P} = \left[\frac{E\left(\frac{dC}{da}\right)}{2B_N(1-v^2)} \right]^{1/2}$ where $\frac{dC}{da} = \left[3.63 - 0.925 \left(0.8 - \frac{B_N}{B} \right) \right] \cdot 10^{-6}$ $= \text{Compliance Derivative } (Ib^{-1})$ $B_N = \text{Net Thickness at Side Groove}$ $E = \text{Elastic Modulus}$
Test Specimen Geometry	DCB (See Figure 2.11)	BDCB (See Figure 2.12)	TDCB (See Figure 2.13)

TABLE 2.3 (Cont'd)

STRESS-INTENSITY FACTOR COEFFICIENTS FOR TEST SPECIMEN GEOMETRIES USED TO GENERATE DAMAGE TOLERANT DATA

Test Specimen Geometry	Stress-Intensity Factor Coefficient	Equation Number	Remarks
SENT (See Figure 2.8)	$\frac{K}{\left(\frac{P}{WB}\right)} = \sqrt{\pi a} \left(1.12 - 0.23\alpha + 10.55\alpha^2 - 21.71\alpha^3 + 30.38\alpha^4\right)$ $\alpha = a / W$	SIF.9	This equation was used to process all new and pre-1993 revision data for SENT specimens.
PTSC (See Figure 2.9)	$\frac{K}{\sigma} = 1.1 \left[\frac{\pi a}{\overline{Q}} \right]^{1/2}$ where for $(a/c) \le 1$; $Q = 1.0 + 1.464 \left(\frac{a}{c} \right)^{1.65}$ and for $(a/c) > 1$; $Q = 1.0 + 1.464 \left(\frac{c}{a} \right)^{165}$ $a = depth$ $2c = surface length$	SIF.10	This equation was used to process all new and pre-1993 revision data for PTSC specimens.
KB BAR (See Figure 2.10)	This equation was used by Aircraft Engine Group of General Electric Company. Closely approximates Newman and Raju Solution presented in AFWAL-TR-82-3073.	SIF.11	This equation was used for da/dN testing. Previously existing data were directly incorporated into the 1993 revision for this geometry; no new data were received.

TABLE 2.3 (Concluded)

STRESS-INTENSITY FACTOR COEFFICIENTS FOR TEST SPECIMEN GEOMETRIES USED TO GENERATE DAMAGE TOLERANT DATA

TEST SPECIMEN GEOMETRY	STRESS-INTENSITY FACTOR COEFFICIENT	EQUATION NUMBER	REMARKS
TDCB (See Figure 2.13)	$\frac{K}{P} = \left[\frac{E}{2B} \frac{dC}{da} \right]^{1/2}$ where $\frac{dC}{da} = \text{constant}$ $E = \text{Elastic Modulus}$ $B = \sqrt{B \cdot B_N}$ $B_N = \text{Net Thickness at Side Groove}$	SIF.15	No new data were processed from TDCB specimens. Data incorpo- rated into pre-1983 handbook revisions utilized this equation.
CNT (See Figure 2.14)	$\frac{K}{\sigma} = \sqrt{\pi a} \cdot [1 - 0.2\alpha + 4\alpha^2]$ $\alpha = a / W$ SIF.16 is comparable to SIF.1 For $0 \le \alpha \le 0.3$	SIF.16	No new data were processed from CNT specimens. Data (Kisce) for sheet materials incorporated into pre-1983 handbook revisions utilized this equation.

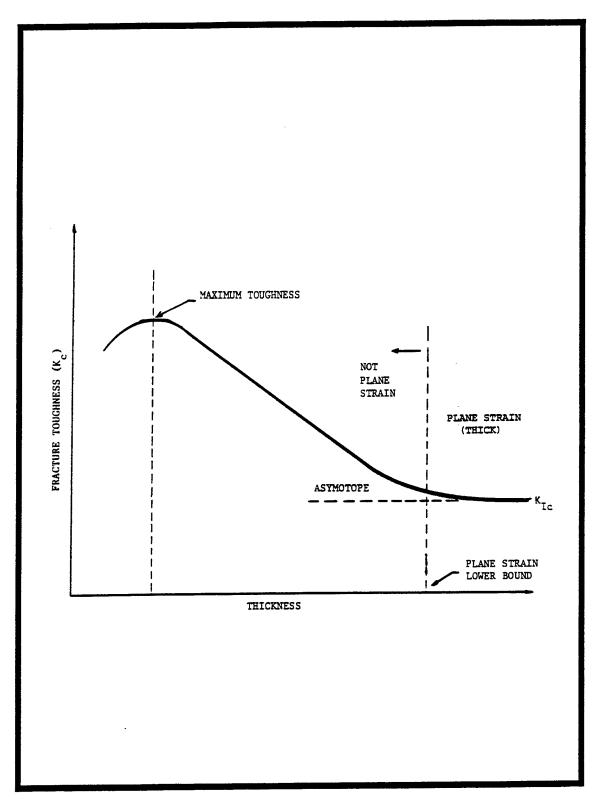


Figure 2.15 Fracture Toughness Behavior as a Function of Thickness.

embarked on a standardization effort that eventually resulted in the ASTM Standard Test Method for plane-strain fracture toughness of metallic materials, i.e., in the ASTM Standard E399.

The ASTM Standard E399 is the current procedure for determining critical plane-strain stress intensity factors ($K_{\rm Ic}$ values) for high-strength alloys. From the method of test, "The property $K_{\rm Ic}$ determined by this method characterizes the resistance of a material to fracture in a neutral environment in the presence of a sharp crack under severe tensile constraint, such that the state of stress near the crack front approaches tritensile plane-strain, and the crack-tip plastic region is small compared with the crack size and specimen dimensions in the constraint direction."

Assuming that plane-strain conditions are approximated when unstable cracking occurs at the crack front during a $K_{\rm Ic}$ test, the critical stress intensity factor calculated from the test data is characteristic of the material of the specimen at the testing temperature and for the specific crack growth direction. Since the properties vary somewhat from specimen to specimen in one plate or in one heat, and from heat to heat of a given alloy type with the same heat treatment, the measured $K_{\rm Ic}$ values for several heats will show some degree of scattering in the data. Usually, the extent of scattering is greater than that for replicate tensile tests. For this reason, a relatively large number of data points would be required to establish minimum design values for any of the fracture mechanics parameters. To minimize the scatter in data, maximum effort is required in controlling the processing, preparation, and testing of each specimen. These precautions are discussed in the Method of Test (ASTM E399).

The ASTM E399 procedure indicates that calculated K values be designated K_Q , which is a provisional value. When the validity of the results is established by the procedures designated in the Method of Test, then the K_Q value can be identified as a valid K_{Ic} value. Some of the primary criteria for judging the validity of K_{Ic} values are based on crack length and specimen thickness conditions. The test data

must demonstrate that sufficient constraint was available to justify the plane strain assumptions. The other requirements for validity of the $K_{\rm Ic}$ values involve measurements of the length of the fatigue crack, contour of the crack front, out-of-plane deviation of the fatigue crack, maximum stress intensity resulting from the fatigue cracking load, and details of the load-deformation curves.

All newly acquired plane-strain fracture toughness (K_{Ic}) data incorporated in the 1993 Handbook revision were generated using the ASTM Standard E399. All suppliers of new K_{Ic} data provided only E399 validated K_{Ic} data in a reduced format which facilitated direct incorporation into the Handbook. Data incorporated in earlier revisions for the most part utilized ASTM Standard E399 or the predecessor tentative method for plane-strain fracture toughness testing; and after review, these data were also included into the 1993 revision. In some instances, nonstandard specimens were used for generating critical plane-strain stress-intensity factors in the earlier revisions. Some of these data were incorporated in the 1993 revision on the basis that a reasonable procedure was used and that corresponding data from other sources were limited for the alloys concerned. All data were checked against the criteria for specimen thickness (B) and crack length (a), i.e., B, a > 2.5 $(K_{Ic}/\sigma_{ys})^2$ where σ_{ys} is the tensile yield strength.

2.2 CRITICAL PLANE STRESS FRACTURE TOUGHNESS

2.2.1 Plane Stress and Transitional Fracture Toughness

The critical level of the stress-intensity factor for non-plane-strain conditions is normally described with the symbol K_c, see Figure 2.15, and is referred to as the plane-stress or transitional fracture toughness. Generally, plane-stress fracture-toughness testing is representative only of through-the-thickness cracks in relatively thin section materials. For a given material thickness, this configuration has the least lateral restraint on the crack front and, hence, approaches most closely the ideal plane-stress stress state conditions at the crack tip. As the material

thickness increases, transitional stress state behavior is introduced by the restraint of additional material along the crack front. In contrast to that in plane-strain fracture-toughness testing, the characterization of fracture toughness in the plane-stress and transitional-stress states is complicated by the degree to which crack tip plasticity and associated stable crack extension are manifested prior to fracture. Although an explicit test method for this mode of toughness has not been formulated, there are a number of useful experimental guidelines which have been developed.

As background information, the nature of plane-stress and transitional fracture toughness is described here in terms of its deviation from that of the plane-strain stress state. Current procedures for this mode of testing and the associated analytical formulations of toughness then are presented.

The difficulties that beset the characterization of plane stress and transitional fracture are not only of a theoretical nature, but also of a practical experimental nature. Basic questions on the nature of plasticity, crack extension, and crack instability, as well as the wide variation in experimental techniques among laboratories all contribute to variability in the resulting fracture toughness evaluations. However, in spite of these difficulties, surprisingly consistent characterizations of fracture behavior can be obtained.

During the fracture test of a structural material in a plane-stress or transitional-stress state, stable extension of the initial fatigue precrack may occur as the load increases. This behavior is illustrated schematically in the crack growth curve of Figure 2.16. Depending on the material, stable crack extension may amount to 30 percent or more of the initial precrack length.

Once it is understood that fracture under these conditions is not an abrupt instability instantaneously associated with a small increment of crack extension, it must also be recognized that a single toughness parameter is not sufficient to characterize this complex behavior. In fact, the concept of crack growth resistance

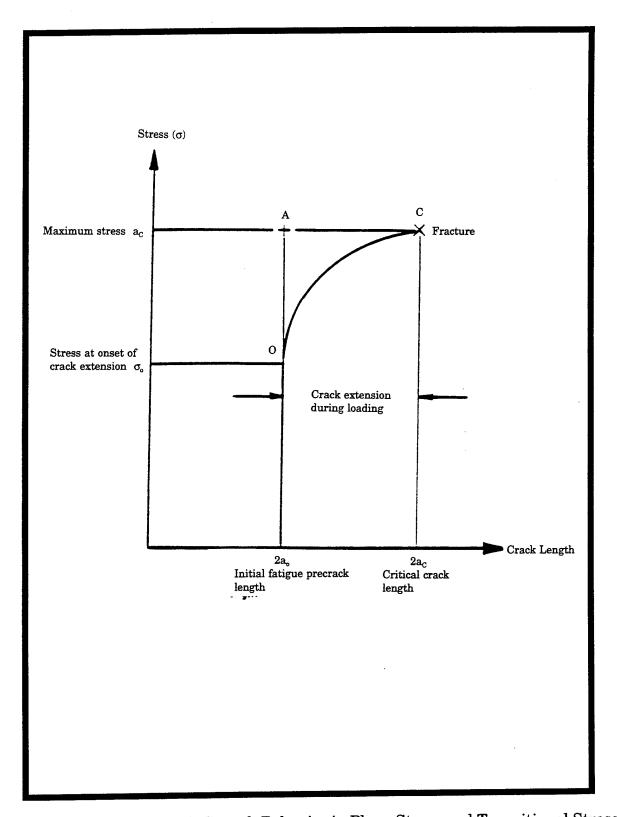


Figure 2.16 Typical Crack Growth Behavior in Plane Stress and Transitional Stress States.

curves (see Section 2.4) is an outgrowth of these observations and best describes the material behavior. However, as a means of characterizing fracture behavior in planestress and transitional stress state, engineers have traditionally utilized abrupt fracture concepts, i.e., have used critical stress-intensity factor levels, to describe various events associated with the observed behavior.

2.2.2 Plane Stress and Transitional Fracture Toughness Testing

The procedures associated with testing thin-section center-cracked tension panels differ from those associated with plane-strain fracture toughness testing only in the additional emphasis and refinement that is directed to monitoring the slow, stable tear portion of the fracture process.

The general testing configuration is illustrated schematically in Figure 2.17. The specimen with an initial fatigue precrack, $2a_o$, is loaded slowly under load or stroke control. The onset and extension of crack growth under increasing load is usually monitored photographically, visually, or by means of compliance gage calibration until fracture occurs.

Although, as previously mentioned, more attention is currently being directed to monitoring the detail stress and crack length dimensions during the slow tear process, the majority of available test data is limited to a record of σ_o or $2a_o$ or σ_c , and $2a_c$, as indicated in Figure 2.16. It is this information which is compiled and analyzed in this Handbook.

2.2.3 Critical Stress-Intensity Factor (K_c)

There are two clearly identified points that can be noted on the crack growth resistance curve shown in Figure 2.16, i.e., points O and C which are associ-

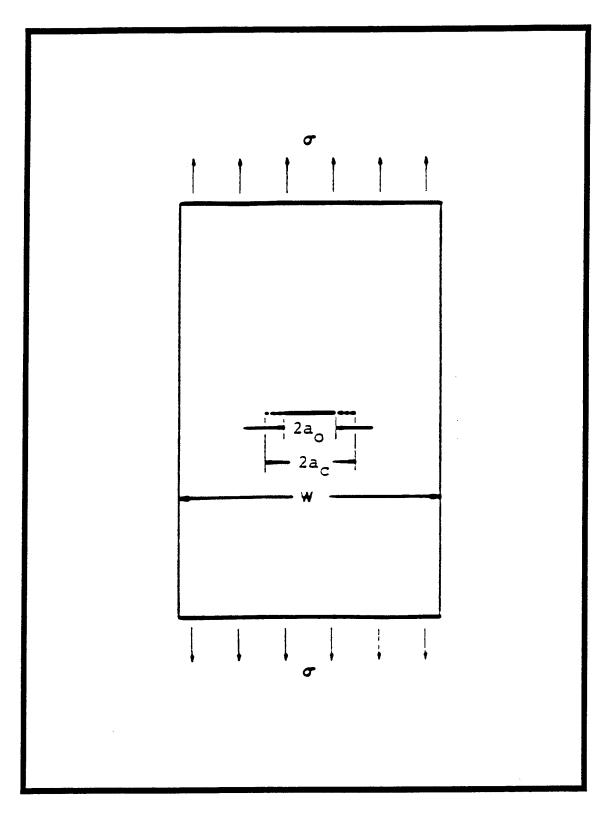


Figure 2.17 Thin-Section, Center-Cracked Tension Panel Configuration.

ated with the onset of tearing and critical conditions, respectively. Using a linear elastic fracture mechanics analysis, these two structural conditions can be formulated as

$$K_{ONSET} = \sigma_o \sqrt{\pi \alpha_o} \left[Sec \frac{\pi \alpha_o}{W} \right]^{\frac{1}{2}}$$
 (2.5)

and

$$K_c = \sigma_C \sqrt{\pi a_c} \left(Sec \frac{\pi a_c}{W} \right)^{\frac{1}{2}}$$
 (2.6)

using the stress-intensity factor information given in Table 2.3, i.e., Equation SIF.1. As requested by industry engineers, available test information (σ_o , $2a_o$, σ_c , $2a_c$) were reported in the plane stress and transitional fracture toughness tables along with a calculation of the critical fracture toughness level based on Equation 2.6. While stress and crack length information were sometimes available for a calculation of the onset fracture toughness (Equation 2.5), insufficient space in the table precluded reporting this toughness.

Plane stress and transitional fracture behavior absorb much more energy than plane-strain behavior due to the lack of thickness constraint on crack tip plasticity, and the assumptions of linear elastic fracture mechanics are violated. The in-plane geometric constraint on crack tip plasticity is required to ensure that gross plasticity is not the controlling mechanisms of fracture. Extensive study has indicated that the condition for CCP specimen instability for ductile materials is given by a net section stress criteria and not by a fracture (crack) controlled instability criteria. While the fracture toughness values for all plane strain type tests are reported, those values calculated for stress conditions where the net section stress ($\sigma_{\rm net} = {\rm Load/B(W-2a_c)}$) exceeds 80 percent of the tensile yield strength are marked with an asterisk. Values so marked are not utilized in any mean or standard deviation calculations summarizing plane-stress fracture critical properties.

2.3 THE APPARENT FRACTURE TOUGHNESS

The apparent fracture toughness (K_{App}) is a plane stress and transitional fracture toughness property that is sometimes utilized as a lower bound on the critical fracture toughness. Its initial purpose was to preclude measurements of the tearing process observed during fracture tests of CCP specimens. As noted in Figures 2.16 and 2.17, the initial crack length $(2a_o)$ extends during the loading to the critical crack length $(2a_c)$. The two simplest measurements to make in such a fracture test are those of the initial crack length $(2a_o)$ and critical (maximum) stress at failure (σ_c) . Thus, for simplicity, a K_{App} fracture toughness calculation was made using

$$K_{App} = \sigma_c \sqrt{\pi a_o} \cdot \left(\sec \frac{\pi a_o}{W} \right)^{\frac{1}{2}}$$
 (2.7)

Equation 2.7 represents the stress-intensity factor corresponding to the stress and crack length condition at point "A" in Figure 2.16. It can be noted by comparing Equations 2.6 and 2.7 that K_{App} will always be less than or equal to K_c since $a_o \le a_c$. Also, K_{App} will always be greater than or equal to K_{ONSET} since $\sigma_o \le \sigma_c$. A comparison of the apparent fracture toughness with the onset and critical fracture toughness is shown in Figure 2.18 for a wide CCP specimen. When the net section stress $(\sigma_{net} = Load/B(W-2a_o))$ exceeds 80 percent of the tensile yield strength, the K_{App} values are marked with an asterisk. Values so marked are not utilized in any mean or standard deviation calculations summarizing plane-stress apparent fracture toughness properties.

2.4 R-CURVE (K_R VERSUS Δa_{eff})

The resistance curve (or R-curve) provides a complete description of the tearing fracture behavior illustrated in Figure 2.16. R-curves characterize the resistance to fracture of materials during incremental slow-stable crack extension and result from growth of the plastic zone as the crack extends. ASTM formalized the collection and

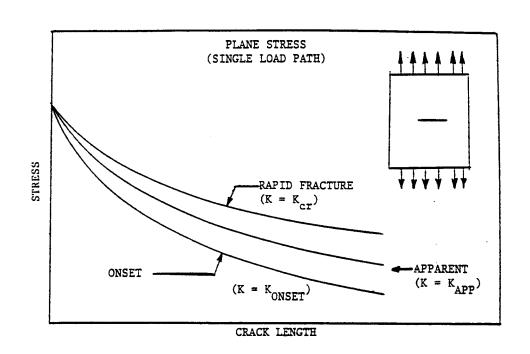


Figure 2.18 Description of the Three Fracture Toughness Criteria that are Utilized to Estimate Residual Strength Under Tearing Fracture Conditions.

reporting of such curves through ASTM Standard E561, covering the standard practice for R-Curve Determination. As stated by ASTM E561, R-curves provide "a record of the toughness development as a crack is driven stably under increasing applied K. They are dependent upon thickness, temperature, and strain rate."

The value of K_R (toughness) is calculated using standard stress-intensity factor equations evaluated with the instantaneous values of applied stress (σ) and crack length (a), as the crack extends. To account for the effects of plasticity, the measured crack length is enhanced with a plastic zone correction, and an effective crack length (a_{eff}) is actually used in the calculation of K_R . For example, when a CCP specimen is used to collect tearing resistance data, the K_R is calculated based on the standard stress-intensity factor equation (SIF.1) given in Table 2.3.

$$K_R = \sigma \sqrt{\pi a_{eff}} \cdot \left(Sec \frac{\pi a_{eff}}{W} \right)^{\frac{1}{2}}$$
 (2.8)

where σ and a_{eff} are the current stress and effective crack length measurements in the test. The effective crack length for optical measurements is calculated from

$$a_{eff} = a + r_{y} \tag{2.9}$$

where a is the optically measured crack length and $\boldsymbol{r}_{\boldsymbol{y}}$, calculated as

$$r_{y} = \frac{1}{2\pi} \left(\frac{K}{\sigma_{ys}} \right)^{2} \tag{2.10}$$

is the plastic zone size for the current applied stress and crack length. If the crack length is automatically monitored by compliance techniques, then the effective crack length is automatically obtained using the two compliance equations presented in ASTM E561.

The K_R value calculated from Equation 2.8 can be described as a function of the increment of physical crack extension ($\Delta a = a - a_o$, $a_o = \text{initial crack length}$) or as suggested by ASTM 561 as a function of the increment of effective crack length ($\Delta a_{\text{eff}} = (a + r_y) - a_o$). The functions K_R versus Δa and K_R versus Δa_{eff} are referred to as R-curves (or resistance curves). Data presented in this Handbook correspond to the use of the ASTM E561 definition of R-curves, i.e., K_R is presented as a function of Δa_{eff} .

All new and existing R-curve data were validated by ensuring that the remaining specimen ligament in the plane of the crack was predominantely elastic. For CCP specimens, ASTM Standard E561 requires the net section stress based on the physical crack size be less than the yield strength of the material, or

$$\sigma_{net} < \sigma_{ys}$$
 ; $\sigma_{net} = \frac{P_{cr}}{B(W-2a)}$ (2.11)

For compact tension (CT) specimens, the validity criteria is given by

$$W-a \ge \frac{4}{\pi} \left(\frac{K_{\text{max}}}{\sigma_{ys}} \right)^2 \tag{2.12}$$

where K_{max} is calculated using the physical crack size in conjunction with equation SIF.2 in Table 2.3.

The majority of R-curve data available for the Handbook were obtained using a compliance based technique for measuring the crack length. The compliance based technique provides a direct measure of the effective crack length, and therefore does not require use of Equations 2.9 and 2.10 to estimate the plastic zone size correction. Therefore, when a compliance based measurement technique is used, only the effective crack length, effective K_R , and $\Delta a_{\rm eff}$ are reported. As a result, the validity criteria given by Equations 2.11 and 2.12 were checked using the effective crack length for those data obtained by a compliance based technique. In some instances,

this resulted in the last few data points of a particular data set to not meet the criteria given by Equation 2.12. However, previous experience has shown that the effect of using $\Delta a_{\rm eff}$ in Equation 2.12 may be such that the test in question may appear to be invalid, when in reality it is not. Based on this and the fact that the tests in question were completed in accordance with ASTM Standard E561, these R-curves, identified by an asterisk, are included in the Handbook.

One of the fundamental hypotheses behind the application of R-curves to the prediction of tearing type fractures in thin structures and in structures fabricated from ductile materials is that the R-curve (material tearing resistance) is independent of crack length for a given geometry and is independent of geometry and external loading. As long as the structure matches the monotonically increasing stress-intensity factor conditions given by the R-curve, the structure will exhibit the same tearing resistance experienced in the laboratory test specimen. The Damage Tolerant Guidelines Handbook (AFWAL-TR-82-3073) describes how the R-curve can be applied to the calculation of critical stress levels in structures.

2.5 FATIGUE CRACK GROWTH RATE

2.5.1 Fatigue Crack Growth Behavior

Under some loading conditions or environmental conditions, cracks can grow at load levels well below that required to cause fracture. As the crack continues to grow, conditions become more favorable for fracture, and eventually under the applied loading fracture does occur. This process whereby cracks are observed to grow at subcritical load levels is referred to as subcritical crack growth. Illustrated in Figure 2.19 is a fatigue crack growth curve, which shows the type of behavior typically observed during a specific subcritical crack growth process; in this case, damage is done to the material by cyclic (or fatigue) loading. This section addresses properties used to measure fatigue crack growth behavior and Sections 2.6 and 2.7 address properties used to characterize sustained load cracking in an environment.

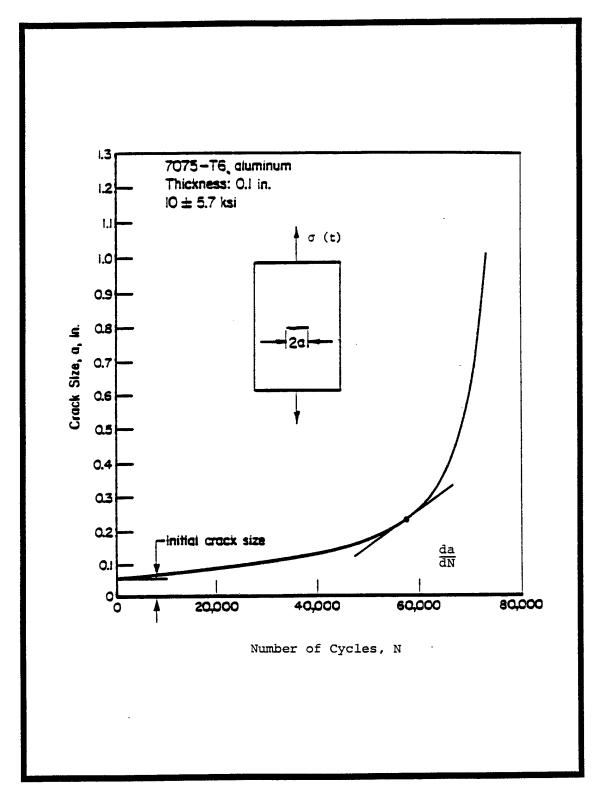


Figure 2.19 Typical Crack Growth-Life Curve.

The objective of fatigue crack growth testing is to determine the rates at which subcritical flaws propagate under cyclic loadings prior to reaching a size critical for fracture. These rates are determined from measurements of the crack extension occurring over an increment of cyclic loading. Typically, these measurements are made by monitoring crack extension optically on the specimen surface during the test. From the basic crack length and cycle count data, the fatigue-crack growth rate is determined as the quotient of the incremental crack growth divided by the incremental cycle count, i.e., $\Delta a/\Delta N$ or da/dN, the slope of the crack growth (life) curve.

The crack growth rate measures the resistance of the material to the applied loading conditions. The similitude parameter that allows data to be transferred from one cracked geometry to another is the range in stress-intensity factor (ΔK). The ΔK parameter is the difference between the maximum and minimum stress-intensity factors (K_{max} and K_{min} , respectively) for a cycle of loading. The property of fatigue crack growth rate is described throughout this Handbook as a function of ΔK .

2.5.2 Data Acceptance Criteria

In general, similar specimen configurations are used for fatigue-crack-growth testing as are used for other types of damage tolerant tests. The applied loads are reduced in magnitude and are cyclic in nature for studies of crack extension under fatigue loading conditions, and the experimental methods are extensions of the fracture testing procedures previously described. Instead of applying either a rising or sustained load to fracture the specimen, a constant amplitude cyclic load is applied to initiate and grow the crack over a significant portion of the specimen width. ASTM has published a standard testing method, i.e., ASTM E647, which covers the collection and reporting of fatigue crack growth rate data. Most of fatigue crack growth rate data reported in the Handbook were collected and reduced utilizing the guidelines and methods described by ASTM E647. For CCP and CT specimen

geometries, the ASTM Standard describes 11 explicit criteria for validating the data; these criteria are summarized in Table 2.4. A field is included in the handbook database which notes the da/dN data that failed to meet these ASTM criteria.

2.5.3 Data Reduction Procedures

Data reduction of crack growth rate from the crack length versus cycle count data was by one of two methods. The secant method was chosen when there were seven or less crack length versus cycle count measurements. A five point polynomial movable strip method was used for data with more than seven crack length versus cycle count measurements. This procedure was similar to the seven point method recommended in the ASTM standard; the five point method was chosen to provide additional data points at the extremes of growth rate range.

It is important to note that the calculation of stress-intensity factor range (ΔK) is the difference between the maximum and minimum stress-intensity factors (K_{max} and K_{min} , respectively) as defined in ASTM Standard E647. These calculations are best expressed using equations specific to a given geometry; for illustration purposes, assume that the test specimen geometry is CCP. Then, the maximum and minimum stress-intensity factors are given by

$$K_{\text{max}} = \sigma_{\text{max}} \sqrt{\pi a} \left[\sec \frac{\pi a}{W} \right]^{\frac{1}{2}}$$
 (2.13)

and

$$K_{\min} = \sigma_{\min} \sqrt{\pi a} \left(\sec \frac{\pi a}{W} \right)^{\frac{1}{2}}$$
 (2.14)

where σ_{max} and σ_{min} are the maximum and minimum stresses in the applied loading cycle. The range of stress-intensity factor is defined as

$$\Delta K = K_{\text{max}} - K_{\text{min}} \tag{2.15}$$

By ASTM convention, if K_{min} is compressive (negative), then $K_{min} \equiv 0$, and $\Delta K = K_{max}$.

TABLE 2.4 CRITERIA CHECKS FOR FATIGUE CRACK GROWTH RATE DATA

Criteria No.	ASTM E647 Paragraph	Specimen Type	Criterion
1	7.1.3.1 7.1.3.2	CT CCP	$\frac{W}{20} \le B \le \frac{W}{4}$
		001	$B \leq \frac{W}{8}$
2	Figure 1	CT CCP	W ≥ 1.00 inch. None
3	8.8.2	CT and CCP	If $B/W \ge 0.15$ need front and back crack lengths.
4	7.1.1 7.1.2	CT CCP	$\begin{array}{l} a_N \geq 0.2W \\ 2a_N \geq 0.2W \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$
5	8.3.1	CT and CCP	$a_1 \ge 0.1B$, h, or 0.04 inch, whichever is greater
6	8.8.3	CT and CCP	(Front Crack Length-Back Crack Length) < 0.025 W or 0.25 B, whichever is less.
7	8.8.1.1	CT	if $0.25 \le a/W \le 0.40$ then $\Delta a \le 0.04$ W $0.40 \le a/W \le 0.60$ then $\Delta a \le 0.02$ W $a/W \ge 0.60$ then $\Delta a \le 0.01$ W
	8.8.1.2	CCP	if $2a/W \le 0.60$ then $\Delta a \le 0.03$ W $2a/W > 0.60$ then $\Delta a \le 0.02$ W
8	8.8.1.3	CT and CCP	$\Delta a \ge 0.01$ inch, except in threshold region
9.	7.2.1	CT	$W - a \ge \frac{4}{\pi} (K_{max}/TYS)^2$
	7.2.2	CCP	W - a ≥ 1.25 P _{max} (B*TYS)
10	8.5.1	CT and CCP	<u>In Test</u> , Load Variation
			$0 \le \left \frac{P_{\max_{a+1}} - P_{\max_a}}{P_{\max_a}} \right \le 0.10$
11	8.3.2	CT and CCP	$\frac{\text{In Precracking}}{P_{\max_{a}} - P_{\max_{a}}} \leq 0.20 \text{ , and}$
			(2) $\Delta a \ge (3/\pi)(K_{\text{max}}^*/\text{TYS})^2$

CT = Compact Tension

CCP = Center Cracked Panel

B = Specimen Thickness W = Specimen Width

a = Crack Length

 $a_N = Notch Size$

a₁ = Fatigue Precrack Length

h = Height of Specimen

 $\Delta a = Change in Crack Length$

 $P_{max} = Maximum Load$ $K_{max} = Maximum Stress Intensity$

TYS = Tensile Yield Strength

 $K_{max}^{\star} = Maximum$ Stress Intensity at Smaller Crack Length Being Considered

2.5.4 Data Reporting Procedures

The presentation of fatigue-crack-propagation rate data is far more complex than the presentation of fracture toughness data (either K_{Ic} or K_c) due to the large quantities of data which must be treated. Where a fracture test generally yields a single characteristic toughness value, a fatigue-crack-growth test specimen generally yields from 10 to 100 rate data points, da/dN, which must be evaluated in terms of the stress-intensity factor range, ΔK .

The Damage Tolerant Design Data Handbook presents fatigue crack growth rate (da/dN) data in both graphical and tabular formats. Subsection 1.6.1 fully describes the presentation format of these data. A graphical format is used to present da/dN versus ΔK data and the mean trend of these data are given in tabular form. The least squares cubic spline approximation method has been selected from those available to provide a practical method for generating tables with fixed ΔK values. A least squares cubic spline approximation is an analytic method of fitting a "French" curve to a data set. The curve is constructed by fitting different cubic polynomials on non-overlapping, connecting subintervals over the range of the independent variable. In the Handbook, the independent variable will be ΔK . The boundary points of the intervals are referred to as knots and the cubic polynomials meet at the knots. The polynomials are also constrained so that the first and second derivatives are continuous at the knots. The result of this process is a smooth curve which passes through the center of the data.

Figure 2.20 is an example of a spline curve fit to a da/dN data set reported by Hudak et al. for 2219-T851 Aluminum alloy. The stress ratio used to establish the data shown was 0.3. The knots are marked in the figure by the large dots.

In general, da/dN data are well enough behaved so that a maximum of five knots was sufficient in generating the handbook tables. The actual number

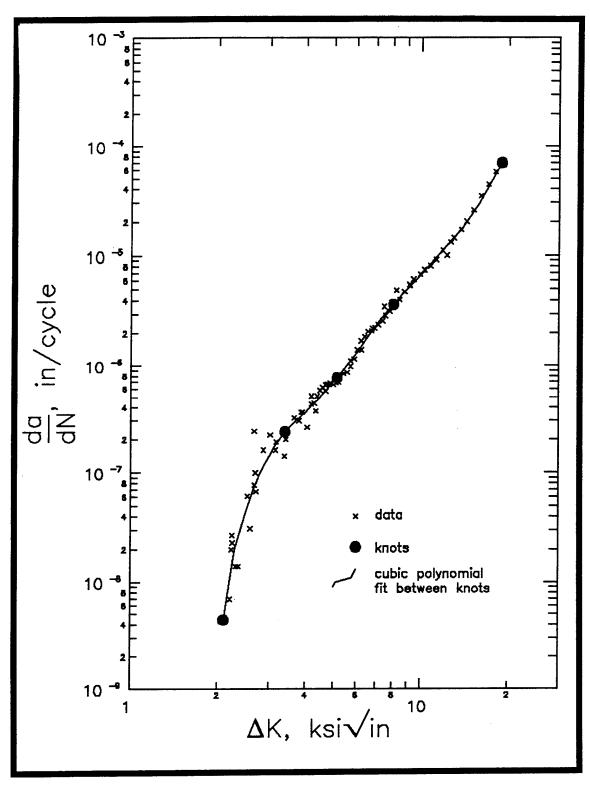


Figure 2.20 A Cubic Spline Curve Fit to FCGR Data for 2219-T851 Aluminum at a Stress Ratio of 0.3.

of knots used in fitting a curve to a set of data is a function of the root mean square percent error of the fit to the data and the pattern of the fitted line in $da/dN-\Delta K$ space.

The mean trend table for a set of da/dN data is generated by selecting points from the spline curve that has been fit to the data. The ΔK values will be chosen such that they are approximately equally spaced in a logarithmic scale and cover the complete range of ΔK values expected. The da/dN values are obtained through the interpolation of the spline curve at the preselected ΔK values. The complete set of ΔK values have been given previously in Table 1.11. Because the da/dN data do not always span the complete ΔK range, the table also reports the minimum and maximum da/dN values corresponding to the recorded minimum and maximum ΔK values. The extreme pairs of (ΔK , da/dN) points correspond to the extremes of the spline curve.

The root mean square percent error (RMSPE) is utilized to describe the statistical accuracy for the spline curve fit at each value of the varying parameter. The RMSPE is given by:

RMSPE = 100 x
$$\sqrt{\frac{1}{n} \sum_{i=1}^{n} \left(\frac{y_i - \hat{y}_i}{\hat{y}_i} \right)^2}$$
 (2.16)

where

 $y_i = observed da/dN |_i$ at ΔK_i

 $\hat{y}_i = da/dN$ interpolated from table at ΔK_i .

The RMSPE is a measure of how close the data lie to the mean trend table and has a similar interpretation to the coefficient of variation, i.e., the smaller the better. The coefficient of variation is used when all the data have the same mean and is calculated by dividing the standard deviation by the mean and multiplying by 100. For da/dN data, the mean da/dN is a function of ΔK so this is taken into account

when calculating the RMSPE. The RMSPE is an average percent error of the observed da/dN values from the curve established by the mean trend table.

When evaluating the mean trend da/dN description, engineers have come to rely on an evaluation of the ability of the mean trend curve to repredict the initial a versus N data and, in particular, to rely on life prediction ratio (N_p/N_A) which relates the predicted number of cycles (N_p) required to propagate a crack through a specified increment to the actual number of cycles (N_A) observed to propagate a crack through the same increment. Life prediction ratios between 0.8 and 1.25 are considered good and a life prediction ratio of 1.0 is ideal.

As a second measure of how well the mean trend curve fits the data, a summary of the life prediction ratios for the specimens used to generate the mean trend curve is included at the bottom of Figure 1.12. This summary places the plot symbol assigned to a specimen test along the LPRS scale at its calculated location. The actual LPRS value is greater than 2 for tests whose plot symbols are placed beyond 2 in the LPRS scale.

The life prediction ratios summarized in Figure 1.12 are self predictions and as such will tend to be good. However, the summary is only valid for the data used to generate it and therefore should not be generalized to other situations. The life prediction ratio summary is not intended to predict how well the mean trend curve will predict crack growth for an arbitrary specimen; however, it does illustrate how well the mean trend in FCGR correlates with the lives of the cracks that were used in generating the mean trend.

2.6 SUSTAINED-LOAD CRACK GROWTH RATES

2.6.1 Sustained-Load Crack Growth Rate Behavior

Sustained-load crack growth rate behavior is another type of subcritical crack growth behavior exhibited by materials which are sensitive to environmental

attack. This type of subcritical crack growth behavior normally exhibits itself as a time-dependent crack growth rate process, whereby cracks are noted to extend under steady-state (sustained) static loading conditions in the presence of environments. Crack growth mechanisms controlling the sustained-load crack growth rate process include: stress-corrosion cracking, hydrogen embrittlement, liquid metal embrittlement, grain boundary separation, and creep. In practice, the time-dependent cracking process has been found to be driven by internal (residual) tensile stresses in the fabricated structure, even in the absence of externally applied loads; typically, however, the stressing condition which drives the crack is provided by external loads.

The objective of sustained-load crack growth testing is to determine the rates at which cracks propagate in precracked specimens subjected to statically applied loads and prescribed environmental conditions. As with fatigue crack growth rate tests, most of the crack length measurements are made optically on the specimen surface during the test. Nonoptical methods used to establish cracking include compliance and stress wave analysis techniques. From the basic crack length and time data, the sustained-load crack growth rate is determined as the quotient of the incremental crack growth divided by the incremental time, i.e., $\Delta a/\Delta t$ or da/dt, the slope of the crack growth (time to failure) curve.

The crack growth rate measures the resistance of the material to the applied loading for the specified environment. In this case, the similitude parameter that allows data to be transferred from one cracked geometry to another is the static stress-intensity factor (K_{max}) . The K_{max} parameter is the stress-intensity factor evaluated for the applied loading and current crack length. The property of sustained-load crack growth rate (da/dt) is described throughout this Handbook as a function of K_{max} .

2.6.2 Data Acceptance Criteria

For the most part, the testing methodology for da/dt properties follows that utilized to obtain da/dN properties. There are, however, no current ASTM standards that specifically cover the collection of da/dt data. Sustained-load data have been obtained with a variety of specimens including double cantilever beams (DCB), tapered double cantilever beams (TDCB), compact tension (CT) specimens, cantilever beams (CANT), single-edge-notch tensile (SENT) specimens, part-through-surface crack (PTSC) specimens, and center-cracked panel (CCP) specimens.

One validity criterion that is sometimes applied to da/dt data is that the thickness dimension and crack length must be greater than 2.5 $(K_{Iz}/\sigma_{ys})^2$. No da/dt data were excluded from the 1993 revision, however, based on this criteria due to the scarcity of da/dt data. The reader will find K_{Ic} , σ_{ys} and thickness reported with da/dt data whenever these were available.

Readers should note that sustained load crack growth rate data in aluminum alloys in planes other than those parallel to the surface of rolled plates are questionable because of the localized corrosion that occurs on the planes even though the initial notch and crack orientation are normal to these planes.

2.6.3 Data Reduction Procedures

Data reduction of sustained-load crack growth rates was accomplished using the secant method applied to crack length (a) measurements recorded as a function of time (t). These calculations and those of static stress-intensity factor were provided to the data processing organization for reformatting.

2.6.4 Data Reporting Procedures

The data reporting procedures for sustained-load cracking data are similar to those discussed in Subsection 2.5.4 for fatigue crack growth rates. The

major difference between the two subcritical cracking rate reporting procedures is that da/dt vs K_{max} describes the sustained-load behavior whereas da/dN vs ΔK describes the fatigue behavior. The reader might also note that no a vs t were available to compare with the integrated crack growth mean trend data and therefore no life prediction ratios were presented.

2.7 THRESHOLD STRESS INTENSITY (K_{Iscc})

2.7.1 The Threshold

In many environments, materials exhibit a condition whereby cracks are not observed to grow if the static stress intensity factor is below a critical level, designated K_{Iscc} . This property is specific for a given material in a given environment within a specified time period. In high-strength materials, K_{Iscc} may be only a small fraction of the plane-strain fracture-toughness value (K_{Ic}) of the material. In lower strength tougher materials where plane-strain conditions still prevail, K_{Iscc} may approach or equal K_{Ic} , if the environment has little or no effect on the stress intensity required to propagate a crack.

K_{Iscc} data have been obtained with a variety of specimens including: Cantilever beam (CANT), 3-point loaded bend beam (NB), 4-point loaded bend beam (4-NB), Single-edge notch tensile (SENT), Center-cracked tensile (CNT), Part-through surface-crack (PTSC), Compact tension (CT), Bolt loaded WOL (BWOL), Double cantilever beam (DCB), and Tapered or contoured double cantilever beam (TDCB). All specimens are notched and precracked by fatigue, and many specimens are side grooved (SG) to ensure that the crack propagates in one plane perpendicular to the applied tensile loading and also to minimize the contribution of shear lips at the edges of the crack.

The types of specimens for determining $K_{\rm Iscc}$ fall into two broad categories: those that are loaded by weights or tensile machines (see Figure 2.21) and

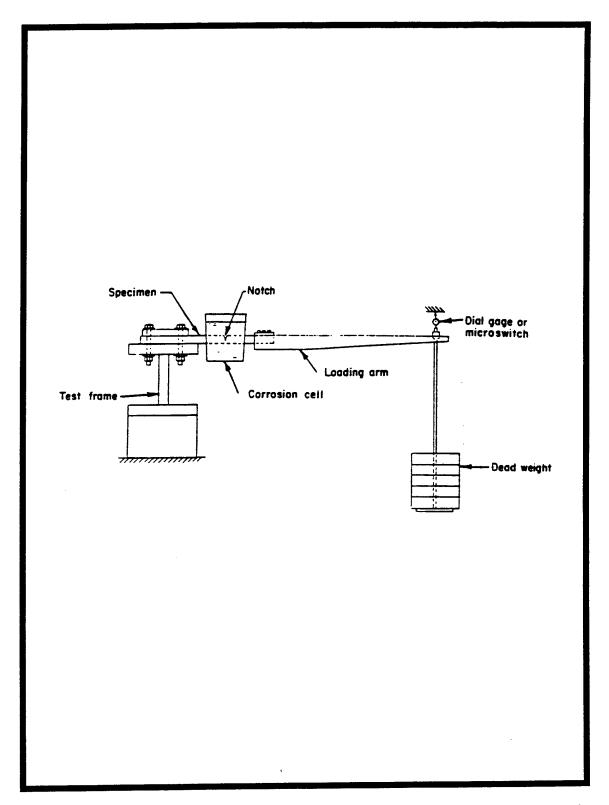


Figure 2.21 Schematic Drawing of Fatigue Cracked Cantilever Beam Test Specimen and Fixtures.

those that are self-loaded as by bolts. The former require bulky setups to accommodate lever arms, weights, and tensile machines while the latter are compact and portable. Thus the environment is applied to the externally loaded specimens usually in the form of a small container sealed onto the specimen, while the self-loaded specimen may be completely immersed in the environment.

Under dead-weight loading conditions, the usual practice is to run a number of specimens at various stress intensities less than $K_{\rm Ic}$ for a finite length of time (more than 24 hours and usually about 500 hours) to establish $K_{\rm Iscc}$. Another method is to step load a single specimen until the crack starts to propagate. This method requires holding after each load increment for a sufficient time to establish that crack propagation does not occur.

Under bolt self-loading conditions, sufficient load is first applied to the bolt to cause the crack to extend beyond its precracked position. The specimen is then exposed to the environment. As the crack propagates in the environment, the stress-intensity factor decreases at the tip of the advancing crack until the crack arrests at K_{lscc} . Specimen length must be sufficient to ensure that the crack arrests before completely penetrating the specimen, thus assuring that a value is obtained for K_{lscc} .

2.7.2 Conditions for Validity of Data

There are no ASTM standards that specifically cover the collection of K_{Iscc} data. The criterion typically used to validate K_{Iscc} data is that the thickness dimension (B) and initial crack size after precracking (a_o) are greater than the ASTM E399 requirement for plane-strain fracture toughness, i.e., that B and $a_o \ge 2.5$ (K_{Ic}/σ_{ys})². However, because the initial crack size is not currently stored in the handbook database, only the thickness requirement was checked. Data which did not meet this criterion are identified in the K_{Iscc} tables with an asterisk. Many tests reveal a drastic reduction in the stress intensity required to propagate a crack even

though the 2.5 $(K_{Ic}/\sigma_{ys})^2$ criterion is not met. Although these data are not recommended for material selection and design purposes, they do indicate a qualitative effect.

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3.22	4340(DH) 3-	
3.23	4340(EFM) 3-	
3.24	4340(MOD) 3-	
3.25	4340(VAR) 3-	
3.26	10101	-202
3.27		-204
3.28	AF1410 3-	
3.29	AF1410(VIM-VAR) 3-	-222
3.30	D6AC 3-	
3.31	H11 3-	
3.32	HP9-4-20 3-	
3.33		-348
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3.35		-356
3.36		-423
3.37	111 100 1111111111111111111111111111111	-424
3.38		-425
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TABLE 3.0.1

Alloy	Condition/ Heat Treatment	Product Form	K _{Ie}	Ke	R Curve	da/dN	da/dt	K _{Isco}
10NI STEEL	Unspecified	Plate				13		
12-9-2 (MAR)	STA 900	Round Bar	1			2		
		Unspecified						8
	Unspecified	Plate						-
	1600F 900F 20HR AC	Plate						2
	BLECTRIC FURNACE	Plate						-
	GTA WELDED	Weldment						1
1ZNF5CK-3MO	LOW-RESIDUAL	Plate						1
	TYS=150KSI	Plate						1
	TYS-160KSI	Plate						1
	TY9-170K9I	Plate						1
	TY8-175KSI	Plate						1
	1500F 1HR AC 900F 3HR	Plate						2
	TY9-170K8I	Plate						1
	TYS-176K8I	Plate						1
	TYS-178KSI	Plate						1
18NI(180XMAK)	TY9-185KSI	Plate						1
	TYS-190KSI	Plate						1
	TY9-195KSI	Plate						-
	TYS-200KSI	Plate						1
	Unspecified	Plate						1
18NI(200XMAR)	1500F 1HR AC 900F 3HR	Plate						2

TABLE 3.0.1 (CONTINUED)

Alloy	Condition/ Heat Treatment	Product Form	\mathbf{K}_{lc}	К	R Curve	da/dN	da/dt	Klscc
	1650F 4.5 HR AC AGED 1000F 6HR	Plate	3					
	1650F 4.5 HR AC AGED 850F 24HR	Forging	1					
	1650F 4.5 HR AC AGED 900F 24HR	Plate	2					
	1650F 4.5 HR AC AGED 900F 6HR	Forging	8					
	1650F 4.5 HR AC AGED 950F 24HR	Plate	3					
18NI(200XMAR) (Cont'd)	1650F 900F 3HR AC	Plate						1
	1675F 2HR AC 500F 0.25HR 850F 4HR COOL 250F/MIN	Plate						1
	1675F 2HR AC 600F 15MIN 850F 4HR COOL 250F/MIN	Plate						-
	TYS-216KSI	Plate						1
	WELD CENTER LINE	Plate						1
18NI(250)	To a second seco	Unspecified					2	
	Onspecino	Plate					-	
	Unspecified	Plate						y
	1500F 11IR AC AGED 900F 31IR AC	Billet	13					
	1500F AC 850F 6HR	Plate	5					
	1500F AC 900F 24HR	Plate	9					
18NI(250)(MAR)	1500F AC 900F 6HR	Plate	8					
	1500F AC 950F 6HR	Plate	9					
	1650F 1.25HR WQ 1626F 1.25HR WQ 900F 3HR AC	Plate						8
	900F ZHR AC	Sheet						2
	AGE 900F 3HR	Plate						1

TABLE 3.0.1 (CONTINUED)

Alloy	Condition/ Heat Treatment	Product Form	$ m K_{Ic}$	K	R Curve	da/dN	da/dt	Kisco
	AGED 900F 3HR AC	Plate						2
18NI(250XMAR)	TYS-250KSI	Plate						-
(Cont'd)	TY9-260KSI	Plate						1
	UTS-243KSI	Billet				s		
18NI(280XMAR)	1600F 1HR AC 900F 3HR	Plate						-
	Unspecified	Unspecified					1	
18N1(300)	AGED GHR 900F	Unspecified					-	
	14	Sheet		29				
	Unspecified	Forging				1		
	1500F 0.5HR AC900F 3HR	Plate						2
	1500F 2HR 800F 10HR	Bar						-
	1500F 2HR 900F 100HR	Bar						و
	1500F 2HR 900F 3.5HR	Bar						5
	1700F 1500F AGED 900F 6HR	Forging						1
18NI(300XMAR)	1700F 1HR AC 1500F 1HR AC 900F 6HR	Forging	æ					
	2300F 11fR 1700F 4HR 800F 10HR	Bar						2
	2300F 1HR 1700F 4HR 900F 100HR	Bar						8
	2300F 1HR 1700F 4HR 900F 3.5HR	Bar						2
	900 F AGED	Plate	1					
	900F 3HR 950F 3HR	Forging						1
	AGE 900F 6HR	Forging						6
	AGE 960F 12HR	Forging						1

TABLE 3.0.1 (CONTINUED)

Alloy	Condition/ Heat Treatment	Product Form	K _{Ic}	Ke	R Curve	da/dN	da/dt	Klscc
	AGED	Unspecified				2		
	ANNEALED	Unspecified				2		
18NT(300XMAR) (Cont'd)	CRACK PRESTRESSED TO 25 PCT KIC	Forging						-
	CRACK PRESTRESSED TO 60 PCT KIC	Forging						1
	CRACK PRESTRESSED TO 80 PCT KIC	Forging						1
18NI(350)	AGED 8HR 800F	Unspecified					1	
	1500F 111R 800F 8HR	Forging						1
	1500F 1HR 900F 8HR	Forging						1
TONIVOEDVICEDO	1500F 1HR 950F 3HR	Forging						1
(NTWWYOOO) NIGH	AGE 800F 811R	Forged Bar						1
	AGE 900F 3HR	Forged Bar						1
	AGE 900F BIIR	Forged Bar						
		Unspecified					1	
	Unspecified	Plate						2
		Forging	8			14		+
***************************************	1500F 0.51IR OQ 550F 2+2 IIR (COARSE GRAINED STRUCTURE)	Plate		·				-
Windows 	1500F 0.51IR OQ 550F 2+2 HR (FINE GRAINED STRUCTURE)	Plate						-
	1500F 0.51IR OQ400F 2+2 HR (COARSE GRAINED STRUCTURE)	Plate						-
	1500F 0.511R OQ400F 2+2 HR (FINE GRAINED STRUCTURE)	Plate						1

Alloy	Condition/ Heat Treatment	Product Form	K _{lc}	K	R Curve	da/dN	da/dt	K _{Iscc}
	1650F 0.6HR OQ 400F 2+2 HR (COARSE GRAINED STRUCTURE)	Plate						1
	1550F 0.51IR OQ 400F 2+2 HR (FINE GRAINED STRUCTURE)	Plate						-
	1550F 0.5HR OQ 550P 2+2 HR (COARSE GRAINED) STRUCTURE)	Plate						-
	1550F 0.51IR OQ 550F 2+2 HR (FINE GRAINED STRUCTURE)	Plate		·				-
	1600F 0.5HR OQ 400F 2+2 HR (COARSE GRAINED STRUCTURE)	Plate						grand
	1600F 0.5HR OQ 550F 2+2 HR (COARSE GRAINED STRUCTURE)	Plate						-
	1600F 0.5IIR OQ 550F 2+2 HR (FINE GRAINED STRUCTURE)	Plate						gant
300M (Cont'd)	1600F 0.511R 9Q 1000F 0.5.1.01fR 0Q 80.180F 25MIN 576F 2+21IR	Forging	12					
	1600F 1.25 HR OQ 600F 2+2HR	Forging	10					
	1600F 1HR OQ 1HR WQ 475F 1HR	Ваг	1					
	1600F 1HR OQ 476F 1HR	Ваг	1					
	1600F 1HR OQ 675F 1HR	Ваг	1					
	1600F 11IR OQ 615F 1HR	Bar	1					
	1600F 1HR OQ 745F 1HR	Bar	1					
	1600F OQ 650F 2+2HR	Plate	1					
	1600F OQ 676F 2+2HR	Sheet					ī	
	1650F 1525P OQ600F 2+2HR	Forging						1
	1650F 1600F 1HR OQ 600F 1+1 HR	Forging						

Alloy	Condition/ Heat Treatment	Product Form	K_{Ic}	Ж	R Curve	da/dN	da/dt	Klscc
	1675F AC 1575F OQ 1100F 2HR (RC 39)	Plate	4					
	1675F AC 1575F OQ 500F 2HR (RC 51.5)	Plate	4					
	1675F AC 1575F OQ 800F 2HR (RC 47.5)	Plate	4					
	1700F 1.5HR AC 1600F 1.5HR OQ 600F 2+2HR	Forging						12
	1700F 1.5HRS AC 1600F 1.5HRS OQ 600F 2+2HRS	Forging				10		
	1700F 11IR AC 1600F 11IR OQ 600F 21IR AC (AMS 6419)	Plate	8					
	1710F+1610F 610F	Bar						7
	2190F 111R FC TO 1600F HOLD 0.5HR OQ 475F 11HR	Bar	2					
	2190F 111R FC TO 1600F HOLD 0.5HR OQ 615F 1HR	Bar						
300M (Cont'd)	2190F 111R FC TO 1600F HOLD 0.51IR OQ 745F 11IR	Bar	-					
	2190F 11IR OQ 400F 11IR	Bar	1					
	2190F HIR OQ 475F HIR	Bar	1					
	2190F 1HR 0Q 475F 1HR W1 475F 1HR	Bar	1					
	2190F 1HR OQ 616F 1HR	Bar	1					
	2190F 1HR OQ 746F 1HR	Bar	1					
	ANG GAS	Sheet		3				
	FOX ONL	Plate		15				
	HEAT TREATED TO 64 RC HARDNESS	Plate	2					
	TENANCE ARE SET	Billet				20		
	O 15 E COUNTY	Bar ·				8		

Klace												-	-					1	1		
da/dt																					
da/dN																					
R Curve																					
Ke																					
$ m K_{lc}$	8	1	2	2	1	2	1	1	8	8	3			1		1	10			1	2
Product Form	Porging	Forging	Plate	Plate	Plate	Plate	Plate	Plate	Billet	Billet	Billet	Plate	Plate	Forged Bar	Forged Bar	Forged Bar	Plate	Plate	Plate	Forged Bar	Forged Bar
Condition/ Heat Treatment	1650F 1HR AC 1550F 1HR OQ -320F 0.51IR 600F 2+2HR AC	1650F 1HR AC 1550F 1HR OQ -320F 0.5HR 600F 2+2HR AC	1500F OQ 400F 2+2HR	1600F OQ 660F 2+2HR	1550F OQ 400F 2+2HR	1650F OQ 650F 2+2HR	1600F OQ 400F 2+2HR	1600F OQ 650F 2+2HR	1700F AC 1600F 11IR OQ 550F 2+21IR	1700F AC 1600F 111R SQ 400F AC 550F 2+211R	1700F AC 1600F 1HR SQ 975F OQ 675F 2+2HR	1550F 1HR OQ 1000F 1HR AC 1125F 1HR AC	1650F 1HR OQ 1250F 1HR AC	1600F 1 HR OQ 400F 1HR	1600F 1 HR OQ 535F 1HR	1600F 1 HR OQ 746F 1HR	1600F 1HR 1550F 1HR OQ AT 150-175F 900F 1HR	1700F 1600F OQ 600F 1+1 HR	1700F 1600F OQ 750F 1+1 HR	2010F 1 HR OQ 400F 1HR	2010F 1 HR OQ 476F 1HR
Alloy	300M (AM)	300M (VAR)					300M (VM)										4140				

Alloy	Condition/ Heat Treatment	Product Form	K _{le}	K	R Curve	da/dN	da/dt	$K_{ m Iscc}$
	2190F 1 HR OQ 400F 1HR	Forged Bar	2					
4140	2190F 1 HR OQ 475F 1HR	Forged Bar	2					
(Cont'd)	2190F 1 HR OQ 615F 1HR	Forged Bar	1					
	2190F 1 HR OQ 660F 1HR	Forged Bar	1					
4330V	QUENCHED + TEMPERED AT 500F	Plate						-
	Unspecified	Billet	3			1		
	1600F 1HR OQ 400F 1HR	Forged Bar	1					
4330V (MOD)	1600F 11IR OQ 535F 1HR	Forged Bar	2					
	1650F 1HR AC 1576F 1HR OQ 800F 2+2HR	Billet	6					
	HEAT TREATED TO 46 RC HARDNESS	Plate	2					
		Unspecified					1	
	. !	Sheet						2
	Unspecified	Plate					1	1
		Forging						1
	1350F OQ 750F 1.25HR	Plate						
4340	1550F OQ 750F 1HR CRACK PRESTRESSED TO 20PCT KIC	Plate		·				1
	1550F OQ 750F CRACK PRESTRESSED TO 20PCT KIC	Plate						
	1650F OQ 750F CRACK PRESTRESSED TO 40PCT KIC	Plate						1
	1650F OQ 750F CRACK PRESTRESSED TO 60PCT KIC	Plate						1

Alloy	Condition/ Heat Treatment	Product Form	K _{le}	Ke	R Curve	da/dN	da/dt	Klscc
	1650F OQ 750F CRACK PRESTRESSED TO 80PCT KIC	Plate						-
	1550F OQ TEMPERED 500F	Plate	4					
	1550F OQ TEMPERED 800F	Plate	2					
	1575F 0Q 675F 4HR	Plate						-
***************************************	1575F OQ 800F 4IIR	Plate						1
	1600F 1HR 1525F 2.5HR OQ AT 150-176F 900F 1HR	Plate	9					
	1600F 1HR OQ 400F 1HR	Forged Bar	1					
	1600F 1HR OQ 635F 1HR	Forged Bar	2					
	1600F 1HR OQ 600F 1+1HR	Forging						-
4340	1600F 1HR OQ 660F 1HR	Forged Bar	-					
(Cont'd)	1600F 1HR OQ 746F 1HR	Forged Bar	1					
	1625F Q 1625F OQ 400F 2+211R 1626F Q 1525F OQ	Forging						2
	1650F 111R AC 1480F 211R OQ LN 0.2511R 400F 1+11R OQ	Bar						
	1650F 1HR AC 1680F 2HR OQ LN 0.25HR 400F 1+1HR OQ	Bar		-				gard
	1650F 1HR AC 1525F 1HR OQ 800F 2HR	Billet	9					
	1700F 0.25HR AC 1550F OQ 600F 1+1HR	Sheet						2
	1800F Q 600F 1+11HR	Forging						12
	2190F 1HR FC TO 1600F HOLD 0.5HR 400F 1HR	Forged Bar	2					
	2190F 1HR FC TO 1600F HOLD 0.5HR 535F 1HR	Forged Bar	2					
	2190F 1HR FC TO 1600F HOLD 0.5HR 660F 1HR	Forged Bar	2					

Alloy	Condition/ Heat Treatment	Product Form	K _{Ic}	Ke	R Curve	da/dN	da/dt	Klscc
	2190F 1HR OQ 476F 1HR	Forged Bar	1					
	2190F 1HR OQ 635F 1HR	Forged Bar	1					
	450F TEMPER	Unspecified				2		
	750F TEMPER	Unspecified				6		
	HEAT TREATED TO 51 RC HARDNESS	Plate	2					
	MARTEMPERED	Plate				4		
	TEMPER 400F 1HR	Plate					80	
	TEMPERED 400F	Unspecified					4	
	TY9-125K8I	Plate						1
	TYS-150KSI	Plate						1
4340	TYS=176KSI	Plate						_
(Cont'd)	TYS-200.240K5I	Extrusion					4	
	TY9-200K3I	Plate						-
	TY9-220KSI	Forging					2	
	TY9-225K9I	Plate						-
	ITTO. JENVOI	Unspecified				7		
	013=100031	Forging				8		
	UTS-160-180KSI	Bar				6		
	UTS=160KSI	Round Bar				3		
	UTS=180 KSI	Round Bar	1					
	TO TO THE SALESTON	Plate				2		
	U 3=180-200A31	Ваг				2		

Kisco							-	-	-	-	-	-	-	-	-	_	1	-		
da/dt						-														ø
da/dN	7	10																		
R Curve																				
K															-					
K_{lc}			8	12	10														8	
Product Form	Forging	Round Bar	Forging	Billet	Forging	Plate	Bar	Bar	Forging	Forging	Forging	Forging	Forging	Forging	Forging	Forging	Forging	Forging	Forging	Extrusion
Condition/ Heat Treatment	107/01 0141	013*190031	1600F 1HR AC 1550F 1HR OQ -320F 0.5HR 400F 2HR AC	1550F OQ 900F 1HR	1600F 11IR AC 1550F 1HR OQ -320F 0.51IR 400F 2HR AC	1550F .5HR 400F 4HR	1650F 1HR 1600F 1HR OQ 1+1 400F (0.09 SI)	1650F 1HR 1600F 1HR OQ 1+1 600F (0.09 SI)	1600F Q 460F 1+11IR (0.20C)	1800F Q 500F 1+11IR (0.21C)	1800F Q 600F 1HR (0.20C)	1800F Q 650F 1+11fR (0.28C)	1800F Q 650F 1HR (0.24C)	1800F Q 700F 1HR (0.21C)	1800F Q 780F 1+1HR (0.33C)	1800F Q 800F 1HR (0.46C)	1800F Q 900F 1HR (0.64C)	1800F Q 925F 1+1HR (0.63C)	1600F 1HR AC 1650F 1HR OQ -320F 0.5HR 400F 2HR AC	Unspecified
Alloy	4340	(Cont'd)	4340 (AM)		4340 (DH)	4340 (EFM)						(100 K) 076 K	(GOW) OFCE						4340 (VAR)	4340V

Alloy	Condition/ Heat Treatment	Product	K _{Ic}	K	R Curve	da/dN	da/dt	Klecc
		Plate	,			80		
A286	1800F 0.5-1.0 HR WQ 1325F 16HR AC	Round Bar				8		
	Unspecified	Forging	10					
	1525F 11fR AC -100F 11fR AC 950F 61fRS AC	Round Bar				12		
-	1675 FOR 1HR; -100 FOR 3HR; 925F FOR 6 HR	Forging	1					
	1676 FOR 211R; -100F FOR 311R; 925F FOR 6 HR	Forging	1					
	1575F FOR 1HR AIR COOLED; 1575F FOR 1HR; -100F FOR 3HR; 925F 6HR	Forging	-					
	1575F FOR 11IR AIWFAN COOLED; -100F FOR 31IR; AIR WARMED 925F FOR 51IR	Forging	-					
	1575F FOR 21IR AIR COOLED; -100F FOR 31IR; 926F 6HR	Forging	-					
	1650F 111R WQ 1500F 111R WQ 950F 611R AC	Plate	9					
AF1410	1650F 11IR WQ 1500F 1IIR WQ 950F 5IIRS AC	Plate	1					
	1650F FOR 21th Air Cool.Ed; 1250F For 81fr; 1575 For 11fr; -100F For 31fr; 925F For 6 ir	Forging	. 1		,			
	1650F FOR 21IR AIR COOLED; 1250F FOR 81IR; 1575F FOR 11IR; -100F FOR 31IR; 925F 6HR	Forging	1					
	AGED AT 900F FOR 5 HOURS	Bar	9.					
	AGED AT 925F FOR 5 HOURS	Bar	1					
	AIR QUENCHED	Plate				-		
	OIL QUENCIIED	Plate				1		
	PRACED AT 0955 TAY OF USE	Forging	1					
		Bar	1					

Alloy	Condition/ Heat Treatment	Product Form	K _{Ic}	Ř	R Curve	da/dN	da/dt	$ m K_{Iscc}$
AF1410 (Cont'd)	REAGED AT 925F FOR 7.5 HOURS	Ваг	1					
AF1410(VIM-VAR)	1650F 1HR WQ 1600F 1HR WQ 950F 5HRS AC	Plate				12		
	1650F 25MIN OQ 850F 1+1 HR	Sheet						2
	1550F AQ 650F 4HR	Sheet						-
	1550F AQ 950F 4HR	Sheet						1
	1615F 2.25HR A-BQ 325F AC 310-345F 3HR 1080F 6-6.5HR	Forging	61					
	1650F 1HR FC 1650F 1HR OQ 1026F 2+2HR	Billet	2					
	1650F 111R FC TO 960F OQ AT 150F AC 1000F 2+211R	Billet	2					
	1650F 111R FC TO 960F OQ AT 180F AC 1025F 2+211R	Forging	6					
	1650F A-BQ AT 975F SQ AT 375F 1000F 2+2HR	Forging				20		
D6AC	1650b A DO AT 0750 GO AT AMO 1000 9. DIT	Plate				17		
	VIII7+7 10001 1006 14 bg 1010 14 bg 11 1001	Forging				1		
	1650F AUS-BAY QUENCH 976F SQ 1000F 2+2HR	Plate	7					
	1650F AUS-BAY QUENCH 975F 9Q 325F 1000F	Plate	78					
	2+2HR	Forging	30					
	1650F AUS-BAY QUENCII 976F SQ 376F 1000F 2+211R	Forging	88					
	1650F AUS-BAY QUENCH 975F SQ 400F 1000F	Plate	103					
	2+2HR	Forging	53					
	1675F AC 1575F OQ 400F 2HR 1100F 2HR (RC 425)	Plate	4					

Alloy	Condition/ Heat Treatment	Product Form	Kle	Ke	R Curve	da/dN	da/dt	Klscc
	1675F AC 1575F OQ 400F 2HR 500F 2HR (RC 50)	Plate	4					
	1675F AC 1575F OQ 400F 2HR 800F 2HR (RC 46.5)	Plate	4					
	1700F 111R FC TO 960F OQ AT 150F AC 1000F 2+211R	Billet	8					
	1700F 1HR OC 1025F 2+2HR	Billet	9					
	THE AT OFFICE OF THE PARTY OF T	Plate				24		
	11001 7:154 A1 8105 O4 A1 1405 10005 2+211183	Forging				01		
D6AC	1700F AUS-BAY QUENCH 976F OQ 140F 1000F	Plate	73					
(1900)	2+2HR	Forging	49					
	1725F 111R AC 1700F 11IR OQ 1000F 11IR 1016F 11IR	Billet	8		-			
	1725F 11IR AC 1700F 11IR OQ 1025F 2+2HR	Billet	9					
	1725F 111R AC 1700F 111R OQ 1100F 2+211R	Billet	9					
	1725F 111R AC 1750F 111R FC TO 960F SQ 350F 0.511R AC 1025F 22HR	Billet	3					
	HEAT TREATED TO 46 RC HARDNESS	Plate	2					
	Unspecified	Unspecified					4	
	1325F 1850F 0.5HR AC 1060F 2+2HR	Sheet						2
	AUSTENIZED & TEMPERED (TYS-220KSI)	Round Bar				9		
	QUENCHED + TEMPERED AT 1100F	Plate						-
		Plate						2
HP9-4-,20	Unspecified	Forging	4			80		23
		Bar				2		

Alloy	Condition/ Heat Treatment	Product Form	$ m K_{Ic}$	K	R Curve	da/dN	da/dt	K _{Iscc}
		Plate				11		
	1525F ZHRS AC - 100F ZHRS 1025F 4HRS	Billet				22		
		Plate						80
	1626F 211RS OQ - 100F 211RS 1025F 411RS	Forged Bar						12
	1525F OQ -100F 11IR 1065F 4+41IR	Forging	2					
	1650F 1-2HR AC 1-2HR 1-2HR AC -100P 1.5HR 1025F 4HR 1060F 4HR	Plate	8				·	
	1650F 1-2HR AC 1-2HR 1-2HR AC -130F 1.5HR 1025-1075F 4HR	Plate	1					
	1650F 1-21IR AC 1525F 1-21IR AC -100F 1-21IR 1025F 41IR	Forging	2					
HP9-420 (Cont'd)	1650F 1-21IR AC 1625F 1-21IR OQ -100F 1-21IR 1025F 41IR	Forging	8					
	1650F 1-2HR AC 1525F 1-2HR OQ -100F 2HR 1000F 4-6HR	Forging	1					
	1650F 1-211R AC 1525F 1-21IR OQ -100F 21IR	Plate	10					
	1025F 4-6HR	Forging	26					
	1650F 1-211R AC 1625F 1-21IR OQ -100F 21IR 1050F 4-611R	Forging	9					
	1650F 1-2HR ACX	Forging	3					
	1650F 2HR AC 1625F 2HR OQ 1000F 2+2HR AC	Forging	8					
	1650F 4.5HR AC TO 900F HELD 0.5HR AC -100F 1.5HR 1025F 8HR A-BQ	Forging	2					
	1700F 4,511R AC 1700F 1.5HR AC -100F 1.5HR 1025F 4HR	Forging	2					

Alloy	Condition/ Heat Treatment	Product Form	K _{Ic}	K	R Curve	da/dN	da/dt	KIscc
	ANNEALED	Forging	16					
	GTA WELD WELDMENT	Plate						-
HP9-420 (Cont'd)	HEAT TREATED	Forging	17					
	QUENCHED + TEMPERED	Plate						2
	WELDED	Weldment				3		
HP9.420(CEVM)	ANNEALED	Forging				80		
HP9-425(VAR)	1650F 11IR OQ 1000F 2+2HR AC	Forging	14					
		Plate				23		
	Unspecified	Forging	4			8		4
		Bar				8		
	1625F 2HRS OQ -100F 1HR 1025F 2+2HR	Forged Bar				1		
	1525F 2HRS OQ -100F 2HRS 1025F 2+2HR	Forged Bar				2		
	1525F OQ -100F 3HR 1050F 4HR	Forging	1					
-	1550F 2HRS OQ - 100F 1HR 1025F 2+2HR	Forged Bar				=		
1119-4-30	1550F 2HRS OQ -100F 3HRS 1000F 2+2HRS	Forged Bar				1		
	1650F 1-2HR AC 1626F 1-2HR OQ -100F 1-3HR 1000F 4HR	Forging						
	1650F 1-2HR AC 1626F 1-2HR OQ -100F 1-3HR 1026F 4HR	Forging	8					
	1650F 1-21IR AC 1625F 1-21IR OQ -100F 1-31IR 1050F 4HR	Forging	2					
	1650F 21IR AC 1650F 21IR OQ -100F 21IR AC 1000F 41IR AC 1000F 41IR AC	Forging	ı					
	1650F 2HR AC 1650F 2HR OQ 1000F 2+2HR AC	Forging	2					

TABLE 3.0.1 (CONCLUDED)

Alloy	Condition/ Heat Treatment	Product Form	$\mathbf{K}_{\mathbf{lc}}$	Ke	R Curve da/dN	da/dN	da/dt	$K_{ m Iscc}$
	1650F AC 1525F 1-2HR OQ -100F 1-3HR 1050F 4HR	Forging	-					
HP9-430	HEAT TREATED TO 49 RC HARDNESS	Plate	2					
(name)	QUENCHED + TEMPERED AT 950F	Plate						2
	UTS=220.240KSI	Billet				25		
90	1600F 0.5HR AC 1500F 0.33HR AC	Sheet						2
05'-1-6-10	476F	Plate						-
HY-150	1500F 1HR WQ	Plate						-
HY-180	STA (UTS-180KSI)	Forged Bar				4		
11Y-80	Unspecified	Unspecified				2		
91.6	1700F 1HR AC 1600F 1HR OQ 550F 2HR	Forging	3					
	1700F 111R AC 1600F 1HR+1000F 20 MIN	Forging	2					

TABLE 3.0.2

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF ALLOY STEELS
AT ROOM TEMPERATURE

		S-L	Min Spec n Mean Std Thk	:	***	1		1	:	1				0.25 4 54.1 1.1	1	1	
	ation		Std S Dev	,			1	3		ı	Į.	1	2.0	1.7		1	,
$K_{Ic}~(Ksi\sqrt{in})$	Specimen Orientation	T·L	Mean	:	:	ı	1	64.1	i	1	1	1	62.9	50.6	i	ï	9 83
ζ_{Ie} ()	men	L	u	:	:	1	!	9	:	1	!	1	1	2	1	I	,
	Specia		Min Spec Thk	1	ı	i	÷	0.50	:	1	1	:	1.25	0.25	i	ı	0.45
			Std Dev	1.2	0.7	9.0	1.2	4.2	1.9	1.2	3.2	2.6	2.3	2.6	0.7	3.8	
		L-T	Mean	102.3	96.5	100.3	6.66	74.3	76.0	80.7	82.3	84.0	62.6	54.6	61.8	47.9	1
		I	g	8	2	3	3	7	8	9	6	6	4	4	3	2	:
			Min Spec Thk	2.40	2.40	2.40	2.40	0.50	1.80	1.80	1.80	1.80	1.25	0.25	09:0	09:0	
Rongo of	Product	Thickness	(••••	4.25	4.25	3.00	4.25	1.00-12.00	4.25	2.00	2.00	2.00	1.25	3.00	0.56-1.00	0.62	1.00
	Product	Form		Plate	Plate	Forging	Plate	Billet	Plate	Plate	Plate	Plate	Forging	Forging	Plate	Bar	Plate
	Condition/	Heat Treatment		1650F 4.5 IIR AC AGED 1000F 6IIR	1650F 4.5 HR AC AGED 900F 24HR	1650F 4.6 HR AC AGED 900F 6HR	1650F 4.5 HR AC AGED 950F 24HR	1500F 1HR AC AGED 900F 3HR AC	1500F AC 850F 611R	1500F AC 900F 24IIR	1600F AC 900F 6HR	1500F AC 950F 6HR	Unspecified	1600F 1.25 HR OQ 600F 2+2HR	1700F 1HR AC 1600F 1HR OQ 600F 2HR AC (AMS 6419)	2190F 111R FC TO 1600F HOLD 0.61R OQ 476F 1HR	HEAT TREATED TO 64 RC
	Allov				MINOCONTRACT	OINI(SOOVIMAIN)			_	18NI(250KMAR)					300M		

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF ALLOY STEELS AT ROOM TEMPERATURE

Ran	Ran	Range of					K	Je (K	K_{Ic} $(Ksi\sqrt{in})$					
	Pro	Product					Specimen Orientation	nen (Orient	ation				
Form Thie	Thi	Thickness (in)		Ŋ	L-T			T-L	Ľ			-	S-L	
		(1111.)	Min Spec Thk	£	Mean	Std	Min Spec Thk	E	Mean	Std Dev	Min Spec Thk	u	Mean	Std Dev
Forging		4.00	06:0	6	46.5	3.8	ļ	1	;	i	:	:	:	
Forging		4.50	06:0	4	62.2	1.3	,		;	,		i	!	
Plate		97.0	09'0	2	48.0	17.0	:	;	1	,	:	;	:	:
Plate		0.56	09:0	2	49.5	10.6	ı	-	ï	!	:		1	!
Plate		0.56	09'0	2	62.5	3.5	ŀ	-	ï	ı	:	1		1
Billet		5.50	ŀ	i	. 1	i	1.00	တ	55.3	0.3	1	1	ŀ	ı
Billet		6.50	:	i	ı	ı	1.00	က	0.83	3.4	1	1	ļ	!
Billet		6.50	:	1	1	:	1.00	3	68.6	2.2	i	ı	ı	
Plate		1.00	ï	ı	ı	:	66.0	7	72.0	18.8	:	ı	i	:
Forged Bar		0.62	09:0	2	62.1	7.4		ï	i	1	:	1		!
Forged Bar		0.62	09.0	2	81.1	13.2		:		ï	i	i	;	!
Forged Bar		0.62	09:0	2	1.99	2.7	1	-	i	1	i	i	:	ŀ

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF ALLOY STEELS AT ROOM TEMPERATURE

	I	_	T	T	1		T -	T	7	T	I	1	T	T	T
			Std Dev	:	1	!	;	!	:	1	!	;	i	1	1
		S-L	Mean			1	:	1	:	!	:	ı		1	ı
		G 2	E		,	:		1	1	!	1	1	-	1	1
			Min Spec Thk	1	1			1	i	;	ı		ı	,	:
	tation		Std Dev	ı	i	9.0	1	1	1.5	!	ł	i	1		1.3
K_{Ic} $(Ksi\sqrt{in})$	Specimen Orientation	T-L	Mean		I	74.7	;		88.2	1	i	,	ı	1	51.7
ζ_{Ic} (men	L	ч	;	1	8	1	i	2	1	÷	i	1	1	2
I	Speci		Min Spec Thk	:	i	0.75	:		1.01	:	ı	i	ł	i	0.50
			Std Dev	3.8	7.6	ı	2.9	4.6	1	9.0	3.6	0.1	3.2	9.0	:
		L-T	Mean	96.7	86.4	ı	45.3	76.6	:	6.09	76.3	76.8	60.1	6.0.8	:
		L	=	2	6	ij	7	2		2	9	2	2	2	÷
			Min Spec Thk	09:0	1.00	i	0.80	0.80		0.60	1.00	0.60	09'0	09:0	1
Range of	Product	Thickness	(1111)	0.62	6.00	0.62	1.00	1.00	1.00	0.62	10.00	0.62	0.62	0.62	0.62
	Product	Form		Forged Bar	Billet	Plate	Plate	Plate	Plate	Forged Bar	Billet	Forged Bar	Forged Bar	Forged Bar	Plate
	Condition/	Heat Treatment		1600F 1HR OQ 535F 1HR	1650F 111R AC 1576F 111R OQ 800F 2+211R	HEAT TREATED TO 46 RC HARDNESS	1650F OQ TEMPERED 500F	1550F OQ TEMPERED 800F	1600F 1HR 1525F 2.5HR OQ AT 150-176F 900F 1HR	1600F 11IR OQ 535F 11IR	1650F 11IR AC 1625F 11IR OQ 800F 21IR	2190F 11IR FC TO 1600F HOLD 0.5HR 400F 1HR	2190F 1HR FC TO 1600F HOLD 0.5HR 535F 1HR	2190F 1HR FC TO 1600F HOLD 0.5HR 660F 1HR	HEAT TREATED TO 51 RC HARDNESS
	Allov				4330V (MOD)						C C C C C C C C C C C C C C C C C C C	OFF			

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF ALLOY STEELS AT ROOM TEMPERATURE

$K_{Ic}~(Ksi\sqrt{in})$	Specimen Orientation	T-L S-L	n Mean Std Spec n	:	1.00 4 66.3 6.2	:	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.25 3 105.6 4.8	2 136.7 7.4	.00 6 78.4 15.1 0.97 52 83.9 14.8	: : : : : : : : : : : : : : : : : : : :			
le (Ksi√in)	nen Orientatio	T.L	Mean	i	66.3	:	1	105.6	136.7	78.4	ı	1	1	
K	Specin		Min Spec Thk	:	1:00			1.25	1.75	00:1	:	1	;	
		F.	Mean Std	40.5 0.5	:	51.0 3.0	65.0 4.4	98.7 11.3	139.6 11.7		78.5 4.7	80.3 0.8	66.9 18.7	
		L-T	u	က	:	2	80	æ	2 1	ŀ	2	2	2	
			Min Spec Thk	0.90	!	0.90	0.90	1.25	1.76	i	1.00	1.00	0.75	
Range of	Product	Thickness	(in.)	4.00	1.00	4.00	4.00	6.75	2.00	09:9	7.00	7.00	0.80-1.50	-
	Product	Form		Forging	Billet	Forging	Forging	Forging	Plate	Forging	Billet	Billet	Plate	ł
	Condition/	Heat Treatment		1600F 1HR AC 1550F 1HR OQ -320F 0.5HR 400F 2HR AC	1550F OQ 900F 1HR	1600F 1HR AC 1550F 1HR OQ -320F 0.511R 400F 2HR AC	1600F 1HR AC 1660F 1HR OQ -320F 0.5HR 400F 2HR AC	Unspecified	1650F 111R WQ 1500F 111R WQ 950F 5HR AC	1616F 2.25HR A-BQ 326F AC 310-346F 3HR 1080F 6-6.5HR	1650F 1HR FC 1650F 1HR OQ 1025F 2+2HR	1650F 1HR FC TO 960F OQ AT 150F AC 1000F 2+2HR	1650F AUS-BAY QUENCH 976F SQ 1000F 2+2HR	1650F AUS-BAY QUENCH 976F SQ
	Alloy	•		4340 (AM)		4340 (DH)	4340 (VAR)	1	AF1410			D6AC	. 1	

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF ALLOY STEELS AT ROOM TEMPERATURE

			y					K	Ic (K	K_{Ic} $(Ksi\sqrt{in})$					
11 4	Condition/	Product	Product					Specimen Orientation	nen (rient	ation				
Alloy	Heat Treatment	Form	Thickness		L-T	T			T-L	اد			62	S-L	
			(III.)	Min Spec Thk	E .	Mean	Std	Min Spec Thk	E	Mean	Std	Min Spec Thk	£	Mean	Std
11	1650F AUS BAY QUENCH 976F SQ 376F 1000F 2+2HR	Forging	1.50	0.75	8	46.0	4.2	1	1	į	i	ı	i	ı	ı
1 -	1650P A 119-BAV OTTENCIT 975P SO	Plate	08'0	09'0	103	64.4	12.1	:	i	1	ı	:	-	ŀ	::
	400F 1000F 2+2HR	Forging	0.80-1.50	09:0	63	66.2	12.3	!	ï	1	:	!	1	:	;
	1700F 1HR FC TO 960F OQ AT 150F AC 1000F 2+2HR	Billet	7.00	1.00	ဇ	80.3	4.3	:	i	ı	ı	1	i	ı	1
l	1700F 1HR OC 1025F 2+2HR	Billet	7.00-10.00	1.00	9	77.3	2.6	· i	i	1	1	:	;	1	1
<u> </u>	AND ALIS BAY OHENCH 926F OO	Plate	0.80-1.50	19.0	8	92.0	8.2	:	1	:	1		:	i	:
7 7 7 7	140F 1000F 2+2HR	Forging	0.80-1.50	0.75	34	96.2	6.4		-	1	i	1	;	1	ı
(Cont'd)	1725F 1HR AC 1700F 1HR OQ 1000F 1HR 1015F 1HR	Billet	7.00	1.00	3	77.2	2.7		ı	I	ì	ŀ	i	ı	ì
1	1725F 11IR AC 1700F 1HR OQ 1025F 2+21IR	Billet	7.00-10.00	1.00	9	74.4	6.2		ı	;	1	i	1	l	ı
	1725F 1HR AC 1700F 1HR OQ 1100F 2+2HR	Billet	7.00.10.00	1.00	9	101.2	6.1	:	ı	!	ı	!	:	!	ı
	1725F 1HR AC 1750F 1HR FC TO 960F SQ 350F 0.5HR AC 1025F 22HR	Billet	7.00	1.00	3	75.1	10.1	ŀ	i	į	ŀ	I		I	i
	HEAT TREATED TO 46 RC HARDNESS	Plate				ı	!	0.70	2	85.8	1.8	-	-	1	ı

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF ALLOY STEELS AT ROOM TEMPERATURE

	7			T			1									
			Std Dev	i		ı	ı		ï		÷	i	1	ı	ı	ï
		S-L	Mean		ì	I	1	i	1		•••		-	-	ı	ì
		G 2	ď	;	:	:	:	;	1	i		!	i	i	i	i
			Min Spec Thk	:	:	1	ı	1	1	ı	:	ı	ı	-	:	-
	ation		Std Dev	16.8	2.0		L'\$	i	1.8		1	ı		ı	1.9	6.6
$K_{Ic}~(Ksi\sqrt{in})$	Specimen Orientation	T-L	Mean	136.3	111.7	1	109.7	ŧ	126.3	ı		I	ŀ		111.7	132.3
Le (J	nen	T	ц	2	2		ဗ	i	9	1	i	I	i		3	7
K	Specin		Min Spec Thk	2.00	1.50		1.76		191			:	;	1	2.00	1.46
			Std Dev	4.6	:	12.0	12.3	29.0	11.6	3.9	3.5	4.4	0.7	0.7	7.3	4.5
		L-T	Mean	150.6	i	123.5	134.8	121.5	135.2	133.2	125.5	. 94.4	128.6	140.5	120.6	140.7
		T	u	2	:	2	6	2	15	5	2	3	2	2	12	10
			Min Spec Thk	2.00	÷	2.00	1.75	2.00	1.61	1.50	1.66	1.24	1.69	1.60	1.00	1.50
Bango of	Product	Thickness	(IB.)	1.25	4.00	2.50	4.00-7.00	2.50	4.00	1.70.3.25	4.00	4.00	4.00	4.00	3.00	3.40-7.00
	Product	Form		Forging	Forging	Plate	Forging	Plate	Forging	Forging	Forging	Forging	Forging	Forging	Forging	Forging
	Condition/	Heat Treatment		Unspecified	1525F OQ -100F 1HR 1065F 4+4HR	1650F 1-2HR AC 1-2HR 1-2HR AC -100F 1.6HR 1025F 4HR 1060F 4HR	1650F 1-211R AC 1525P 1-21IR OQ -100F 1-211R 1025F 411R	1650F 1-211R AC 1525F 1-211R 09	-100F 2HR 1025F 4-6HR	1650F 1-2HR AC 1626F 1-2HR OQ -100F 2HR 1050F 4-6HR	1650F 1-2HR ACX	1650F 2HR AC 1525F 2HR OQ 1000F 2+2HR AC	1650F 4.5HR AC TO 900F HELD 0.5HR AC -100F 1.5HR 1025F 8HR A-BQ	1700F 4.5HR AC 1700F 1.5HR AC -100F 1.5HR 1025F 4HR	ANNEALED	HEAT TREATED
	Allow									HP9.4.20						

TABLE 3.0.2 (CONCLUDED)

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF ALLOY STEELS AT ROOM TEMPERATURE

									,	
			Std Dev	ŀ	-		ŧ	i	:	-
		S-L	Mean	1	i	i	ı	i	:	-
		02	£	;	!	:	1	!	;	1
			Min Spec Thk	1	:	i	I	i	-	;
	tation		Std Dev	4.6	3.0	0.7	9.0	ı	6.0	2.1
$K_{Ic}~(Ksi\sqrt{in})$	Specimen Orientation	T-T	Mean	98.9	89.0	93.5	87.6	1	82.5	111.5
ζ_{le} (1	men	T	u	2	3	2	2	i	2	2
I	Speci		Min Spec Thk	2.00	1.00	1.00	1.00	!	1.01	1.00
			Std Dev	1	1.4	1	ı	0.0	1	!
		L-T	Mean	ŧ	106.0	ŀ	I	82.0	i	i
		L	п	i	2			2		
			Min Spec Thk	:	1.00			2.02	:	
Rango of	Product	Thickness	(III.)	3.00	3.00	3.00	3.00	3.25	3.25	6.50
	Product	Form		Forging	Forging	Forging	Forging	Forging	Flate	Forging
	Condition/	Heat Treatment		1550F 111R OQ 1000F 2+2HR AC	1650F 1-2HR AC 1625F 1-2HR OQ -100F 1-3HR 1000F 4HR	1650F 1-2HR AC 1626F 1-2HR OQ -100F 1-3HR 1025F 4HR	1650F 1-2HR AC 1625F 1-2HR OQ -100F 1-3HR 1050F 4HR	1650F 2HR AC 1650F 2HR OQ 1000F 2+2HR AC	HEAT TREATED TO 49 RC HARDNESS	1700F 1HR AC 1600F 1HR OQ 650F 2HR
	Allow	· ·		HP9-425(VAR)			HP9.4.30			HY-TUF

TABLE 3.0.3

PLANE STRESS AND TRANSITIONAL FRACTURE TOUGHNESS OF ALLOY STEELS (WITHOUT BUCKLING CONSTRAINTS)

		Ę		Specimen	F1 - 20.						K _c (Ksk∕in)	sk/in)					
Alloy	Condition/ Heat Treatment	Temp (°F)			riela Strength (Ksi)		n - S	ample	S _l size	pecim	en Th Mean	Specimen Thickness (in.) n Sample size μ · Mean σ · Standard Deviation	ss (in.	ardI	evia	tion	
			Orient	Width (in.)		0	0.025			0.1			0.125			0.2	
						u	=1	ь	_	=	ь	٦	=	ь	c	=	6
		-423.	LT	4.0	86.0	9	86.4	7.2									
		320	F	2.0	36.0	9	142.6	7.3									
BNEGOCKMARI	in an and it			4.0	36.0	9	124.2	8.0	H								
				2.0	77.0	9	132.1	4.3									
		R.T.	1. 1	4.0	77.0	9	128.4	3.8									T
				18.0	77.0	*	109.8	8.9	-								

TABLE 3.0.4.1

FOR ALLOY STEELS IN LAB AIR AT ROOM TEMPERATURE FATIGUE CRACK GROWTH RATE (FCGR) COMPARISON AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK

	100.0		
Hz	00	37.13	18
FREQUENCY: 1 - 30 Hz	FCGR (10.4 trycycle) A.K. Lovel (Ksiv/in) 10.0 20.0 5	4.2	4.4
QUENC	C. Lovel		
FRE	FC AA		
	2.5		
98	FREQ (Hz)	10-30	1-30
STRESS RATIO: 0.08	R	0.08	0.08
STRESS	PRODUCT	PLATE	PLATE
ORIENTATION: UNSPECIFIED	CONDITION/ HEAT TREATMENT	AIR QUENCHED	OIL QUENCHED
ORIENTA	ALLOY	A 134440	AF 1410

TABLE 3.0.4.2

FATIGUE CRACK GROWTH RATE (FCGR) COMPARISON AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK FOR ALLOY STEELS IN LAB AIR AT ROOM TEMPERATURE

STRESS RATIO: -1.0 - 0.8

ORIENTATION: L-T

FREQUENCY: 0.1 - 30. Hz

AO LIV	INOLLIGINOS	THE STATE OF THE				FC	10 HOR	PCGR (10 * tr/gde)	•	
Tomwar and Town	HEAT TREATMENT	FORM	Ħ	HE (HZ)		ΔK	Love	ΔK Level (Kai√in)	(2)	
					2.5	e s	10.0	20.0	50.0	100.0
19 0 9 14 4 10	OU ATTA	מ אינו מימינים	0.1	10				8.17		
WUM 7-0-71	008 W10	KOUND BAK	0.1	30			0.15	8.92		
			-1	10				3.65	38.07	
	UTS=280.300KSI	BAR	0.02	10				3.52	47.71	
300M			0.5	10			1	6.55		
	Taran Sadora	CAMPROCA	0.02	1-15			99'0	4.24		
	ONSFECIFIED	FORGING	0.02	0.1-20			0.67	4.26	104.94	
4330V (MOD)	UNSPECIFIED	BILLET	0.02	1-30			1.98	7.29	27.92	
	MARTEMPERED	PLATE	0.02				0.52	3.06	22.98	115.4
	107704 - 1011	FORGING	0.1	30	,	0.02	0.28	2.44		
	O LOS LBONDAI	UNSPECIFIED	-0.1	2-5			0.44			
			0.1	7				2.47		
4340	UTS=160KSI	ROUND BAR	0.5	7			19:0	3.6		
			0.5	7		0.09				
		•	0.1	20				2.69	30.66	
	UTS=160-180KSI	BAR	0.5	20		0.09	0.64	3.9	34.11	
			9.0	20			99'0	4.16		

FOR ALLOY STEELS IN LAB AIR AT ROOM TEMPERATURE FATIGUE CRACK GROWTH RATE (FCGR) COMPARISON AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK

100.0 151.39 0.03 32.69 51.35 27.26 23.41 31.4865.2 FREQUENCY: 0.1 - 30. Hz AK Level (Ksiylin) PCGR (10 * tr/cycle) 20.0 2.85 2.89 1.59 3.88 9.59 5.61 2.62 3.4 3.6 10.0 0.42 0.65 0.65 0.35 0.58 9.6 6.0 0.11 0.03 90.0 0.09 . . FREQ (Hz) 0.1-30 20-30 0.1 ဓ္က 9 20 30 STRESS RATIO: -1.0 - 0.8 0.08 0.05 0.02 0.5 0.1 0.1 0.0 0.1 0.5 0.1 0.6 0.1 2 0.1 PRODUCT FORM ROUND BAR ROUND BAR FORGING PLATE PLATE PLATE PLATE 1800F 0.5-1.0 HR WQ 1325F 16HR AC 1660F 1HR WQ 1500F 1HR WQ 950F 5HRS AC 1525F 1HR AC -100F 1HR AC 950F 5HRS AC 1650F A-BQ AT 975F SQ AT 400F 1000F 2+2HR 1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS CONDITION/ HEAT TREATMENT UTS=180KSI ORIENTATION: L-T AF1410(VIM-VAR) ALLOY 4340 (Cont'd) AF1410 D6AC A286

TABLE 3.0.4.2 (CONCLUDED)

FATIGUE CRACK GROWTH RATE (FCGR) COMPARISON AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK FOR ALLOY STEELS IN LAB AIR AT ROOM TEMPERATURE

ORIENTATION: L-T STRESS RATI

STRESS RATIO: -1.0 - 0.8

FREQUENCY: 0.1 - 30. Hz

			100.0					125.87									
	•	(a)	0.00					18.9	33.15	37.05	37.38	46.37	46.57	30.82			
	^o in/ayd	(Kat/,	20.0	3.53	2.95	4.94	4.93	1.61	3.58	6.33	2.97		3.59	4.29	3.72	5.61	4.5
1 233	PCGR (10 ^d tr/cycle)	ΔK Level (Ksk/in)	10.0		0.34		0.72	0.18			0.41				0.48		0.53
,	PC	ΔK	5.0				0.09								0.11		0.11
			2.5														
		FREQ (Hz)		10	30	10	30	0.1-20	10	5-10	5-20	1	10	10	30	10	30
		R		0.1	0.1	0.5	0.6	0.02	0.02	0.1	0.02	0.02	0.02	0.1	0.1	0.5	0.5
		PRODUCT FORM				ROUND BAK		FORGING	BAR	FORGING	FORGING		BAR			FORGED BAR	
		CONDITION/ HEAT TREATMENT			AUSTENIZED & TEMPERED	(TYS=220KSI)			ONSPECIFIED	ANNEALED		UNSPECIFIED				STA (UTS=180KSI)	
		ALLOY			,	НП			HF9-420	HP9-420(CEVM)		HP9-430				HY-180	

TABLE 3.0.4.3

AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK FOR ALLOY STEELS IN LAB AIR AT ROOM TEMPERATURE FATIGUE CRACK GROWTH RATE (FCGR) COMPARISON

					FC	KGR (10	FCGR (10 4 tr/cycle)	(e	
CONDITION/ HEAT TREATMENT	PRODUCE	R	FREQ. (Hs)		ΔK	Lovel	(Ksk/	(n)	
				2.5	5.0	10.0	20.0	60.0	100.0
UTS=243KSI	BILLET	0.1	10			1.16	16.91	71.03	
UNSPECIFIED	FORGING	0.02	0.1-20		0.14	0.7	4.35	156.19	
1800F 0.5-1.0 HR WQ 1325F 16HR AC	PLATE	0.05	3				1.82		
1626F 1HR AC -100F 1HR AC 950F 5HRS AC	ROUND BAR	0.02	0.1-30		0.11	89'0	3.64	31.7	172.61
		0.08	1-30			0.71	3.95	29.34	
3 WQ 1500F 1HR WQ 950F	STEEL VICE	0.08	1-30			0.71	3.95	29.34	
6HRS AC	FLAIE	0.3	10-30			1.11	5.35	36.14	
		0.3	10-30			1.11	5.35	36.14	
UNSPECIFIED	FORGING	0.02	0.1-20			0.24	2.99	30.69	489.57
UNSPECIFIED	FORGING	0.02	0.1-20			0.48	3.14	49.14	1733.09
######################################	UTS=243KSI UNSPECIFIED 1800F 0.5-1.0 HR WQ 1325F 16HR AC 1526F 1HR AC -100F 1HR AC 950F 5HRS AC UNSPECIFIED UNSPECIFIED UNSPECIFIED		BILLET FORGING PLATE ROUND BAR PLATE FORGING FORGING	HORGING 0.02 PLATE 0.02 ROUND BAR 0.02 ROUND BAR 0.02 0.08 PLATE 0.3 PLATE 0.3	HOHLM BILLET 0.1 10 FORGING 0.02 0.1-20 ROUND BAR 0.08 1-30 0.08 1-30 0.08 1-30 0.08 1-30 0.08 1-30 0.08 1-30 FLATE 0.08 1-30 0.09 1-30 0.09 1-30 FORGING 0.02 0.1-20	FORGING 0.02 0.1-20 0.1 FORGING 0.02 0.1-20 0.1 PLATE 0.05 3 0.1-30 0.1 ROUND BAR 0.02 0.1-30 0.1 O.08 1-30 0.1 O.08 1-30 0.1 O.08 1-30 0.1 FLATE 0.3 10-30 0.1 O.09 0.02 0.1-20 0.1 FORGING 0.02 0.1-20 0.1 FORGING 0.02 0.1-20 0.1	FORGING 0.02 0.1-20 0.1 FORGING 0.02 0.1-20 0.1 PLATE 0.05 3 0.1-30 0.1 ROUND BAR 0.02 0.1-30 0.1 O.08 1-30 0.1 O.08 1-30 0.1 O.08 1-30 0.1 FLATE 0.3 10-30 0.1 O.09 0.02 0.1-20 0.1 FORGING 0.02 0.1-20 0.1 FORGING 0.02 0.1-20 0.1	HORINA 0.01 10 2.5 5.1 5.1 10	FORKING CHR) CHR) CAR LAVE CRR/IN CR

TABLE 3.0.5

	STRESS CORROSION CRACKING THRESHOLD DATA FOR CTEFT	ACKING	THRESH	TAN OLIV	A EOD CT	NEW T			_
	ALLOYS AT ROOM TEMPERATURE	T ROOM	M TEMPE	RATURE	A FOR SI	Taa			
					K_{Iscc}	K_{Iscc} (Ksi \sqrt{in} .)			
ALLOY	CONDITIONAL	PRODUCT	BPECIMEN		ENV	ENVIRONMENTS			_
				SIMULATED SEA WATER	SEA WATER	DISTILLED	8.6 % NACL	SUMP TANK WATER	
5	1650p AQ 650p 41ir	Sheet	LT			7.0			_
Deac	1550F AQ 950F 4IIR	Sheet	LT			46.2			
	GTA Weld	Plate	:	65.0					_
-	Quenched and Tempered	Plate					110.0(2)		+
	1625F 2IIR OQ	E	L-T					105.0(3)	7
HP9-420	TOOF AIR	Finte	T-L					97.4(5)	
 			LT					110.0	
		Forged Bar	T:L					107.0(2)	
			S-T					78.3(3)	_
HP9-446	476F	Plate	•				20.0		
H-11	Quenched and Tempered at 1100F	Plate	••				30.0		
	Electric Furnace	Plate	***	40.0					
	GTA Welded	Weldment	:	33.0					T
 12Ni-5Cr-3Mo	Low Residual	Plate		108.0					T
	1650F, 900F 20HR AC		L-S				80.0		_
		Plate	T.S				70.0		1
									3

	STRESS CORROSION CRACKING THRESHOLD DATA FOR STEEL ALLOYS AT ROOM TEMPERATURE	ACKING T ROOF	JON CRACKING THRESHOLD DAY	OLD DAT	A FOR ST	EEL		
					K_{Iacc}	K_{Isoc} (Ksi \sqrt{in} .)		
ALLOY	CONDITION/HT	PRODUCT	SPECIMEN ORIENTATION		ENV	ENVIRONMENTS		
				BIMULATED SEA WATER	SEA WATER	DISTILLED WATER	8.6 % NACL	SUMP TANK WATER
	TYS = 178 KSI	Plate	***	108.0				
. 18Ni(180KMAR)	TYS = 196 KSI	Plete	1				60.0	
	TYS = 200 KSI	Plate	ı				105.0	
	TYS = 216 KSI	Plate					70.0	
	Weld Center Line	Plate	6-7				70.0	
18Ni(200XMAR)	1500F 1HR AC 900F 3HR	Plate	T-S				39.0	
	1676F 2HR AC	Plate	T-9				48.0	
	600F 0.25IIR 850F 4IIR/cool 250F/min	Weldment	T.S				78.0	
	AGE 900F 3HR AC	Ę	L.S				40.5(2)	
		Linke	LT				45.0	
18Ni(250XMAR)	TYS = 250 KSI	Plate					60.0	
	TYS = 260 KSI	Plate		-			70.0	
	1650F 1.25IIR WQ 1525F 1.25 HR WQ 900F 3HR AC	Plate		36.7				
18Ni(280XMAR)	1600F 1HR AC 900F 3HR	Plate					14.0	

	STRESS CORROSION CRACKING THRESHOLD DATA FOR STEEL ALLOYS AT ROOM TEMPERATURE	ACKING T ROOM	THRESH M TEMPEI	OLD DAT	A FOR ST	BEL		
		·			K_{Igcc}	K _{Iscc} (Ksi√in.)		
ALLOY	CONDITION/HT	FORM	SPECIMEN		ENV	ENVIRONMENTS		
				SEA WATER	BEA WATER	DISTULED WATER	8.5 % NACL	BUMP TANK WATER
	AGED 900F 6IR	1	LT				7.0	
		rotking	T-L				6.0(2)	
	AGED 960F 121IR	Forging	T.L				6.0	
	Crack Prestressed to 50 PCT KIC	Forging	T.L				6.0	
IBNICORONABA	Crack Prestressed to 25 PCT KIC	Forging	T-L				6.0	
(ATTURNOON TO THE TOTAL THE TOTAL TO THE TOTAL THE TOTAL TO THE TOTAL THE TOTAL TO THE TOTAL TOT	Crack Prestressed to 80 PCT KIC	Forging	T.L				10.0	
	1600F 0.5HR AC 900F 3HR	Plate	Ls			48.0(2)		
	1500F 21IR 800F 10 HR	Bar	L.S			9.0		
	1700F, 1500F AGED 900F 6HR	Forging	T-L				7.5	
	900F 3HR 950F 3HR	Forging	T.L				5.0	
	AGE 800F 8HR	Forged Bar	ì				6.0	
	AGE 900F 3HR	Forged Bar	:				10.0	
18NIGSOVMAR)	AGE 900F 8HR	Forged Bar	:				10.0	
	1500F 1HR 800F 8HR	Forging	F-1				6.0	
	1500F 11IR 900F 8IIR	Forging	L-S				10.0	
	1600F 1HR 960F 3HR	Forging	L-S				10.0	

	STRESS CORROSION CRACKING THRESHOLD DATA FOR STEEL ALLOYS AT ROOM TEMPERATURE	CKINC F ROOF	THRESH A TEMPEI	OLD DAT	A FOR ST	EEL		
					$K_{I_{BCC}}$	K_{Isc} (Ksi \sqrt{in} .)		
ALLOY	CONDITIONAL	PRODUCT	BPECIMEN		ENV	ENVIRONMENTS		
				SIMULATED SEA WATER	SEA WATER	DISTILLED WATER	8.5 % NACL	BUMP TANK WATER
	1500F 0.5HR OQ 400F 2+2HR (Coarse Grain)	Plate	1				12.0	
	1500F 0.5HR OQ 400F 2+2HR (Fine Grain)	Plate	•••				12.0	
	1500F 0.51IR OQ 550F 2+21IR (Coarse Grain)	Plate	:				15.0	
	1500F 0.5IIR OQ 550F 2+2IIR (Fine Grain)	Plate	•				15.0	
	1550F 0.5HR OQ 400F 2+2HR (Coarse Grain)	Plate	:				15.0	
	1550F 0.511R OQ 400F 2+21IR (Fine Grain)	Plate					15.0	
	1650F 0.51IR OQ 650F 2+21IR (Coarse Grain)	Plate	1				15.0	
300M	1550F 0.511R OQ 550F 2+21IR (Fine Grain)	Plate	:				15.0	
	1600F 0.5HR OQ 400F 2+2HR (Coarse Grain)	Plate					12.0	
	1600F 0.5HR OQ 550F 2+2HR (Coarse Grain)	Plate	1				12.0	
	1600F 0.5HR OQ 650F 2+2HR (Fine Grain)	Plate	:				12.0	
	1650F, 1600F HR OQ 600F 1+1HR	Forging	L.9				19.6	
	1700F 1.5HR AC 1600F 1.5HR OQ 600F 2+2HR	Forging	8-1.					15.6(2)
	1710F, 1610F 610F	Ē	L-T				17.4(3)	
		Bar	T-L				17.6(4)	
-	1700F 1600F OQ 750 1+1HR	Plate	***			15.0		
	1700F 1600F OQ 600F 1+1HR	Plate	ï			11.0		

	STRESS CORROSION CRACKING THRESHOLD DATA FOR STEEL ALLOYS AT ROOM TEMPERATURE	ACKING T ROOM	THRESE WILL	IOLD DAT	'A FOR ST	EEL		
					K_{Isoc}	K_{Isoc} (Ksi \sqrt{in} .)		
ALLOY	CONDITION/HT	PRODUCT FORM	SPECIMEN		ENV	ENVIRONMENTS		
				SIMULATED SEA WATER	BEA WATER	DISTILLED WATER	8.6 % NACL	BUMP TANK WATER
4330V G	Quenched and Tempered at 500F	Plate	8-7				25.0	
	TYS - 160 KSI	Plate	T:L		69.0			
	TYS = 176 KSI	Plate	T.L		27.0			
<u>- [</u>	TYS = 200 KSI	Plate	T-L		10.0			
	TYS = 225 KSI	Plate	T:L		6.0			
	1350F OQ 750F 1.25HR	Plate	T-8		8.5			
-1	1550F OQ 750F Crack Prestressed to 80 PCT K.	Plate					24.0	
	1550F OQ 750F Crack Prestressed to 60 PCT K.	Plate	i				23.0	
	1650F OQ 750F Crack Prestressed to 40 PCT K.	Plate	i		,		17.0	
4340	1550F OQ 750F Crack Prestressed to 20 PCT K.	Plate	:				12.0	
<u>.71</u>	1650F OQ 750F 1HR	Plate	:				8.0	
<u>-1</u>	1676F OQ 676F 411R	Plate	:			8.6		
-1	1575F OQ 800F 411R	Plate	•			9.6		
<u>-1</u>	1600F 1 HR OQ 600F 1+1HR	Forging	•				10.0	
	1650F 111R AC 1680F 21IR OQ LN 0.25HR 406F 1+1HR OQ	Bar	LT				15.0	
<u>-1</u>	1650F 1HR AC 1480F 2HR OQ LN 0.25HR 406F 1+1HR OQ	Bar	LT				15.0	
<u>-1</u>	1700F 0.25HR AC 1660F OQ 600F 1+HIR	Sheet	:				29.0	
	1800F Q 600F 1+1HR	Forging	L-S				26.2(12)	

TABLE 3.0.5 (CONCLUDED)

	STRESS CORROSION CRACKING THRESHOLD DATA FOR STEEL ALLOYS AT ROOM TEMPERATURE	ACKING T ROO	3 THRESH M TEMPEI	OLD DAT	A FOR ST	BEL		
					K_{Iacc}	K_{Isoc} (Ksi $\sqrt{in.}$)		
ALLOY	CONDITION/HT	PRODUCT	SPECIMEN		ENV	ENVIRONMENTS		
				BIMULATED SEA WATER	BEA WATER	DISTILLED WATER	8.5 % NACL	BUMP TANK WATER
	1650F 1HR 1600F 1HR OQ 1+1 600F (0.09 SI)	Bar	T.L				18.0	
	1650F 1HR 1600F 1HR OQ 1+1 400F (0.09 SI)	Bar	T-L				13.0	
	1800F Q 460F 1+1HR (0.20C)	Forging	L-S				56.0	
	1800F Q 500F 1+1HR (0.21C)	Forging	L-8				52.0	
	1800F Q 600F HIR (0.20C)	Forging	1.8				72.0	
GON 6767	1800F Q 650F 1HR (0.24C)	Forging	L-8				62.0	
TOW OFF	1800F Q 650F 1HR (0.28C)	Forging	L9				35.0	·
	1800F Q 700F 11IR (0.21C)	Forging	гs				42.0	
	1800F Q 780F 1+1HR (0.33C)	Forging	LS				32.0	
	1800F Q 800F 1HR (0.46C)	Forging	IS				20.0	
	1800F Q 900F 1HR (0.64C)	Forging	LB				30.0	
	1800F Q 926F 1+11IR (0.53C)	Forging	E-1	-			42.0	

TABLE 3.1.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 10NI STEEL AT ROOM TEMPERATURE

ORIENTATION: L-T

ENVIRONMENT: Dry Air

			100.0					
(of		J.	60.0	25.18	22.92			
d in/cyc		(Ksk/ii	20.0	3.9	5.2	5.21	5.02	5.73
PCGR (10 ⁻⁸ in/cycle)		ΔK Level (Ksk/in)	10.0	0.45		0.8	0.88	0.84
FC		4	6.0				0.12	0.13
			8.9					
	FREQ	(Hz)		9	9	9	8	9
	¢	1		0.1	0.1	0.3	0.5	0.7
	PRODUCT	FORM				PLATE		
	CONDITION/	HEAT TREATMENT				UNSPECIFIED		

TABLE 3.1.1.2.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK 10NI STEEL AT ROOM TEMPERATURE

ORIENTATION: L-7	4: L-T			ENVIRONMENT: S.T.W.	NME	T.S.T.	×.		
GONDITION/ HEAT TREATMENT	PRODUCT FORM	Я	FREQ (Hz)		FCC	FCGR (10 ^d in/cycle) AK Level (Ksk/in)	^B in/cyc (Ksk/ii	[b]	
				2.5	5.0	10.0	20.0	50.0	100.0
		0.1	0.1					49.13	
UNSPECIFIED	PI.ATR	0.1	1			0.11	2.92	40.39	
		0.5	0.1			1.53	13.72	77.81	
		9.0				0.47	7.31	37.14	

TABLE 3.1.1.2.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 10NI STEEL AT ROOM TEMPERATURE

	100.0	131.22
	20.0	33.03
	FCGR (10 ⁻⁶ in/cycle) AK Level (Ksi/in)	2.21
ENVIRONMENT: S.T.W.	CGR (10 ⁻⁶ in/cycle AK Level (Ksi/in)	
MENT	FCGR AK I	
TRON	2.8	
ENV		
	FREQ (Hz)	1
	R	0.1
	ЭT	
	PRODUCT FORM	PLATE
V: T.L	PI	
ORIENTATION: T.	INI	
RIENT	CONDITION/ HEAT TREATMENT	IFIED
Ō	ONDI I TRE	UNSPECIFIED
	C	

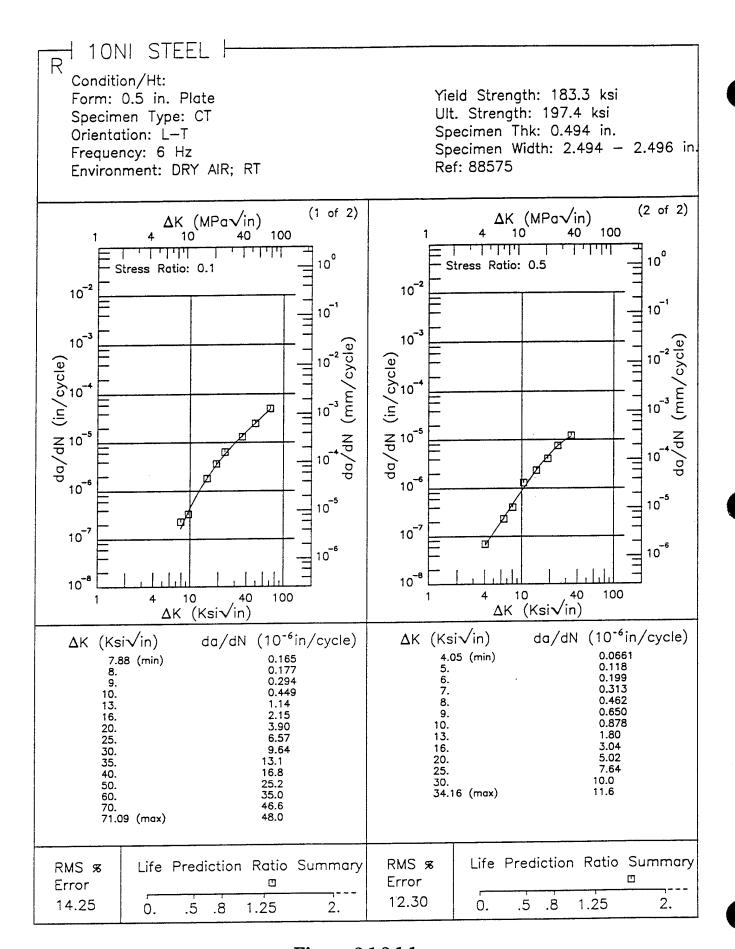


Figure 3.1.3.1.1

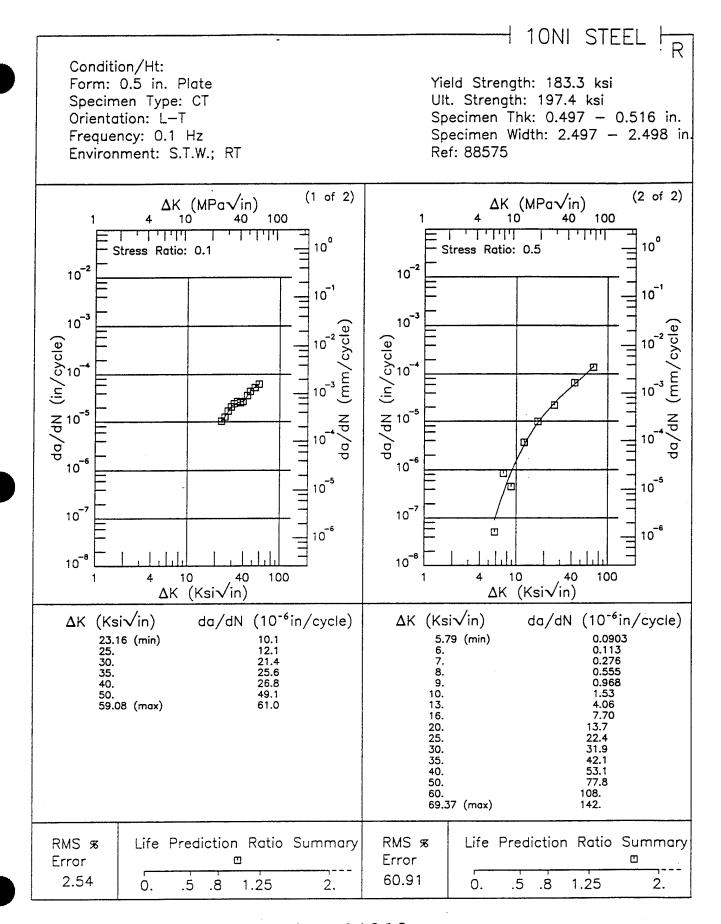


Figure 3.1.3.1.2

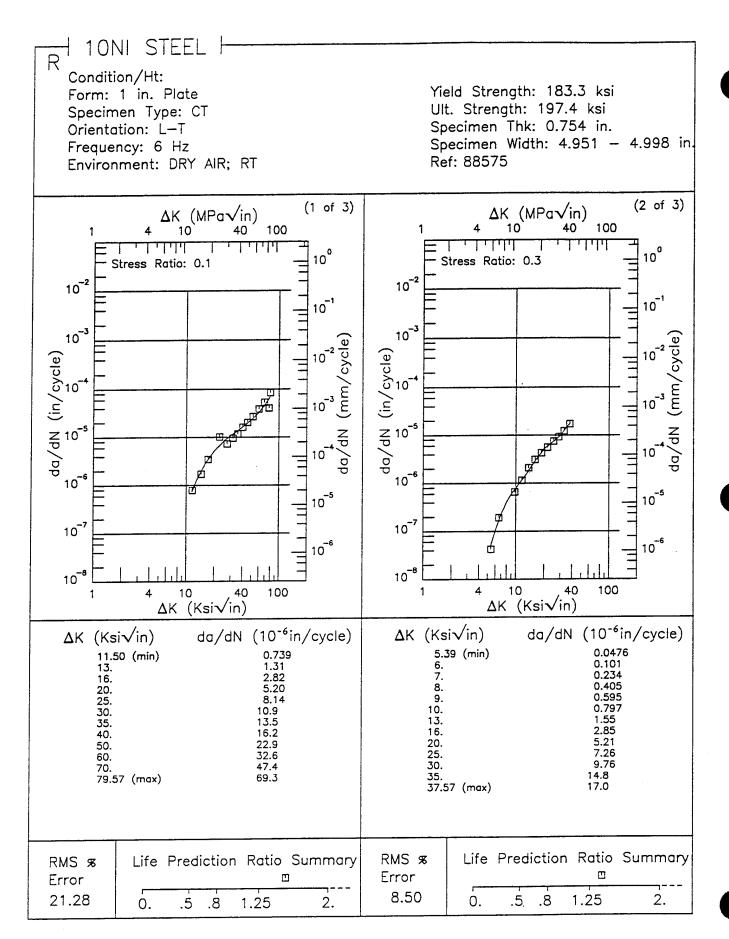


Figure 3.1.3.1.3

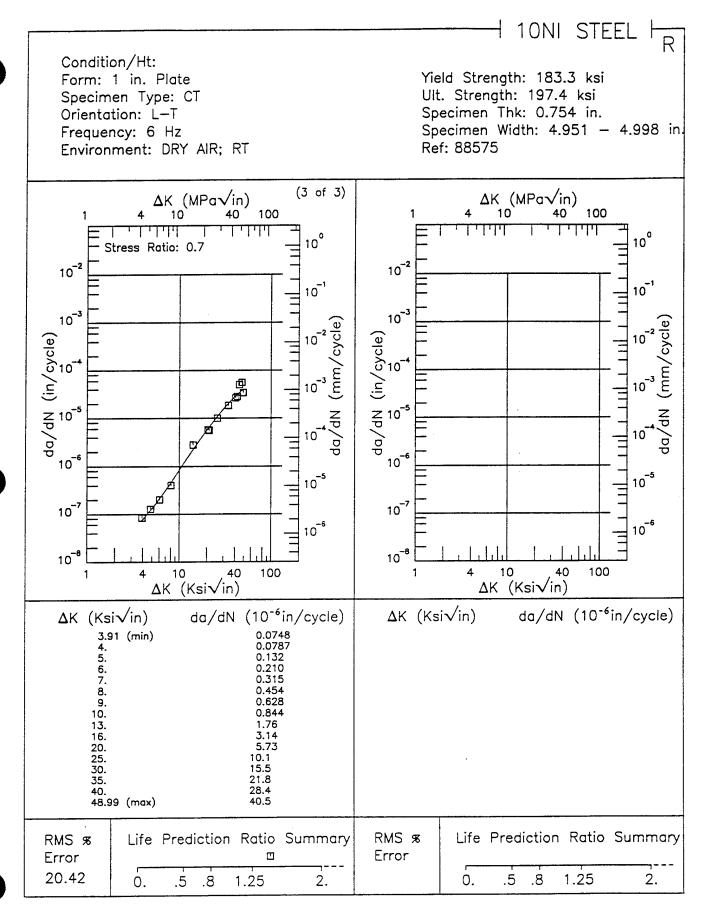


Figure 3.1.3.1.3 (Concluded)

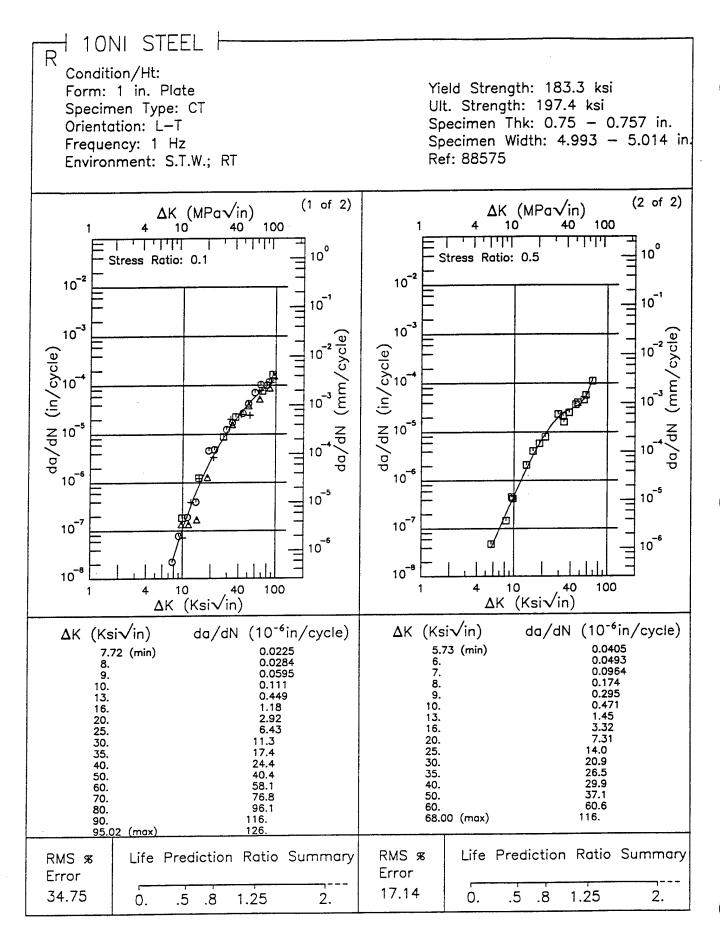


Figure 3.1.3.1.4

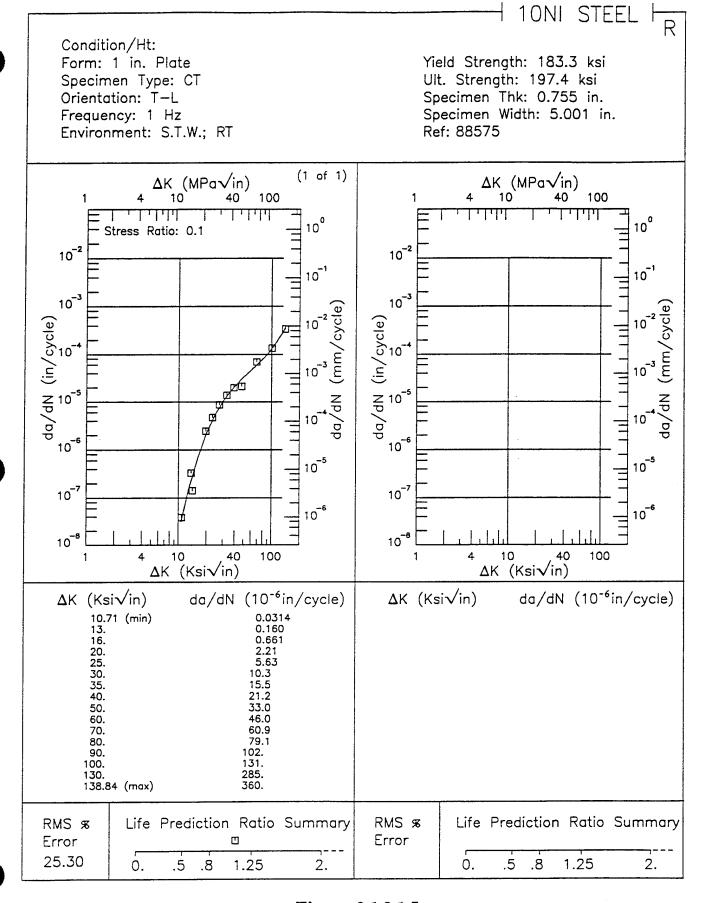


Figure 3.1.3.1.5

TABLE 3.2.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 12-9-2 MAR AT ROOM TEMPERATURE

ENVIRONMENT: Lab Air

ORIENTATION: L-T

	100.0			
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		HE		
		HEAT TREATMENT		

					ALLOY STEEL	TEEL	12-9-2	12-9-2 (MAR)	.) K _{Ie}						
	PRODUCT	UCT					SPECIMEN	z	CRACK			K _{Ie}			
CONDITION	FORM	THICK (in.)	TEST TEMP (FF)	SPRC OR	YTRLD BTR (Kal)	WIDTH (in.)	THICK (IB.)	DESIGN	LENGTH (fa.) A	(K. TY8)* (In.)	R. Sei e (giè	R. MRAN	STAN	DATE	RBFER
STA 900	Round Ber	3.00	R.T.	LT	251.3	2.005	0.968	CT	0.942	90'0	29.60	ı	,	1979	DA001

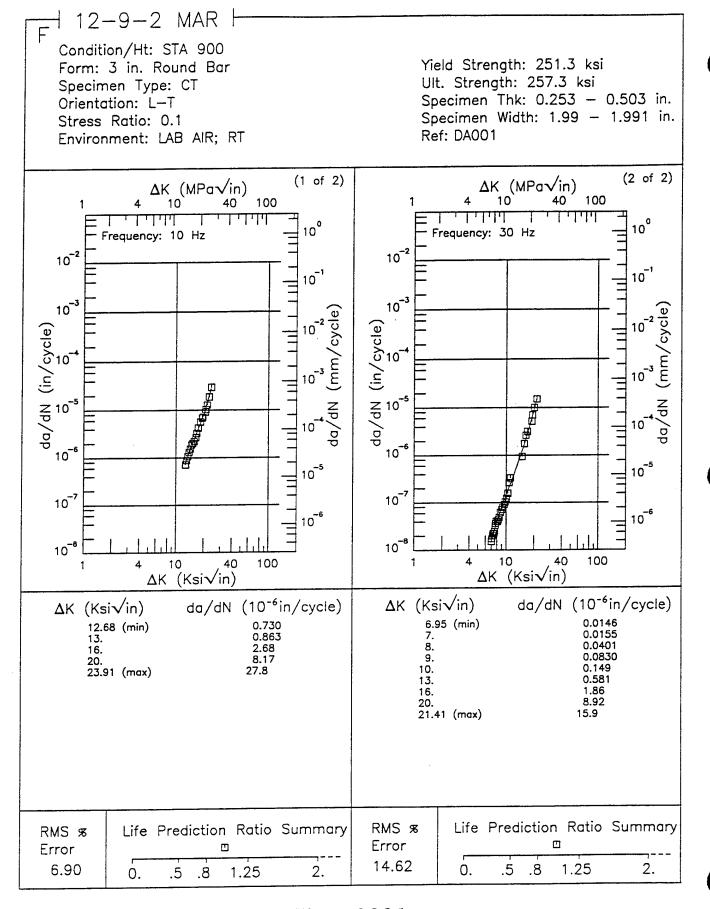


Figure 3.2.3.1

TABLE 3.3.3.3

K_{Isco} SUMMARY FOR ALLOY STEEL 12Ni-5Cr-3Mo

	·	Test		Yield		Sc	Specimen		Prod				Toat		
Condition/ Heat Treat	Form	Temp (°F)	Spec Or.		Envir.	Design	Width (in)	Thick (in)		Crack (in)	Ko (Ksi√in)	K _{law} (Ksivin)	Time (min)	Test Date	Reference
11		£		1	Syn. Seawater	CANT	***		i	i		38	:	1969	74232
Onspecified	i	K. I.	:	184	Syn. Seawater		1	:	i	i	•	20	i	1969	74232
Unspecified			T-S	185	3.5% NaCl	CANT		1			135	83	4800	1967	70887
				Ì		.TOM	3.2	1		1.52	95.8	43.6	:	1969	84317
	f	Ę		183	3.5% INBCI	CANT.	-		-	;	138	44	i	1969	84317
Unspecified	بد	ж. Т.	:	3	***********	JOW.	3.2	1	1	1.52	85	52	į	1969	84317
				190	3.5% NaCi	CANT.		1	1		123	90		1969	84317
1500° F 900° F	,	E G	L-S	176	3.5% NaCl	CANT.	2.5	0.5	-	:	249	80	1	1970	84342
20hr AC	Ъ	K.T.	T-S	176	3.5% NaCl	CANT.	2.5	9.0	1		246	20		1970	84342
Electric Furnace	Ъ	R.T.		176	Syn. Seawater	CANT.	1		-	ŀ	130	40	00009	1966	65166
GTA Welded	W	R.T.	:	178	Syn, Seawater			•	***			33		1969	74232
Low-residual	P	R.T.		183	Syn. Seawater	CANT.	1	#1	1	1	169	108	60000	1966	65166
TYS=150.0KSI	P	R.T.	•	150	3.5% NaCl	CANT	ï	1	1	***	150	130+	•••	1972	83619
TYS=160.0KSI	P	R.T.		160	3.5% NaCl	CANT.		1	1	i	205	130+	:	1972	83613
TYS=170.0KSI	P	R.T.	1	170	3.5% NaCl	CANT.		1	1		165	110*		1972	83613
TYS=175.0KSI	Ъ	R.T.	-	175	3.5% NaCl	CANT.	i	-		:	140	105		1972	83613

 $^{+}$ specimen thickness does not meet minimum requirements of $2.5~(rac{K_{low}}{\sigma_{yy}})^{2}$

^{*} asterisk in specimen design column indicates that specimens are side-grooved

TABLE 3.4.3.3

K_{Isce} SUMMARY FOR ALLOY STEEL 18Ni(180)(MAR)

	r u	Test	0	Yield		S	Specimen		Prod	,		ŀ	Test		
Condition/ Heat Treat	Form	Temp (°F)	Spec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)	Thk (in)	(in)	Roi√in)	h _{les} (Ksi√in)	Time (min)	Test Date	Reference
1500°F 1hr AC	c	E C	č E	100	Seawater	CANT					÷	143*		1971	81004
900°F 3hr	4	n.1.		1//	3.5% NaCl	CANT	i	ł		;	-	130+	30000	1971	81004
TYS=170Ksi	Ъ	R.T.	:	170	35% NaCl	CANT		1	1	1	160	140.	1	1972	83613
TYS=175Ksi	Ь	R.T.	:	175	3.5% NaCl	CANT.		-	1	÷	160	125+	1	1972	83613
TYS=178Ksi	Ъ	R.T.	1	178	Synth. Seawater	CANT	1	1	1		118	108	60000	9961	65166
TYS=185Ksi	P	R.T.		185	3.5% NaCl	CANT.	•	1	1	•••	180	130+	ł	1972	83613
TYS=190Ksi	Ъ	R.T.	·	190	3.5% NaCl	CANT.		1	1		170	120	1	1972	83613
TYS=195Ksi	P	R.T.		195	3.5% NaCl	CANT.		1	1	:	165	09	:-	1972	83613
TYS=200Ksi	P	R.T.	1	200	3.5% NaCl	CANT	i	1	-	i	190	105	·	1972	83613

 $^{\circ}$ specimen thickness does not meet minimum requirements of $2.5~(rac{K_{loo}}{\sigma_{yy}})$

^{*} asterisk in specimen design column indicates that specimens are side-grooved

TABLE 3.5.1.1

FOR ALLOY STEEL 18NI(200)(MAR) AT ROOM TEMPERATURE MEAN PLANE STRAIN FRACTURE TOUGHNESS

D					K_{lc}	$K_{Ic}~(ksi\!\sqrt{in})$	<u>(i</u>			
Form	Condition/Heat Treatment			01	Specimen Orientation	n Orien	itation			
			L-T			T-L			S-L	
		Mean K ₁ e	Std Dev	и	Mean K _{re}	Std Dev	u	Mean K _{le}	Std Dev	g
	1650F 4.5 HR AC AGED 1000F 6HR	102.3	1.2	3	•	-	:	i	:	:
Plate	1650F 4.5 HR AC AGED 900F 24HR	96.5	0.7	2	•••	ı	ï	i	į	i
	1650F 4.5 HR AC AGED 950F 24HR	99.3	1.2	3		ï	i	:	i	:
Forging	1650F 4.5 HR AC AGED 900F 6HR	100.3	9.0	3	-	•	:	:		;

TABLE 3.5.2.1

				ALL	ALLOY STEEL		8NI (200	18NI (200) (MAR)	K _{Io}						
	PROI	PRODUCT					SPECIMEN	z	CRACK			K			
CONDITION	FORM	THICK (in.)	TEMP TEMP (°F)	SPEC	YIRLD STR (Ket)	WIDTH (in.) W	THICK (in.) B	DESIGN	LENGTH (in.) A	E.6 (K. TYS)* (In.)	K (al)	K. MEAN	BTAN	DATE	REFER
		4.25			211.0	4.700	2.400	CT	2.400	09:0	103.00			1972	83834 (1)
1650F 4.5 HR AC AGED 1000F 6 HR	Plate	4.25	R.T.		211.0	7.900	3.900	NB	3.930	0.67	101.00	102.3	1.2	1972	83834 (1)
		4.25			211.0	6.310	3.900	CT	3.220	09:0	103.00			1972	83834 (1)
1650F 4.5 HR AC AGED 850F 24 HR	Forging	3.00	R.T.	LT	224.0	6.300	3.900	ст	3.160	0.33	81.00	i	1	1966	76411 (1)
1650F 4.5 HR AC		4.25	E		219.0	4.730	2.400	СТ	2.390	0.48	96.00			1972	83834 (1)
AGED 900F 24 HR	Figure	4.25	K.T.	-	219.0	7.890	3.900	NB	3.940	0.49	97.00	96.5	0.7	1972	83834 (1)
		3.00			210.0	6.300	3.900	CT	3.180	0.57	100.00			1972	83834 (1)
1650F 4.5 HR AC AGED 900F 6 HR	Forging	3.00	R.T.	L-1	210.0	4.700	2.400	CT	2.360	0.58	101.00	100.3	9.0	1972	83834 (1)
		3.00			224.0	7.900	3.900	СŢ	3.880	0.57	100.00			1972	83834 (1)
		4.25			216.0	4.720	2.400	CT	2.390	0.54	100.00			1972	83834 (1)
1650F 4.5 HR AC AGED 950F 24 HR	Plate	4.25	R.T.	ŗ	216.0	6.300	3.940	CT	3.940	0.54	98.00	99.3	1.2	1972	83834 (1)
		4.25			216.0	7.870	3.900	SE SE	3.930	0.54	100.00			1972	83834 (1)

NOTES: (1) VACUUM ARC REMELITED

TABLE 3.5.3.3

K_{Isco} SUMMARY FOR ALLOY STEEL 18Ni(200)(MAR)

/==;+;F==0.	1	Test	ŭ	Yield		ß	Specimen		Prod	,			Test		
Heat Treat	Form	Temp (°F)	Spec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)	Thk (in)	Crack (in)	Ro (Ksi√in)	Ksivin)	Time (min)	Test Date	Reference
1500°F 1hr AC;	c.	E	ē	010	0.257.81.01	CANT	•		1			38	20000	1971	80824
900°F 3hr	4	ъ. I.	2	617	5.3 % (NBC)	CANT		1	1	1		.#6	00009	1261	81004
1650°F; 900°F 3hr AC	Р	R.T.		197	3.5% NaCl	CANT.	2.5	9.0	-	i	231	104⁺	i	1970	84342
1675F 2hr AC; 500°F 15min;	F	Ę	č E	192.6	3.5% NaCi	CANT.	866.0	0.75	76'0	0.25	146	48	39000	1967	29169
850°F 4hr Cool 250°F/min	4	K.I.	T-2	197.5	3.5% NaCl	CANT.	0.938	0.75	•••	0.25	144	78	30000	1967	69162
TYS=215Ksi	P	R.T.	-	215	3.5% NaCl	CANT.		-	1	-	125	70	1	1972	83613
Weld center line	P	R.T.	L-S	215	3.5% NaCl	CANT			•••		115	02	19000	1961	78807
Unspecified	Ь	R.T.	L-T	207	Unsymmetrical dimethyl hydrozina	TDCB	53.5	6.5	0.5	i	110	.011	47500		80667

 * specimen thickness does not meet minimum requirements of $2.5~(rac{K_{Loo}}{\sigma_{ys}})^2$

^{*} asterisk in specimen design column indicates that specimens are side-grooved

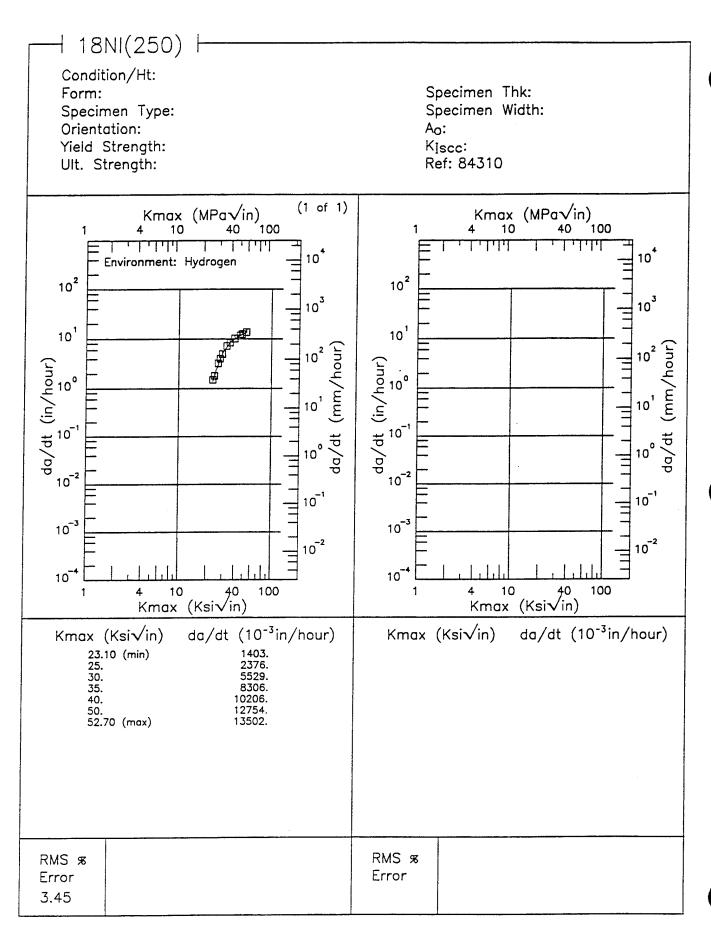


Figure 3.6.3.2.1

H 18NI(250) H Condition/Ht: Specimen Thk: Form: Specimen Width: Specimen Type: TDCB Orientation: Ao: Yield Strength: Kiscc: Ult. Strength: Ref: 78313 Kmax (MPa√in) 40 100 (1 of 1) Kmax (MPa√in) \$ 10 40 100 1 11111 <u>111111</u> 104 10 Environment: 3.5% NaCl 10² 10² 103 103 101 101 da/dt (in/hour) da/dt (in/hour) 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ 10-2 10-2 10-4 10-4 4 10 40 Kmax (Ksi√in) 4 10 40 Kmax (Ksi√in) 100 100 ·Kmax (Ksi√in) $da/dt (10^{-3}in/hour)$ Kmax (Ksi√in) $da/dt (10^{-3}in/hour)$ RMS % RMS & Error Error

Figure 3.6.3.2.2

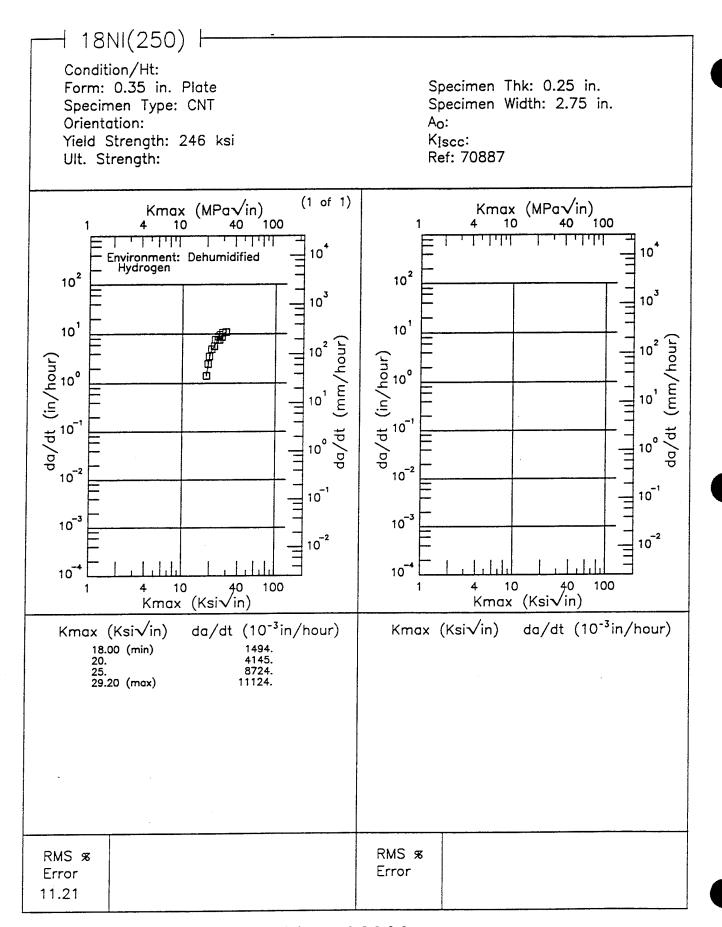


Figure 3.6.3.2.3

TABLE 3.7.1.1

FOR ALLOY STEEL 18NI(250)(MAR) AT ROOM TEMPERATURE MEAN PLANE STRAIN FRACTURE TOUGHNESS

Product					K_{Ie}	$K_{Ic}~(ksi\sqrt{in})$	<u>(</u>			
Form	Condition/Heat Treatment			<i>S</i> 2	Specimen Orientation	n Orien	tation			
			L-T			T-L			S-L	
		Mean K _{to}	Std Dev	u	Mean K _{te}	Std Dev	п	Mean K _{to}	Std Dev	п
	1500F AC 850F 6HR	76	1.9	70		:	ł			:
	1500F AC 900F 24HR	80.7	1.2	9	:	:		••	፡	ŀ
rate	1500F AC 900F 6HR	82.3	3.2	9	:	÷			:	•
	1500F AC 950F 6HR	84	2.6	9	:	:	:	÷	:	ij
Billet	1500F 1HR AC AGED 900F 3HR AC	74.3	4.2	7	64.1	4.4	9	:	i	i

TABLE 3.7.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 18NI(250)MAR AT ROOM TEMPERATURE

ENVIRONIMENT: 3.5% NaCl	FCGR (10 ⁻⁸ ir/cycle) AK Lovel (Kst/in)	18.43
	R FREQ	0.1
: L-T	PRODUCT FORM	BILLET
ORIENTATION: L-1	CONDITION/ HEAT TREATMENT	UTS=243KSI

TABLE 3.7.1.2.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 18NI(250)MAR AT ROOM TEMPERATURE

	50.0 100.0	71.03
Air	FCGR (10 ⁻⁸ in/cycle) ΔK Lovel (Ksi/in) ΔK Lovel (Ksi/in) 25 10.0 20.0 50.0	5.91
ENVIRONMENT: Lab Air	2GR (10 .K Lovel	1.16
RONME	FY A	
ENAI		
	FREQ (Hz)	10
	Ħ	0.1
	RODUCT	BILLET
T-L	PRODUCT	BIL
ORIENTATION: T-	int	
ORIENT	CONDITION/ HEAT TREATMENT	UTS=243KSI
	CONI	UTS
	P	

TABLE 3.7.2.1

				WITH AFT	ALLOY STEEL		18NI(250)(MAR))(MAR)	K _{Ie}						
	PROI	PRODUCT				4 2	SPECIMEN	7	CRACK			K _{Io}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (in.)	THICK (in.) B	DESIGN	LENGTH (In.) A	2.0 (K.,TYS)* (in.)	K. (Kai •	K. MEAN	BTAN	DATE	REFER
		12.00			231.0	2.000	1.020	NB	:	0.24	70.90			1974	90981 (1)
		12.00			231.0	2.000	1.020	NB	:	97.0	74.90			1974	90981 (1)
		1.00			233.0	2.000	1.020	NB		0.24	72.20			1974	90981 (1)
1500F 1HR AC AGED 900F 3HR AC	Billet	12.00	R.T.		233.0	1.000	0.500	CT		0.25	73.40	74.3	4.2	1974	90981 (1)
		12.00			233.0	1.000	0.500	LO		0.27	77.20		!	1974	90981 (1)
		12.00			233.0	2.000	1.020	NB		0.22	69.60			1974	90981 (1)
		12.00			233.0	1.000	0.500	CT		0.31	81.80			1974	90981 (1)
		12.00			232.0	2.000	1.020	NB	i	0.22	69.10			1974	90981 (1)
		12.00		1	232.0	2.000	1.020	NB	:	0.17	61.00			1974	90981 (1)
1500F 1HR AC	771120	12.00	E	1	232.0	1.000	0.500	C.	ï	0.20	65.00			1974	90981 (1)
AGED 900F 3 HR AC		12.00		3	232.0	1.000	0.500	CJ	i	0.22	69.20	64.1	4.4	1974	90981 (1)
		12.00		1	232.0	2.000	1.020	NB	1	0.16	69.00			1974	90981 (1)
		12.00			232.0	1.000	0.500	cr		0.17	61.20			1974	90981 (1)
		4.26			253.0	3.750	1.800	NB	1.800	0.22	73.00			1972	83834
		4.25		1	253.0	3.000	1.800	CT	1.800	0.24	78.00			1972	83834
1500F AC 850F 6HR	Plate	4.25	R.T.	5	253.0	3.000	1.800	CT	1.800	0.23	77.00	76.0	1.9	1972	83834
		4.25			263.0	3.750	1.800	NB	1.800	0.22	76.00	····		1972	83834
		4.26			253.0	3.000	1.800	C.	1.800	0.22	76.00			1972	83834

NOTES: (1) COMPOSITION (WT PERCENT) 0.014C, 0.087Mn, 0.006P, 0.078l, 18.6Nl, 0.10Cr, 4.75Mo, 0.41Tl, 0.11Al

TABLE 3.7.2.1 (CONCLUDED)

				ALI	ALLOY STEEL		18NI(250)(MAR))(MAR)	K _{Io}						
	PRODUCT	DUCT				uz	SPECIMEN	7	CRACK			K _{ro}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIRLD STR (Kel)	WIDTH (in.)	THICK (in.) B	DESIGN	LENGTH (in.) A	E.6 (K.,,TYS)* (in.)	K. (Ked • √(n.)	K, MEAN	STAN	DATE	REFER
		2.00		1	259.0	3.000	1.800	СT	1.800	0.25	82.00			1968	73612
		2.00	·		259.0	3.750	1.800	NB NB	1.800	0.24	80.00			1968	73612
anre good ov goost	Ē	2.00	E	I	259.0	3.750	1.800	NB	1.800	0.25	82.00			1968	73612
1000F AC 900F 24filk	Flate	2.00		<u> </u>	259.0	3.000	1.800	cr	1.800	0.24	81.00	80.7	1.2	1968	73612
		2.00	 -		259.0	3.000	1.800	СТ	1.800	0.24	80.00			1968	73612
		2.00			259.0	3.750	1.800	NB	1.800	0.23	79.00			1968	73612
		2.00			259.0	3.000	1.800	CT	1.800	0.23	79.00			1968	73612
		2.00			259.0	3.750	1.800	NB	1.800	0.24	81.00			1968	73612
1 FOND A COOR CITE	i i	2.00	E	E	259.0	3.750	1.800	NB	1.800	0.26	84.00			1968	73612
1000F AC 500F SIIN	Flate	2.00		<u> </u>	259.0	3.000	1.800	cr	1.800	0.24	81.00	82.3	3.2	1968	73612
		2.00			259.0	3.000	1.800	CT	1.800	0.24	81.00			1968	73612
		2.00			259.0	3.750	1.800	NB RB	1.800	0.29	88.00			1968	73612
		2.00			252.0	3.000	1.800	CT	1.800	0.28	84.00			1968	73612
		2.00		1	252.0	3.750	1.800	NB NB	1.800	0.26	82.00			1968	73612
15000 AC GOOD SHD	5	2.00	£	E	252.0	3.750	1.800	NB	1.800	0.28	84.00			1968	73612
MINOS AC BOOK BITM		2.00	į	1 	262.0	3.000	1.800	СT	1.800	0.27	83.00	84.0	2.6	1968	73612
		2.00			252.0	3.000	1.800	C.I.	1.800	0.26	82.00			1968	73612
		2:00			252.0	3.750	1.800	NB	1.800	0.32	89.00			1968	73612

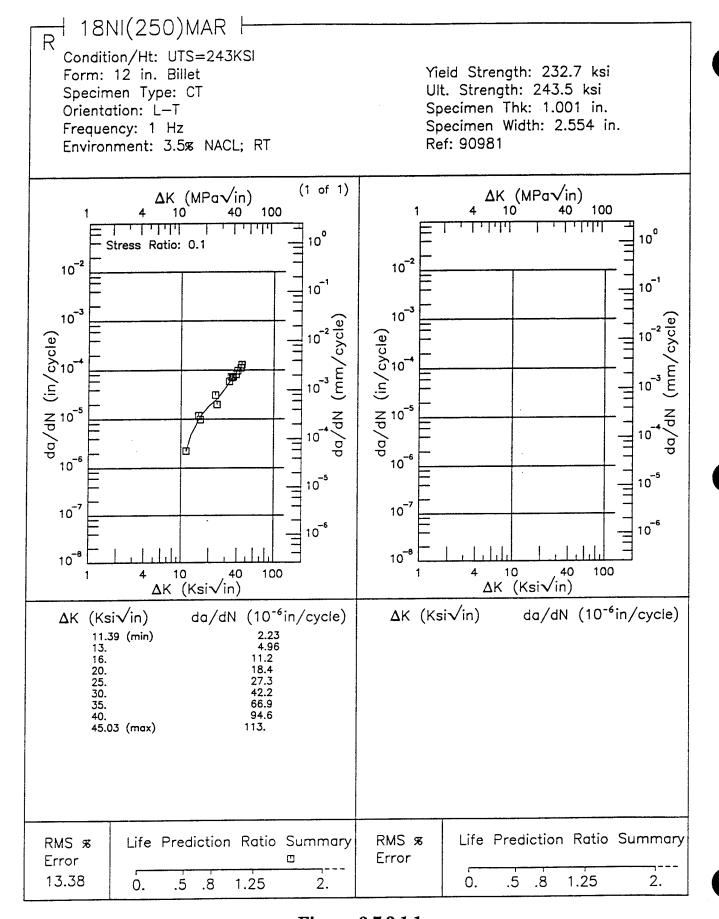


Figure 3.7.3.1.1

Yield Strength: 231.8 ksi Form: 12 in. Billet Ult. Strength: 243 ksi Specimen Type: CT Specimen Thk: 1 - 1.001 in. Orientation: T-L Specimen Width: 2.553 in. Stress Ratio: 0.1 Ref: 90981 Frequency: 10 Hz (2 of 2) (1 of 2) $\Delta K (MPa\sqrt{in})$ Δ K (MPa \sqrt{in}) 10 100 100 10° 10° Environment: 3.5% NACL; R.T. Environment: LAB AIR; R.T. 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 8 ; 10⁻⁶ 10-6 10⁻⁵ 10 -5 10⁻⁷ 10⁻⁷ 10 6 10⁻⁶ 10-8 10 8 40 100 10 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) $da/dN (10^{-6}in/cycle)$ ΔK (Ksi√in) ΔK (Ksi√in) 7.69 (min) 8. 9. 13. 16. 20. 25. 30. 50. 52.78 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error 20.85 0. .5 8. 1.25 2. Ò. .Ś .8 1.25 2.

Condition/Ht: UTS=243KSI

H 18NI(250)MAR H

Figure 3.7.3.1.2

TABLE 3.7.3.3

K_{Isce} SUMMARY FOR ALLOY STEEL 18Ni(250) (MAR)

		Test		Yield		S.	Specimen		Drod				100		
Condition/ Heat Treat	Form	Temp (°F)	Spec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)		Crack (in)	Ko (Ksi√in)	K _{le∞} (Ksi√in)	Time (min)	Test Date	Reference
				252	Synth. Seawater	CANT	1	1	1	i	72.6	69	3000	1966	65166
					•	CANT.	3	1	1.25	1.05	93	35	00009	1968	73829
Unspecified	<u>~</u>	R.T.	1			CANT.	0.5	1	1.25	0.17	89	21	00009	1968	73829
				259	Synth. Seawater	CANT.	1	1	1.25	0.35	78	37	00009	1968	73829
						CANT.	ಬ	1	1.25	1.75	95	38	00009	1968	73829
						•		i	ŀ	i	i	36.5	;	1969	74232
1650F 1 95hr WO.						CANT	3	T	125		93	35	i	1970	78065
1525F 1.25hr WQ;	ч	R.T.	ŀ	259	Synth. Seawater	CANT	-	1	1.25	ı	78	37	-	1970	78065
SOUF SOF AC						CANT	5	1	1.25		98	38		1970	78065
10000		Ę		6	3.5% NaCl	CNT	2	0.05	0.08		ï	110+	20000	1968	72283
900F Zhr AC	מ	K.T.	-	877	Dist. Water	CNT	8	0.05	90.0		i	110*	30000	1968	72283
Age 900F 3hr	Ъ	R.T.	L-T	249	3.5% NaCl	NB	1.5	0.48	0.48		92	45	:	1971	84351
Agg GOOD Shy AC	P	Ę	٥ -			CANT	0.5	0.375	9.0			50		1971	80824
ow life Joog nage		1.1.	r-J		o.o.o Mari	CANT	0.482	0.375	0.5	1	i	31		1971	80824
TYS=250Ksi	Ъ	R.T.		250	3.5% NaCl	CANT.		1	1		70	50	1	1972	83613
TYS=260Ksi	Ъ	R.T.		260	3.5% NaCl	CANT		1	1	I	95	70		1972	83613

* specimen thickness does not meet minimum requirements of 2.5 $(\frac{K_{Loo}}{\sigma_{yy}})^2$

asterisk in specimen design column indicates that specimens are side-grooved

TABLE 3.8.3.3

K_{Isce} SUMMARY FOR ALLOY STEEL 18Ni(280)(MAR)

	£		7	Yield		Ś	Specimen		Prod	-	22	ì	Test		
Condition/ Heat Treat	Form		Spec Or.	Temp Or. (Ksi)	Envir.	Design	Width (in)	Thick (in)	Thk (in)	Crack (in)	Thk Crack ho (in) (Ksi√in)	n _{lo∞} (Ksi√in)	Time (min)	Test Date	Reference
1500°F 1hr AC; 900°F 3hr	Ь	R.T.		277	3.5% NaCl	CANT	0.75	0.75	:		09	14	14400	1971	82164

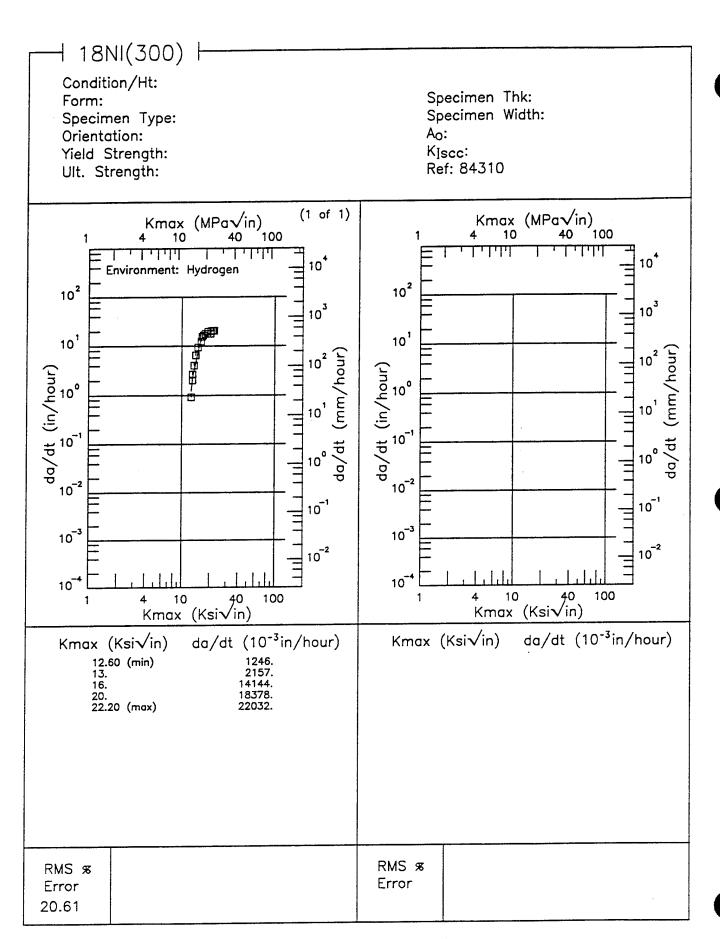


Figure 3.9.3.2.1

H 18NI(300) H Condition/Ht: AGED 6HR 900F Specimen Thk: 0.5 in. Form: Specimen Width: 1.5 in. Specimen Type: NB - 3 pt Orientation: Ao: Yield Strength: K_{Iscc}: Ref: 74719 Ult. Strength: Kmax (MPa√in) 40 100 Kmax (MPa√in) 40 100 (1 of 1) 1 1 1111 1 1 1 1 1 1 1 1 111111104 Environment: 3.5% NaCl 10² 10² 103 103 101 10¹ da/dt (in/hour) o. o. o. da/dt (in/hour) 10-2 10-2 10-1 10 1 10⁻³ 10-3 10-2 10-2 10-4 10-4 4 10 40 Kmax (Ksi√in) 100 4 10 40 Kmax (Ksi√in) 100 da/dt (10⁻³in/hour) $da/dt (10^{-3}in/hour)$ Kmax (Ksi√in) Kmax (Ksi√in) RMS % RMS & Error Error

Figure 3.9.3.2.2

TABLE 3.10.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK 18NI(300)MAR AT ROOM TEMPERATURE

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ENVIRONMENT: 3.5% NaCl	ěi.	
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ORIENTATION: L-T	CONDITION/ HEAT TREATMENT	UNSPECIFIED
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TABLE 3.10.1.2.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK

100.0 60.0 23.22 FCGR (10⁻⁸ in/cycle) ΔK Level (Kei√in) 20.0 9.38 ENVIRONMENT: H.H.A. 10.0 1.51 0.8 18NI(300)MAR AT ROOM TEMPERATURE 2) 2) FREQ (Hz) Ø 90.0 0.67 ĸ PRODUCT FORM FORGING ORIENTATION: L-T HEAT TREATMENT CONDITION UNSPECIFIED

TABLE 3.10.1.2.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK

•		196.0	
		[6] (1) (50.0	
	ľ.A.	d in/cyc	7.42
	AT: L.F	7. (10 Tovel 10.0 10.0	1.49
RE	ENVIRONMENT: L.H.A.	FCC AK	
RATU	INVIR	2.3	
TEMPE	1	FREQ (Hz)	23
T ROOM		æ	0.67
18NI(300)MAR AT ROOM TEMPERATURE	: L-T	PRODUCT	FORGING
	ORIENTATION: L-'	CONDITION/ HEAT TREATMENT	UNSPECIFIED

TABLE 3.10.1.2.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 18NI(300)MAR AT ROOM TEMPERATURE

ORIENTATION: Unspecified

ENVIRONMENT: Dry Argon

Q.		
100.0		
07		İ
) 80		
FCGR (10 ⁻⁸ in/cycle) AK Level (Kst/in) 1 10.0 20.0 80.0		
ye.		
fe si	1.98	2.1
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9 6	0.17	0.18
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FC A1		
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CONDITION/ HEAT TREATMENT		

TABLE 3.10.2.1

				AL	ALLOY STEEL		18NI(300)(MAR))(MAR)	K _{Io}						
	PRODUCT	UCT				w.	SPECIMEN	-	CRACK			K _{Io}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kat)	WIDTH (In.)	THICK (in.)	DEBIGN	LENGTH (in.) A	2.6 (K.,TYS)* (in.)	7. 2. j.	K. MBAN	STAN	DATE	REFER
1700F 1HR AC 1500F 1HR AC 900F 6HR	Forging	10.00	99-	LR		1.000	0.500	NB	0.500	i	64.00	,	ı	1970	78425
1700F 1HR AC	, ,	10.00	ę		280.0	1,000	0.500	NB	0.500	0.16	71.20			1970	78425
1500F 1HR AC 900F 6HR	gungaoa	10.00	i.	ž	300.0	1.000	0.500	NB	0.500	0.11	64.20	67.7	6.4	1970	78425
1700F 1HR AC	Ē	10.00	Ę	,	280.0	1.000	0.500	NB	0.500	0.18	75.50			1970	78425
1600F 1HR AC 900F 6HR	rorging	10.00	K.T.) 1	299.0	1.000	0.500	NB	0.500	0.11	62.50	69.0	9.5	1970	78425
900F AGED	Plate	1.00	R.T.	L-T	276.0	0.800	0.400	CT	0.400	i	1	:		1761	86582 (1)

NOTES: (1) COMPOSITION (WT PERCENT) 0.017C, 0.05Mn, 0.004P, 0.007S, 0.09Si, 18.8Ni, 4.95Mo, 7.2Cb, 0.58Ti, 0.13Al

TABLE 3.10.2.2

_			1	, -		,			-	_								_
		REFER		60578	60578	60578	60578	60578	80578	60578	60578	60578	60578	8/909	8/909	60578	60578	60578
		DATE		1961	1964	1964	1964	1964	1964	1964	1964	1964	1964	1964	1964	1964	1964	1964
		BTAN				7.9					7.4					08		
	K c	K _c MEAN				86.4					142.6					124.2		
		K _o (Kelvin.)		97.12	82.39	79.86	90.70	82.04	152.50	143.35	143.35	131.80	141.76	113.18	130.56	133.50	121.61	122.40
		BTAN				6.0					7.4					6.7	!	
	Керр	K.				84.8					142.6					124.1		
		K (Kalvin.)	INED	95.20	82.39	79.86	84.28	82.04	152.50	143.35	143.35	131.80	141.76	113.18	130.56	132.83	121.61	122.40
К _С	SS SSS	MAX (Kal)	RESTRA	63.80	55.80	55.80	56.50	65.00	150.00	141.00	141.00	131.00	138.00	76.50	88.00	89.50	81.90	82.50
	GROSS STRESS	ONSET (Kei)	BUCKLING OF CRACK EDGES NOT RESTRAINED		:	ı	i	ļ	ı	:	ı	ı	i	i	i	ì	÷	1
18NI(300)MAR	CRACK	FINAL (in.) Se,	жаск еп	1.290	1.230	1.170	1.400	1.250	0.590	0.590	0.590	0.580	0.600	1.230	1.240	1.250	1.240	1.240
18N	CR	INIT (in.) Sa,	NG OF	1.250	1.230	1.170	1.250	1.250	0.590	0.590	0.590	0.580	0.600	1.230	1.240	1.240	1.240	1.240
	SPECIMEN	THICK (In.) B	BUCKLI	0.026	0.028	0.028	0.029	0.029	0.025	0.025	0.025	0.025	0.025	970.0	0.026	0.027	0.027	0.027
	SPEC	WIDTH (in.)		4.000	4.010	4.020	4.010	4.010	2.020	2.020	2.020	2.020	2.020	3.950	4.020	4.010	4.020	4.020
	YIELD STR (Kat)			386.0	386.0	386.0	386.0	386.0	336.0	336.0	336.0	336.0	336.0	336.0	336.0	336.0	336.0	336.0
		SPEC				F.7					7.			7 7 7				
	ĹO DE	TEMP (°F)				-423					-320					-320		
	ucr	THICK (in.)		0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03
	PRODUCT	FORM			1	Sheet					Sheet					Sheet		
		CONDITION HEAT TREAT				i					ı					ţ		E-V-A

TABLE 3.10.2.2 (CONCLUDED)

		REFER		60578	60578	60578	60578	60578	60578	60578	60578	60578	60578	60578	60578	80578	60578
		DATE		1964	1964	1964	1964	1964	1962	1964	1964	1964	1964	1961	1964	1964	1961
		STAN				6.					60	}		1		10.9	
	K	K. MEAN				182.1					128.5			1		110.8	
		K _o (Kolvin.)		133.81	130.80	132.52	125.83	137.65	124.41	132.42	129.75	124.47	131.39	108.40	104.74	103.26	122.91
		BTAN			I	8. 70								ı		11.0	
	Карр	MEAN				131.6					128.1			:		110.3	
		K (Kelvlin.)	INED	133.81	130.80	132.52	125.83	134.82	124.41	132.42	129.75	123.22	130.72	108.40	104.74	103.14	122.91
Kc	SS	MAX (Kai)	RESTRA	133.00	130.00	136.00	125.00	134.00	83.80	89.20	87.40	83.00	98.50	34.70	33.70	33.10	39.50
	GROSS	ONSET (Kai)	GES NOT	:		ï		:	i	:				1	:	i	ł
18NI(300)MAR	CRACK	FINAL (in.) Sa,	BUCHLING OF CRACK RINGES NOT RESTRAINED	0.580	0.580	0.650	0.580	0.600	1.240	1.240	1.240	1.260	1.240	5.490	5.470	6.500	5.480
18N	CRACK	INIT (in.) Sa,	NG OF C	0.580	0.580	0.550	0.580	0.680	1.240	1.240	1.240	1.240	1.230	5.490	6.470	6.490	5.480
,	PECIMEN	THICK (in.) B	BUCKL	0.025	0.025	0.025	0.026	0.026	0.028	0.028	0.028	0.028	0.029	0.025	0.022	0.025	0.025
	SPEC	WIDTH (in.) W		2.020	2.020	2.020	2.010	2.020	4.000	4.000	4.000	4.000	4.000	17.700	18.100	18.060	18.100
	YIELD STR (Kel)			277.0	277.0	277.0	277.0	277.0	277.0	277.0	277.0	277.0	277.0	277.0	277.0	277.0	277.0
		SPEC				LT					LT			1.7		7	
	T CONT	TEMP (°F)				R.T.					R.T.			R.T.		R.T.	
	UCT	THICK (in.)		90.03	90.03	0.03	0.03	90.03	0.03	0.03	0.03	0.03	0.03	0.03	97.0	97.0	0.03
	PRODUCT	FORM		L		Sheet					Sheet	.		Sheet		Sheet	
		CONDITION HEAT TREAT				ŀ					!			:		!	

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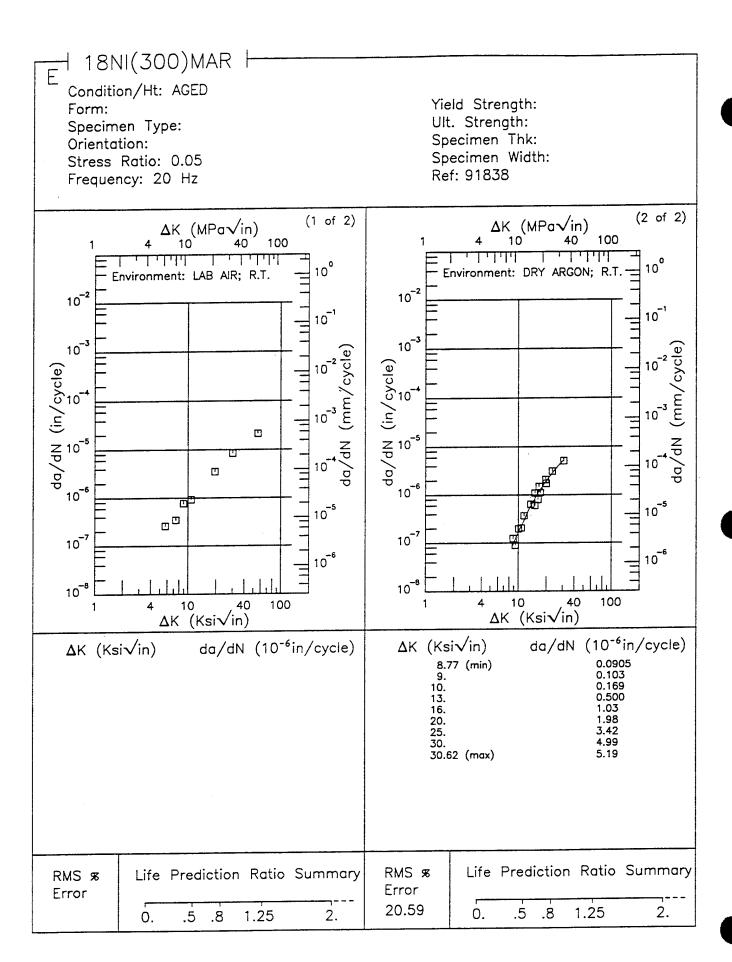


Figure 3.10.3.1.1

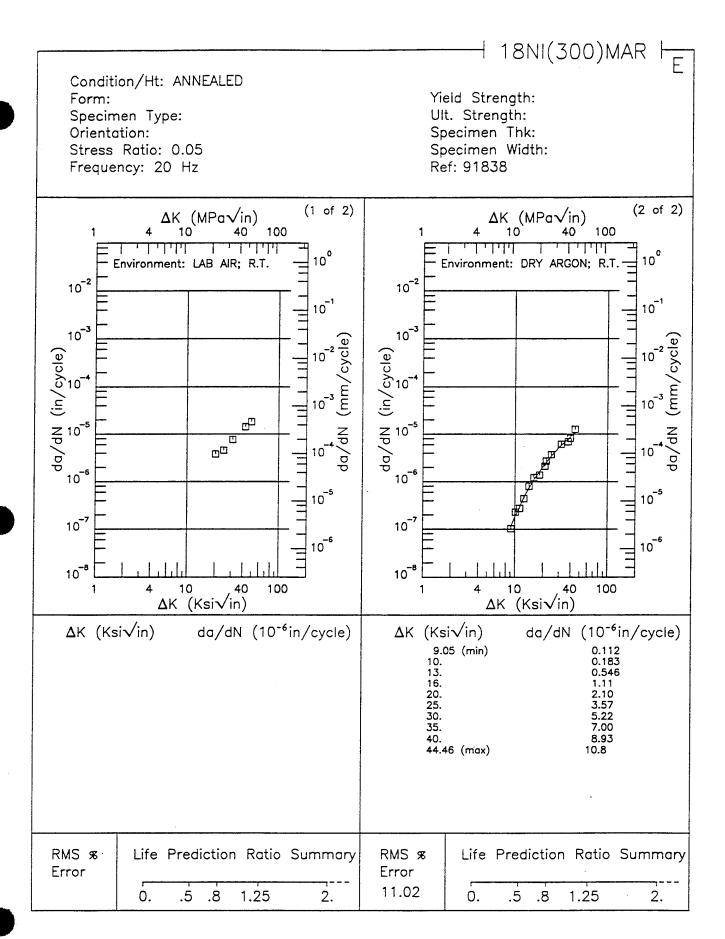


Figure 3.10.3.1.2

18NI(300)MAR R Condition/Ht: Yield Strength: Form: 0.13 in. Forging Specimen Type: CCP (max stress specified) Ult. Strength: Specimen Thk: 0.125 in. Orientation: L-T Specimen Width: 3 in. Frequency: 2 Hz Ref: 78425 Environment: H.H.A.; RT (1 of 1) Δ K (MPa \sqrt{in}) ΔK (MPa√in) 100 10 10 40 100 11111 10° 10° Stress Ratio: 0.06 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ 10 -2 da/dN (in/cycle) da/dN (in/cycle) 10⁻³ 10⁻⁶ 10-6 10⁻⁵ 10 -5 10⁻⁷ 10⁻⁷ 10 -6 10-6 10-8 10 -8 40 100 10 100 10 40 $\Delta K (Ksi\sqrt{in})$ ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) Δ K (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 20.16 (min) 25. 30. 35. 40. 2.74 6.18 8.91 50. 23.2 60. 67.79 (max) 38.1 46.5 Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error 13.67 .5 .8 1.25 2. 1.25 0. 0. .5 .8 2.

Figure 3.10.3.1.3

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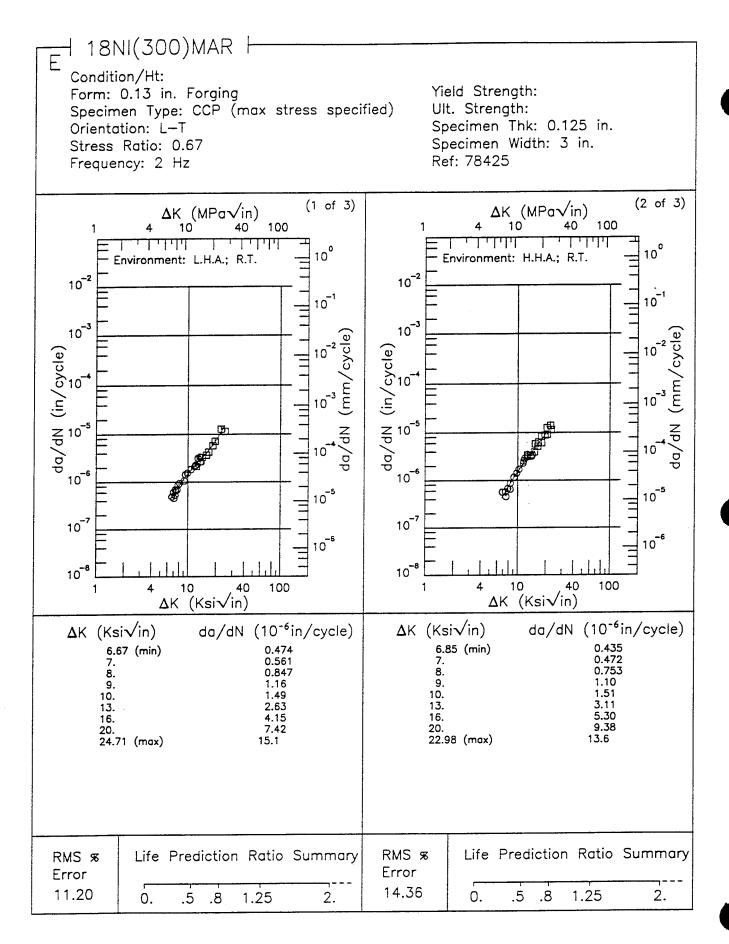


Figure 3.10.3.1.4

H 18NI(300)MAR H Condition/Ht: Yield Strength: Form: 0.13 in. Forging Specimen Type: CCP (max stress specified) Ult. Strength: Specimen Thk: 0.125 in. Orientation: L-T Stress Ratio: 0.67 Specimen Width: 3 in. Ref: 78425 Frequency: 2 Hz (3 of 3) Δ K (MPa \sqrt{in}) $\Delta K (MPa\sqrt{in})$ 100 10 10 100 40 10° 10° Environment: 3.5% NACL; R.T. 10-2 10-2 10-1 10-1 10⁻³ 10-3 da/dN (in/cycle) da/dN (in/cycle) 10 -6 10⁻⁶ 10 5 10 -5 10-7 10⁻⁷ 10⁻⁶ 10-6 10 8 4 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) Δ K (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) 14.61 (min) 16. 3.56 4.82 20. 22.60 (max) 10.2 16.4 Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS & Error Error 6.81 .5 .8 1.25 0. .5 .8 1.25 2. 0. 2.

Figure 3.10.3.1.4 (Concluded)

TABLE 3.10.3.3

Kisce SUMMARY FOR ALLOY STEEL 18Ni(300)(MAR)

	•								Complete		enacionarios	1	hasterensons
	Reference	63061	63061	77716	77716	77716	77716	77716	77716	77716	77716	77716	77716
	Test Date	1965	1965	1970	1970	1970	1970	1970	1970	1970	1970	1970	1970
Teat	Time (min)	10000	10000	:	10000		1	l	÷	i	1	10000	1000
	K _{lac} (Ksi√in)	36	99	10	6	10	6	12	6	6	10	10	15
. 1	Ko (Ksi√in)	93.9	63.1	120	120	120	120	66	70	70	02	66	70
	Crack (in)	0.2	0.2		-	ļ	•	i	ï	i			j
Prod	Thk (in)	0.25	0.25		-	•	**	ł	i	:			i
	Thick (in)	0.25	0.25	0.5	0.5	0.5	3.0	0.5	0.5	0.5	9.0	0.5	0.5
Specimen	Width (in)	1	1	0.625	0.625	0.625	0.625	0.625	0.625	0.625	0.625	0.625	0.625
Ś	Design	CANT	CANT	CANT.	CANT	CANT.	CANT	CANT.	CANT	CANT.	CANT	CANT.	CANT
	Envir.	. III - 2Q	LABE, WRIEF	1N H ₂ SO ₄	3% NaCl Ph1.7	3% NaCl Ph6.3	Dist. Water	1.5% Na ₂ Cr ₂ O7	'OS'H NI	3% NaCl -0.4V to -1.2V	3% NaCl O _g Sat.	3% NaCl Ph1.7	3% NaCl Ph1.7
Yield	Str (Ksi)	0 400	700.0		Coc	700		280		280		280	280
7	Spec Or.	5	<u>1</u>		ت +	2		L-S		L-S		r-s	g-T
Test	Temp (°F)	£	n. 1.		Đ	į		R.T.		R.T.		R.T.	R.T.
F	Form	£	4		ρ	9		В		В		В	В
	Condition/ Heat Treat	1500°F 0.5hr; AC	900°F 3hr		1500°F 2hr	800°F 10hr		1500°F 2hr 900°F 3.5hr		1500°F 2hr 900°F 100hr		1500°F 2hr 900°F 3.5hr	1500° F 2hr 900° F 100hr

TABLE 3.10.3.3 (CONTINUED)

K_{Isco} SUMMARY FOR ALLOY STEEL 18Ni(300)(MAR)

	Reference	77716	77716	77716	77716	78761	77716	77716	77716	77716	77716
·	Test Date	1970	1970	1970	0261	1970	1970	1970	1970	1970	1970
Test	Time (min)		•	ł		i		1	•	-	1
	K _{le∞} (Ksi√in)	12	17	8	01	7.5	10	10	14	8	13
:	Kai√in)	66	66	66	70	72.4	53	53	58	57	58
,	Crack (in)	••••	i	:		1	1	1	i	:	
Prod	Thk (in)	:	i	:	-	6		i		•••	_
	Thick (in)	9.0	0.5	0.5	970	0.4	0.5	0.5	0.5	0.5	0.5
Specimen	Width (in)	0.625	0.625	0.625	0.625	1	0.625	0.625	0,625	0.625	0.625
Σ	Design	CANT.	CANT	CANT.	CANT	CHAR	CANT	CANT.	CANT	CANT.	CANT
	Envir.	3% NaCl Ph11	3% NaCl Ph3.9	3% NaCl Ph6.3	3% NaCl Ph6:3	3.5% NaCl	1N Hgo,	3% NaCl Ph1.7	3% NaCl Ph1.7	3% NaCl Ph1.7	3% NaCi Ph6.3
Yield	Str (Ksi)		280		280	284		280	280	280	280
7	Spec Or.		L-S		r-s	T-T		L-S	r-s	r-s	r-s
Test	Temp (°F)		R.T.		R.T.	R.T.		R.T.	R.T.	R.T.	R.T.
	Form		В		В	দ		B	В	В	В
	Condition/ Heat Treat		1500°F 2hr 900°F 3.5hr		1500°F 2hr 900°F 100hr	1700°F 1500°F Aged 900°F 6hr	2300°F 1hr	1700°F 4hr 900°F 100hr	2300°F 1hr 1700°F 4hr 800°F 10hr	2300°F 1hr 1700°F 4hr 900°F 3.5hr	2300°F 1hr 1700°F 4hr 800°F 10hr

TABLE 3.10.3.3 (CONCLUDED)

K_{lsce} SUMMARY FOR ALLOY STEEL 18Ni(300)(MAR)

				Yield		ls.	Specimen		Prod				Too.T.		
Condition/ Heat Treat	Form	Temp (°F)	Spec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)		Crack (in)	Ko (Ksi√in)	K _{liss} (Ksi√in)	Time (min)	Test Date	Reference
2300°F 1hr 1700°F 4hr 900°F 3.5hr	В	R.T.	S-T	280	3% NaCl Ph6.3	CANT.	0.625	0.5	;	į	57	6	i	1970	77716
2300°F 1hr 1700°F 4hr 900°F 100hr	В	R.T.	S-T	280	3% NaCl Ph6.3	CANT.	0.625	0.5	-	1	63	6	ı	0261	77718
900°F 3hr 950°F 3hr	F	R.T.	T-L	306	3.5% NaCl	CANT	1.5	0.48	1	i	70	ಸ	ŀ	1970	78425
			L-T	302	3.5% NaCi	CANT	1.5	0.48	1	1	70	Ł	1	1970	78425
Age 900°F 6hr	ſΞŧ	R.T.	Ē	284.3	3.5% NaCl	CANT	1	0.5	6	·	72.4	5		1972	84356
			71-1	302	3,5% NaCi	CANT	1.5	0.48	1	÷	70		;	1970	78425
Age 950°F 12hr	Ŗ	R.T.	T-L	302	3.5% NaCl	CANT	1.5	0.48	1		89	9	;	1970	78425
Crack Prestressed to 50% K _{lc}	Ę	R.T.	T-L	284.3	3.6% NaCl	CANT	1	9'0	6		72.4	8	1	1972	84356
Crack Prestressed to 80% K _{lc}	FI.	R.T.	T-L	284.3	3.5% NaCl	CANT	1	0.5	6	i	72.4	10	i	1972	84356
Crack Prestressed to 25% K _{lt}	দ	R.T.	T-L	284.3	3.5% NaCl	CANT	1	0.6	6	_	72.4	5	1	1972	84356

asterisk in specimen design column indicates that specimens are side-grooved

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18NI(350) H Condition/Ht: AGED 8HR 800F Specimen Thk: 0.394 in. Form: Specimen Width: 0.394 in. Specimen Type: NB - 3 pt Ao: Orientation: K_{Iscc}: Yield Strength: 330 ksi Ref: 74719 Ult. Strength: Kmax (MPa√in) 40 100 Kmax (MPa√in) 40 100 (1 of 1) 111111 104 اللبليلي 104 Environment: 3.5% NaCl 10² 10² 103 103 10¹ 101 da/dt (in/hour) da/dt (in/hour) da/dt 10-2 10⁻¹ 10-1 10⁻³ 10 10-2 10-2 10-4 10-4 4 10 40 Kmax (Ksi√in) 100 4 10 40 Kmax (Ksi√in) 100 Kmax (Ksi√in) $da/dt (10^{-3}in/hour)$ Kmax (Ksi√in) $da/dt (10^{-3}in/hour)$ 13.00 (min) 16. 20. 25. 30. 32.00 (max) 2898. 3454. RMS % RMS % Error Error 11.26

Figure 3.11.3.2

TABLE 3.12.3.3

K_{Isco} SUMMARY FOR ALLOY STEEL 18Ni(350)(MAR)

7	r F	Test	2	Yield		S	Specimen				4	1	Test	E	
Condition/ Heat Treat	Form	Temp (°F)	Or. (Ksi)	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)	Thk (in)	(in)	Crack Ro (in) (Ksivin)	(Ksivin)	Time (min)	lest Date	Reference
1500°F 1hr; 800°F 8hr	F	R.T.	r-s	299	3.5% NaCl		968 0	0.394	4		70.1	S	1	1969	75677
1500°F 1hr; 900°F 8hr	F	R.T.	S-T	325	3.5% NaCl	:	0.394	0.394	4	i	35	10	ł	1969	75677
1500°F 1hr; 950°F 3hr	저	R.T.	r-s	325	3.6% NaCl		0.394	0.394	4	1	40	10	-	1969	75677
Age 800° F 8hr	FB	R.T.		299	3.5% NaCl	CHAR	0.394	0.394		::	30	2	•	1971	84351
Age 900° F 3hr	FB	R.T.		330	3.5% NaCl	CHAR	0.394	0.394	-	-	42	10		1971	84351
Age 900° F 8hr	FB	R.T.	;	335	3.5% NaCl	CHAR	0.394	0.394		1	98	10	•	1971	84351

TABLE 3.13.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL 300M AT ROOM TEMPERATURE

					K_{Ic}	$K_{Ic}~(ksi\sqrt{in})$	<u>@</u>			
Product Form	Condition/Heat Treatment			02	pecime	Specimen Orientation	itation			
			L-T			T-T			S-L	
		Mean K _{le}	Std Dev	ď	Mean K _{ie}	Std Dev	u	Mean K _{te}	Std Dev	£
Plate	1700F 1HR AC 1600F 1HR OQ 600F 2HR AC (AMS 6419)	51.8	0.7	က	}	i	i	į	:	i
	HEAT TREATED TO 64 RC HARDNESS	·	i	:	58.6	3.5	2	:	:	i
4	1600F 1.25 HR OQ 600F 2+2HR	54.6	2.5	4	50.6	1.7	2	54.1	1.1	4
rorging	Unspecified	52.6	2.3	4	62.9	2.	4	:	:	:
Ваг	2190F 1HR FC TO 1600F HOLD 0.5HR OQ 476F 1HR	47.9	3.8	2		i	:	i	ŀ	i

TABLE 3.13.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 300M AT ROOM TEMPERATURE

ENVIRONMENT: 3.5% NaCl

100.5	2.24				10	0.	BILLIEI	1010000000
105.32	4.2				.4	o'	PAT T TEC	TOUND AGO DATE
66.0 100.0	20.0	8.0 10.0 20.0 50.0		8.8				
<i></i>	*******							
	(Kat/ir	A. K. Lavel (Ket/in)			(Hz)	U	FORM	HEAT TREATMENT
					FREG	-	PRODUCT	CONDITION/
(9)	^d in/cyc	FCGR (10 ⁻⁸ in/eyele)	3					

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK

300M AT ROOM TEMPERATURE

ORIENTATION:

ENVIRONMENT: Alt Immersion Seawater - Immersion

		80.0 100.0		
		2	50.57	
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cile	(3)			<u> </u>
FCGR (10 ⁴ in/ayale)	ΔΚ Level (Kak/in)	10.0 20.0	80	_
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TABLE 3.13.1.2.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 300M AT ROOM TEMPERATURE

ORIENTATION:

ENVIRONMENT:

Alt Immersion Seawater - 1st Half Dry Cycle

		100.0		
		0.08		Г
		9		
6	•			
FCGR (10 ⁻⁶ in/cycle)	ΔK Lovel (Kek/in)			-
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TABLE 3.13.1.2.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 300M AT ROOM TEMPERATURE

ENVIRONMENT:

ORIENTATION:

100.0 Alt Immersion Seawater - 2nd Half Dry Cycle 0.08 PCGR (10 d in/ayule) ΔK Level (Kat/in) 99 2.48 5.74 10.0 0; 20 10 61 FREQ (Hz) 1.10 2 × ö o PRODUCT FORM BILLET HEAT TREATMENT CONDITION UTS=280-300KSI

TABLE 3.13.1.2.5

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK 300M AT ROOM TEMPERATURE

ENVIRONMENT: L.H.A.

7. a Commanda Company	moranoma				FCE	<i>2R</i> (10	PCGR (10 ^d ín/cycle)	(e)	
CONDITION/ HEAT TREATMENT	FORM	R	(HZ)		ΔF	Z Loval	ΔK Lovel (Ksiγin)	ı)	
				2.5	6.0	10.0	20.0	80.0	100.0
		90.0	1				3.67		
1700F 1.5HRS AC 1600F 1.5HRS OQ 600F	PAR PORCE	90.0	9			0.65	4.03		
2+2HRS	FORGING	0.3	9				4.75		
		0.5	8			0.9	6.83		
		-1	10				3.18	187.62	
UTS=280-300KSI	BILLET	0.	10				2.96	37.96	
		0.5	10			0.65	5.39		

TABLE 3.13.1.2.6

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK 300M AT ROOM TEMPERATURE

ENVIRONMENT: Lab Air

104.94	4.26	0.67			0.1-20	0.02		
	4.24	0.66			1-15	0.02	UNIDBOR	
	6.55	1			10	0.5		
47.71	3.52				10	0.02	BAR	UTS=280-300KSI
38.07	3.65				10	1-		
60.0 100.0	20.0	10.0	5.0	2.5				
n)	ľ (Ksh/ii	Δ <i>K Level (Ksl</i> /in)	Δ.		(Hz)	ä	FORM	HEAT TREATMENT
					FREQ	ä	PRODUCT	CONDITION/
(eff	⁸ in/cyc	PCGR (10.4 in/cyale)	FC					

TABLE 3.13.1.2.7

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 300M AT ROOM TEMPERATURE

ENVIRONMENT: S.S.W.

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- 18					
			100.0		
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			60.0	348.82	149.82
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	PCGR (10 ⁻⁸ in/cycle)	-			ł
	Ŕ	ΔK Level (Ksi√in)	20.0		
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	PROD	FOR		MIDGO	FORGING
	PROD	FOR		NIOGOS	FONGING
				NI OROM	FORGING
				MISGON	PONGING
				Miodog	FORGING
				NI DOCA	FORGING
				Minana	
		HEAT TREATMENT FOR			

TABLE 3.13.1.2.8

 $\Delta \mathbf{K}$

<u>2.5 5.0 10.0 20.0 50.0 50.0 50.0 50.0 50.0 50.0 5</u>	ORIENTATION: T-L ENVIRONMENT: L.H.A.	FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR A 300M AT ROOM TEMPERATURE	STRESS INTENSITY FACTOR A RE VIRONMENT: L.H.A. FCGR (10 ⁻⁶ in/cycle) AK Level (Kei/in) ss ss ss so so	EVELS OF MPERATU	FINED L	TH KATE AT DE 300M AT R 1: T-L PRODUCT FORM	ORIENTATION CONDITION HEAT TREATMENT
	FREQ FREQ	ION: T-L ENVIRONMENT; L.H.A. PRODUCT R FREQ FORM AK Level (Ksk/in)	4.1	9	0.08	FORGING	1700F 1.5HRS AC 1600F 1.5HRS OQ 600F
	PRODUCT " FREG	ATION: T-L ENVIRONM E	ΔK Level (Kst/in)	(Hz)	4	FORM	HEAT TREATMENT
FORM R (Hz)			FCGR (10 ⁻⁸ in/cycle)	FREG	ı	PRODUCT	CONDITION/

100.0

TABLE 3.13.1.2.9

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 300M AT ROOM TEMPERATURE

ORIENTATION: T-L

ENVIRONMENT: Lab Air

5 156.19	0.7 4.35	0.14		0.1-20	0.02	FORGING	UNSPECIFIED
5 50.0 100.0	10.0 20.0	6.8	2.5				
***	(A) (A) (A) (A) (A) (A) (A) (A) (A) (A)	4.7.44					
(m) 7	AR I amol (Ext./tm)	ZV	, ((HZ)	4	FORM	HEAT TREATMENT
				FRE	ı	PRODUCT	CONDITION/
cycle)	PCGR (10 ⁻⁸ inewla)	ECG					

TABLE 3.13.1.2.10

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK 300M AT ROOM TEMPERATURE

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		FCGR (10.4 in/cycle) AK Level (Ksi/in) 5.0 10.0 80.0 8	
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		CONDITION/ HEAT TREATMENT	
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TABLE 3.13.1.2.11

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK 300M AT ROOM TEMPERATURE

ORIENTATION: T-1	i T-L		ENVIRO]	ENVIRONMENT: S.T.W.	
CONDITION/ HEAT TREATMENT	PRODUCT FORM	R FREQ (Hz)	8.3	FCGR (10 ^d in/cyclθ) ΔK Level (Ksi/in) 5.0 10.0 20.0 50.0	1007
1700F 1.5HRS AC 1600F 1.5HRS OQ 600F 2+2HRS	FORGING	0.08			

TABLE 3.13.1.2.12

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK

ENVIRONMENT: L.H.A. 300M AT ROOM TEMPERATURE ORIENTATION: S-L

4.09			9 80.0	FORGING	1700F 1.5HRS AC 1600F 1.5HRS OQ 600F 2+2HRS
20.0 50.0 100.0	6.0 10.0	8:8			
Kut/in)	AK Land (Kol/in)	0	(Hz)	FORM	HEAT TREATMENT
		0		PRODUCT	CONDITION/
in/cycle)	FCGR (10 d in/cycle)				

TABLE 3.13.2.1

					ALLO	ALLOY STEEL	T 300M	M K _{Ie}							
	PRODUCT	oucr					SPECIMEN	,	CRACK			K			
CONDITION	FORM	THICK (fn.)	TEST TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (in.)	THICK (in.)	DEBIGN	LENGTH (in.) A	2.0 (K _{e,} TYS)* (in.)	K. (Kel •	K, MEAN	STAN	DATE	REFER
		1.25		•	239.0	2.504	1.267	CT	1.293	0.12	63.59			1977	MA005
	β	1.25	E	E	239.0	2.509	1.249	CT	1.279	0.13	65.50			1977	MA005
i	For Bring	1.26		<u></u> 1	246.5	2.505	1.251	CT	1.267	0.10	60.80	52.6	2.3	1977	MA005
		1.25			246.6	2.490	1.261	CT	1.286	0.10	50.70			1977	MA005
		1.25			240.0	2.496	1.256	CT	1.271	0.13	55.50			1977	MA005
	Í	1.25	E		240.0	2.512	1.254	CT	1.288	0.12	53.50			1977	MA005
*	rorging	1.25	표 		246.5	2.507	1.247	СТ	1.228	0.10	61.70	62.9	2.0	1977	MA005
		1.25			246.5	2.508	1.252	CT	1.296	0.10	60.90			1977	MA005
		5.50			245.0	1.501	0.760	ст	0.734	0.07	41.50			1970	84280 (1)
1600F 0.5 HR SQ 1000F 0.5-1.0 HR OQ 80-180F 25MIN 575F 2+2HR	Forging	5.50	26		245.0	1.503	0.750	CT	0.758	0.10	48.00	46.0	68	1970	84280 (1)
		6.50			245.0	1.505	0.747	ст	0.752	0.10	48.40			1970	84280 (1)
		5.50			231.0	1.499	0.745	CT	0.735	0.14	55.30			1970	84280 (1)
1600F 0.5 HR SQ 1000F 0.5-1.0 HR OQ 80-180F 25MIN 575F 2+ZHR	Forging	6.50	•	:	231.0	1.503	0.746	CI	0.742	0.16	58.70	67.1	1.7	1970	84280 (1)
		5.50			231.0	1.501	0.750	CT	0.736	0.15	67.20			0261	84280 (1)
		5.60			230.0	1.501	0.749	СT	0.737	0.19	64.30			1970	84280 (1)
1600F 0.5 HR SQ 1000F 0.5-1.0 HR OQ 80-180F 25MIN 575F 2+2HR	Forging	5.50	R.T.	;	230.0	1.499	0.750	CT	0.735	0.20	64.60	64.9	0.7	1970	84280 (1)
		6.60			230.0	1.504	0.750	CT	0.739	0.20	65.70			0261	84280 (1)
		5.60		L	220.0	1.502	0.749	CT	0.729	0.25	68.90			1970	84280 (1)
1600F 0.5 HR SQ 1000F 0.5-1.0 HR OQ 80-180F 25MIN 575F 2+2HR	Forging	5.50	200		220.0	1.500	0.746	CT	0.734	0.24	67.70	68.2	9.0	1970	84280 (1)
		2.50			220.0	1.499	0.745	ct	0.734	0.24	68.10			1970	84280 (1)

2 of 3

TABLE 3.13.2.1 (CONTINUED)

					ALLO	ALLOY STEEL	L 300M	M K _{Ie}							
	PROI	PRODUCT				92	SPECIMEN	7	CRACK			K _{Io}			
CONDITION	FORM	тніск (ів.)	TEST TEMP (°F)	SPEC	YIELD STR (Kal)	WIDTH (in.) W	THICK (in.) B	DESIGN	LENGTH (In.)	2.6 (K. TYS)* (ln.)	K. (Kai •	K. MEAN	STAN	DATE	REFER
		3.00		L	237.0	1.002	0.247	CT	0.491	0.15	56.10			1973	85836
erro. o door oo day se t door o	ŕ	3.00	E	I	237.0	1.002	0.247	CT	0.495	0.15	57.10			1973	85836
1000F 1.20 IIN OG 600F 2+2IIN	rorging	3.00	1	<u> </u>	237.0	1.000	0.249	ст	0.495	0.13	61.60	54.6	2.5	1973	85836
		3.00			237.0	1.002	0.248	cr	0.502	0.14	53.80			1973	85836
dire, o door oo dir no t door	Ē	3.00	E	l	240.0	1.002	0.248	cr	0.507	0.13	61.80			1973	85836
1900F 1.20 ftN U¶ 600F 2+2ftN	rorging	3.00	K.I.	72	240.0	0.987	0.247	СТ	0.492	0.12	49.40	50.6	1.7	1973	85836
		3.00			230.0	1.005	0.248	CT	0.496	0.14	55.10			1973	85836
The co door of the second of t	ģ	3.00	6		230.0	1.002	0.248	CT	0.497	0.13	52.80			1973	85836
1900F 1.20 HK UY 500F Z+ZHK	rorging	3.00	7. T.	,	230.0	1.004	0.247	СТ	0.504	0.14	64.90	64.1		1973	85836
		3.00			230.0	1.000	0.248	CT	0.485	0.14	53.60			1973	85836
1600F 1HR OQ 1HR WQ 475 1HR	Bar	0.62	R.T.	LT	240.0	2.000	0.600	CT	1.000	0.05	34.30		1	1973	87241 (1)
1600F 1HR OQ 475F 1HR	Bar	0.62	R.T.	L.T	240.0	2.000	0.600	CT	1.000	0.06	34.80	:		1973	87241 (1)
1600F 1HR OQ 575F 1HR	Bar	0.62	R.T.	7.	245.0	2.000	0.600	CT	1.000	0.15	69.40	!		1973	87241 (1)
1600F 1HR OQ 615F 1HR	Bar	0.62	R.T.	LŢ	246.0	2.000	0.600	ÇŢ	1.000	0.15	60.90	ı	!	1973	87241 (1)
1600F 1HR OQ 746F 1HR	Bar	0.62	R.T.	LT	245.0	2.000	0.600	CT	1.000	0.17	64.80	ı	1	1973	87241
1600F OQ 550F 2+2HR	Plate	0.56	R.T.	LT	236.0	1.500	0.500	NB	:	0.20	66.00	•	1	1970	78305 (2)
		1.00		L	200.0	1.997	1.012	cr.	1.137	0.42	81.50			1973	85883 (3)
1675F AC 1675F OQ 1100F 2 HR	Ē	1.00	Ē		200.0	1.989	1.010	CT	1.139	0.45	84.80			1973	85883 (3)
(RC 39)	S) HI	1.00	į	.	200.0	1.996	1.010	cr	1.123	0.43	82.90	81.4	3.7	1973	85883 (3)
		1.00			200.0	2.000	1.009	cr	1.103	0.36	76.20			1973	85883 (3)
1675F AC 1675F OQ 500F 2 HR	7	1.00	Ę		240.0	1.995	1.010	cT	1.054	60:0	46.20			1973	85883 (3)
(RC 61.5)		1.00			240.0	2.001	1.010	CT	1.092	0.12	62.60	49.1	3.6	1973	85883 (3)

TABLE 3.13.2.1 (CONCLUDED)

					ALLO	ALLOY STEEL	L 300M	M K _I							
	PROI	PRODUCT				W	SPECIMEN	-	CRACK			₩ o,			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (in.)	THICK (in.)	DESIGN	LENGTH (in.) A	2.6 ° (K _{e,} TYS)* (in.)	K. (Red •	K. MEAN	STAN	DATE	REFER
1675F AC 1575F OQ 500F 2 HR	Plate	1.00	R.T.	;	240.0	2.001	1.010	CT	1.147	60.0	46.90			1973	85883 (1)
(RC 51.5) Cont'd	Cont'd	1.00	Cont'd	Cont'd	240.0	1.996	1.010	CT	1.065	0.12	51.80	Cont'd	Cont'd	1973	85883 (1)
		1.00			220.0	1.998	1.010	CŢ	1.122	0.13	50.10			1973	85883 (1)
1675F AC 1575F OQ 800F 2HR	Plate	1.00	R.T.	I	220.0	1.995	1.010	CT	1.081	0.13	49.60			1973	85883 (1)
(RC 47.5)		1.00			220.0	1.988	1.010	CT	1.088	0.12	47.30	49.2	1.3	1973	85883 (1)
		1.00			220.0	1.994	1.010	CT	1.068	0.13	49.80			1973	85883 (1)
		1.00			236.0	1.000	0.500	NB	0.490	0.12	62.40			1974	88136
1700F 1HR AC 1600F 1HR OQ 600F 2HR AC	Plate	1.00	R.T.	ŗ	236.0	0.995	0.502	NB	0.491	0.12	61.00	61.8	7.0	1974	88136
		1.00			236.0	0.991	0.501	NB	0.485	0.12	52.00			1974	88136
2190F 1HR FC TO 1600F HOLD	í	0.62	Ę		235.0	2.000	0.600	CT	1.000	0.12	50.60			1973	87241
0.5HR OQ 476F 1HR	bar	0.62	K.F.	1	235.0	2.000	0.600	CT	1.000	0.09	45.20	47.9	3.8	1973	87241
2190F 1HR FC TO 1600F HOLD 0.5HR OQ 616F 1HR	Bar	0.62	R.T.	LT	240.0	2.000	0.600	CT	1.000	0.12	62.70	ı	ı	1973	87241
2190F 1HR FC TO 1600F HOLD 0.5HR OQ 745F 1 HR	Bar	0.62	R.T.	LT	240.0	2.000	0.600	cr	1.000	0.18	63.50	:	:	1973	87241
2190F 1HR OQ 400F 1HR	Bar	0.62	R.T.	LT	219.0	2.000	0.600	CT	1.000	0.29	75.90	ï	1	1973	87241
2190F 1HR OQ 475F 1 HR	Bar	0.62	R.T.	LT	230.0	2.000	0.600	CT	1.000	0.23	69.20	***	1	1973	87241
2190F 1HR OQ 476F 1HR WQ 476F 1HR	Bar	0.62	R.T.	LT	232.0	2.000	0.600	CT	1.000	0.24	71.80			1973	87241
2190F 1HR OQ 615F 1HR	Bar	0.62	R.T.	LT	236.0	2.000	0.600	CT	1.000	0.26	75.50	:	1	1973	87241
2190F 1HR OQ 745F 1HR	Bar	0.62	R.T.	L.T	240.0	2.000	0.600	CT	1.000	0.24	74.70		;	1973	87241
HEAT TREATED TO	Ē	1.00	E	Ė	250.0	0.904	0.447	NB	0.485	0.12	56.10			1971	84029 (2)
64 RC HARDNESS	Finte	1.00	K.T.	1-I	250.0	0.903	0.448	NB	0.473	0.15	61.10	58.6	3.5	1971	84029 (2)

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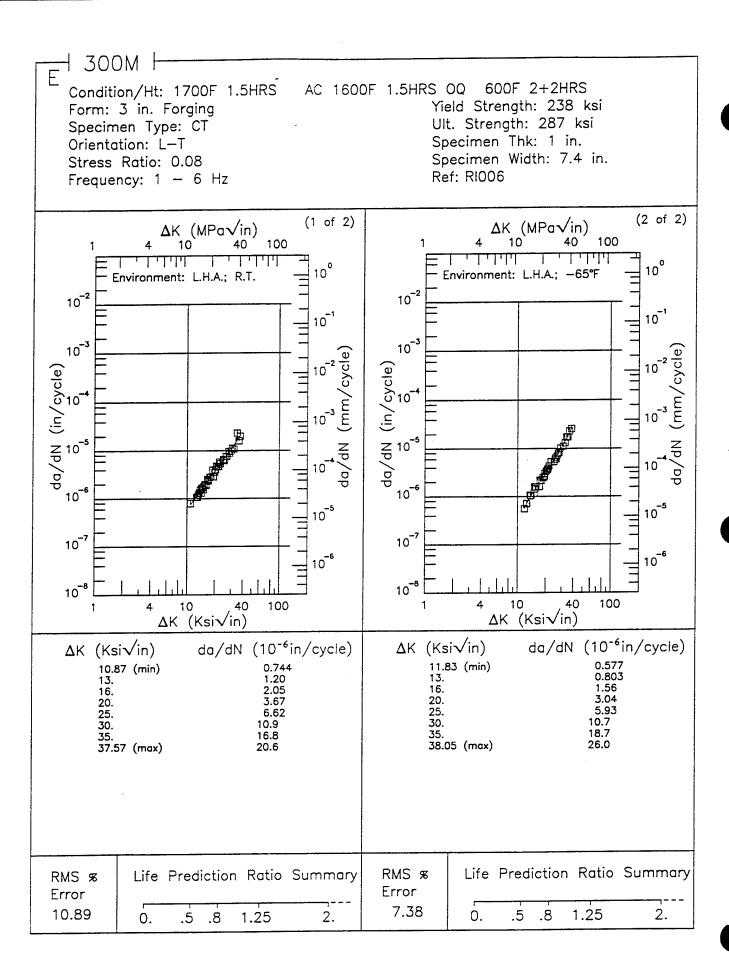


Figure 3.13.3.1.1

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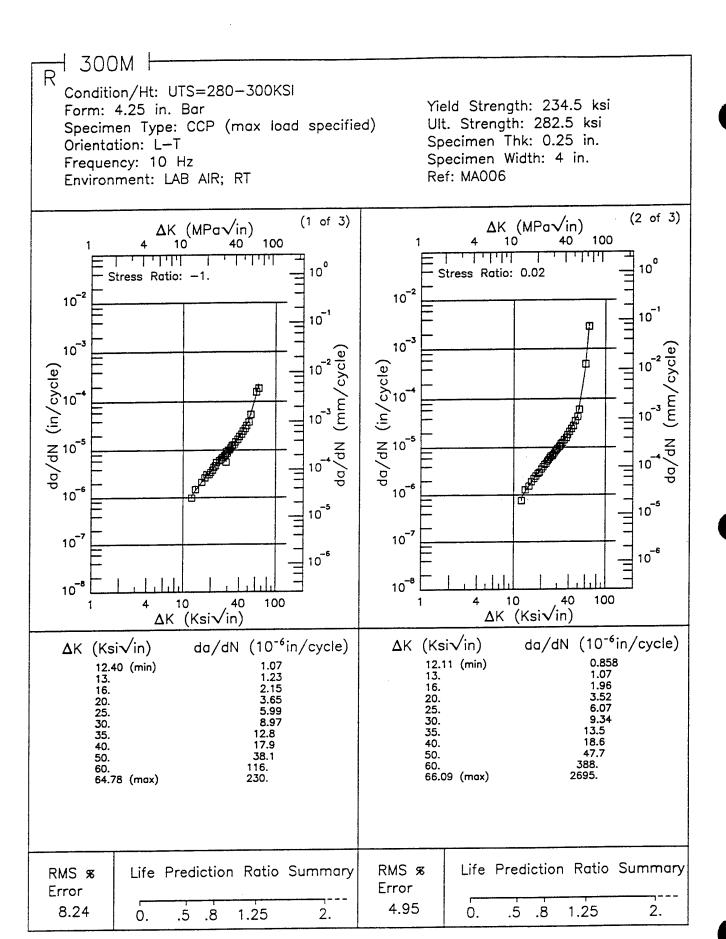


Figure 3.13.3.1.2

300M H Condition/Ht: UTS=280-300KSI Yield Strength: 234.5 ksi Form: 4.25 in. Bar Ult. Strength: 282.5 ksi Specimen Type: CCP (max load specified) Specimen Thk: 0.25 in. Orientation: L-T Specimen Width: 4 in. Frequency: 10 Hz Ref: MA006 Environment: LAB AIR; RT (3 of 3)ΔK (MPa√in) ΔK (MPa \sqrt{in}) 100 100 11111 10° 100 Stress Ratio: 0.5

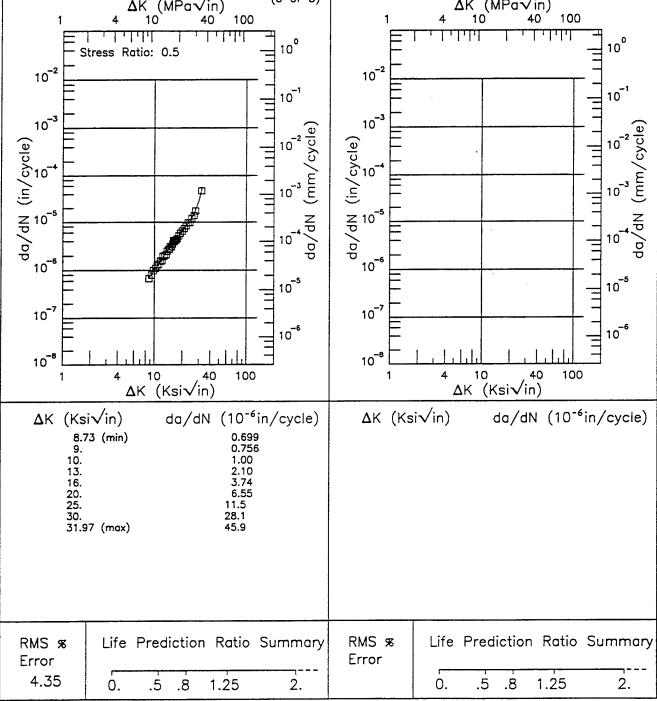


Figure 3.13.3.1.2 (Concluded)

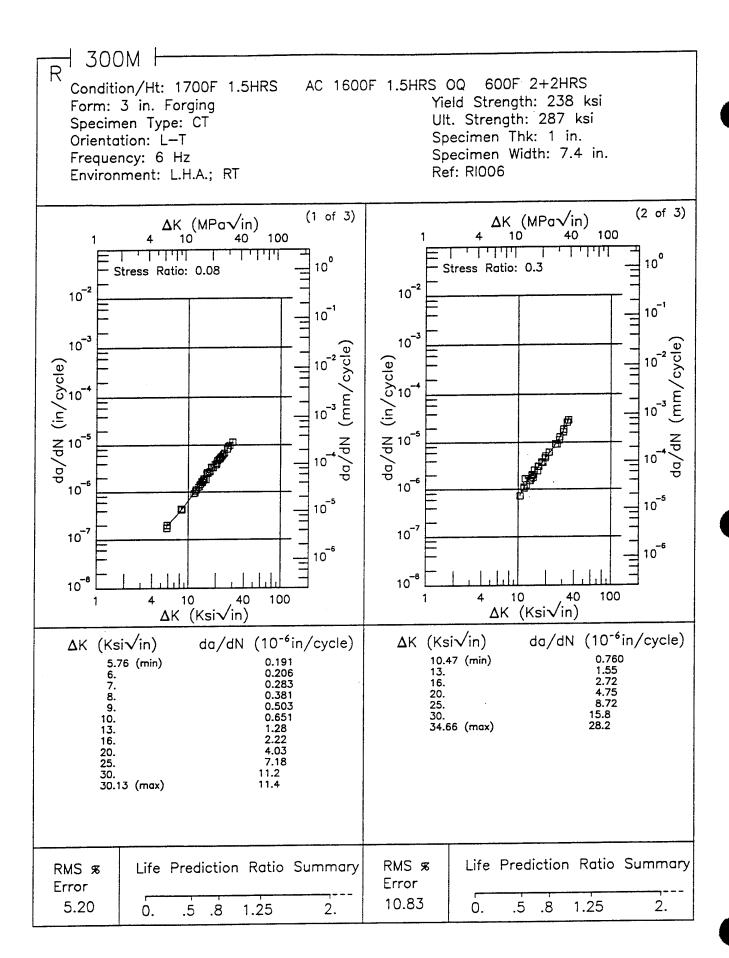


Figure 3.13.3.1.3

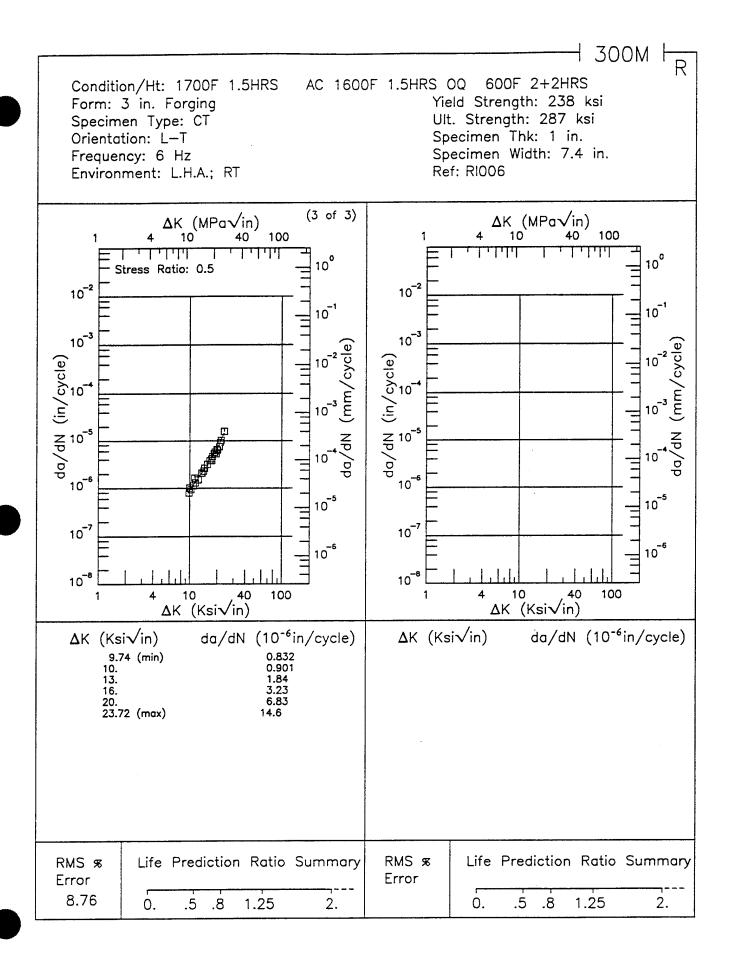


Figure 3.13.3.1.3 (Concluded)

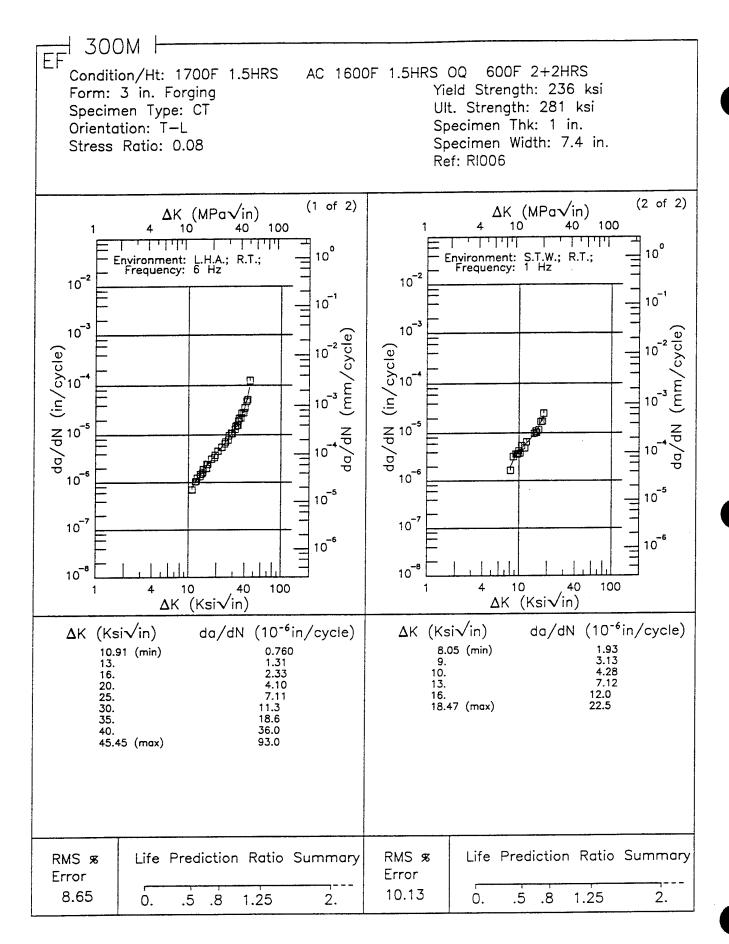


Figure 3.13.3.1.4

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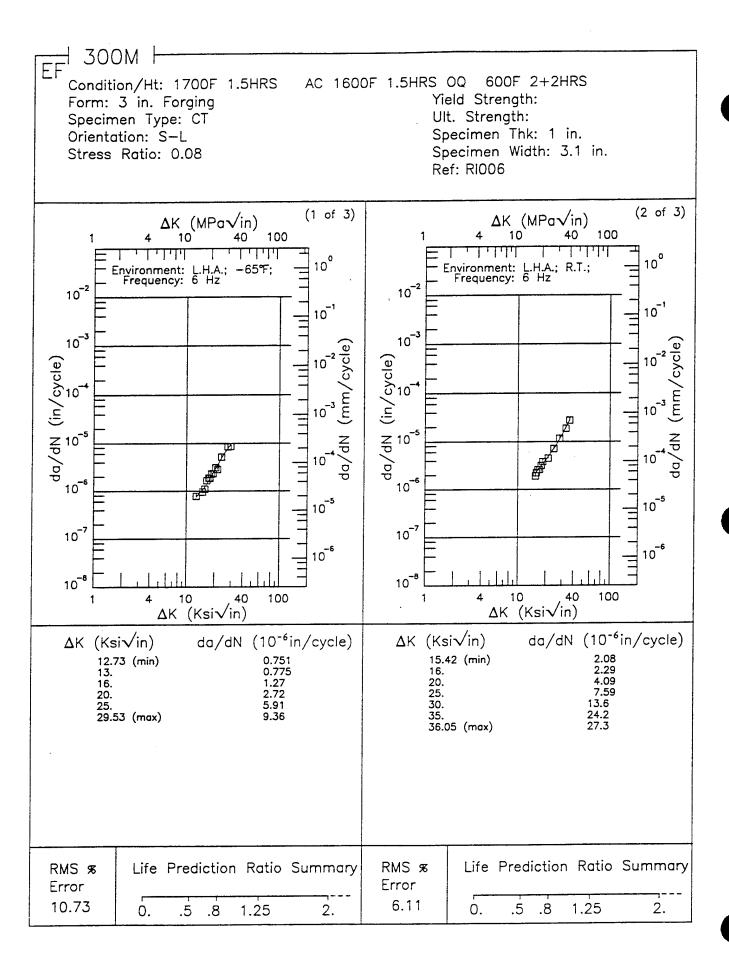


Figure 3.13.3.1.5

1 300M | EF AC 1600F 1.5HRS OQ 600F 2+2HRS Condition/Ht: 1700F 1.5HRS Form: 3 in. Forging Yield Strength: Ult. Strength: Specimen Type: CT Specimen Thk: 1 in. Orientation: S-L Specimen Width: 3.1 in. Stress Ratio: 0.08 Ref: RI006 (3 of 3)ΔK (MPa√in) Δ K (MPa \sqrt{in}) 10 40 100 100 10° ليليليا 10° Environment: S.T.W.; R.T.; Frequency: 1 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ 10-2 da/dN (in/cycle) da/dN (in/cycle) 10⁻³ 10 10⁻⁵ 10⁻⁵ 10⁻⁷ 10⁻⁷ 10⁻⁶ 10-6 10⁻⁸ 10-8 10 100 100 40 10 40 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error .5 1.25 2. 0. .5 .8 1.25 2. 0. .8

Figure 3.13.3.1.5 (Concluded)

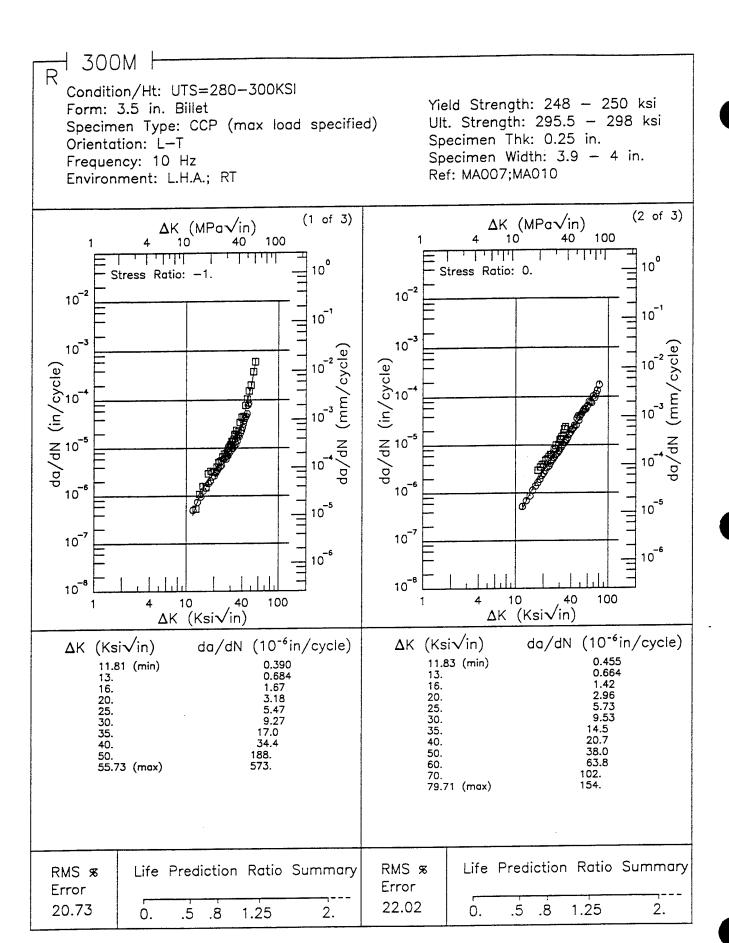


Figure 3.13.3.1.6



Condition/Ht: UTS=280-300KSI

Form: 3.5 in. Billet

Specimen Type: CCP (max load specified)

Orientation: L-T Frequency: 10 Hz Environment: L.H.A.; RT Yield Strength: 248 - 250 ksi Ult. Strength: 295.5 - 298 ksi

Specimen Thk: 0.25 in.

Specimen Width: 3.9 - 4 in.

Ref: MA007;MA010

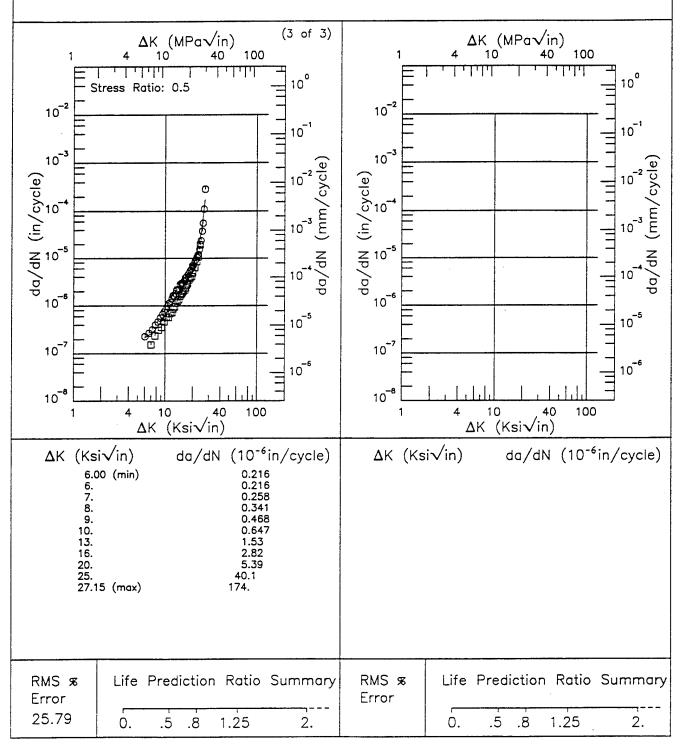


Figure 3.13.3.1.6 (Concluded)

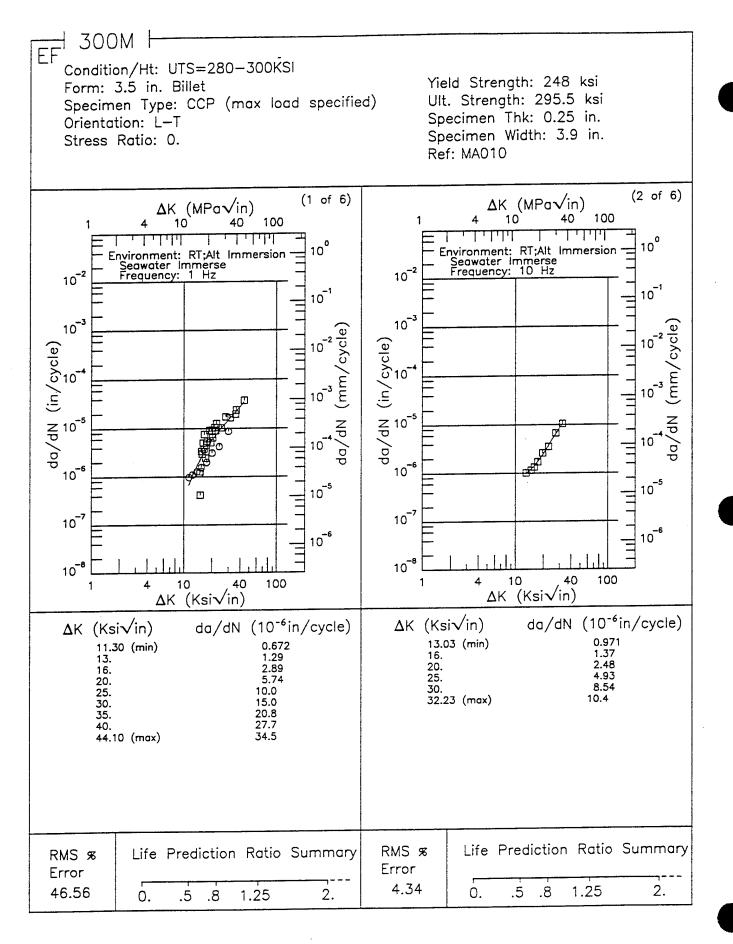


Figure 3.13.3.1.7

4 300M EF Condition/Ht: UTS=280-300KSI Yield Strength: 248 ksi Form: 3.5 in. Billet Ult. Strength: 295.5 ksi Specimen Type: CCP (max load specified) Specimen Thk: 0.25 in. Orientation: L-T Stress Ratio: 0. Specimen Width: 3.9 in. Ref: MA010 (4 of 6)(3 of 6) Δ K (MPa \sqrt{in}) ΔK (MPa√in) 100 10 40 100 10 40 10° 10° Environment: RT;Alt Immersion Seawater—1st Half Dry Cycle Frequency: 10 Hz Environment: RT;Alt Immersion Seawater—1st Half Dry Cycle Frequency: 1 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ 10-2 da/dN (in/cycle) (in/cycle) 10 10 Np/pp 10 10⁻⁶ 10⁻⁶ 10 -5 10⁻⁵ 10⁻⁷ 10⁻⁷ 10 -6 10⁻⁶ 10-8 10 8 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) da/dN ($10^{-6}in/cycle$) ΔK (Ksi \sqrt{in}) ΔK (Ksi√in) 1.42 2.51 7.06 14.74 (min) 11.22 (min) 0.382 0.543 16. 13. 20. 25. 16. 1.01 20. 2.17 25. 30. 30. 14.8 4.65 35. 18.0 8.12 40. 11.9 37.07 (max) 50. 50.6 13.4 51.60 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS & Error Error 44.44 17.96 .5 1.25 0. .5 .8 1.25 2. 0. .8 2.

Figure 3.13.3.1.7 (Continued)

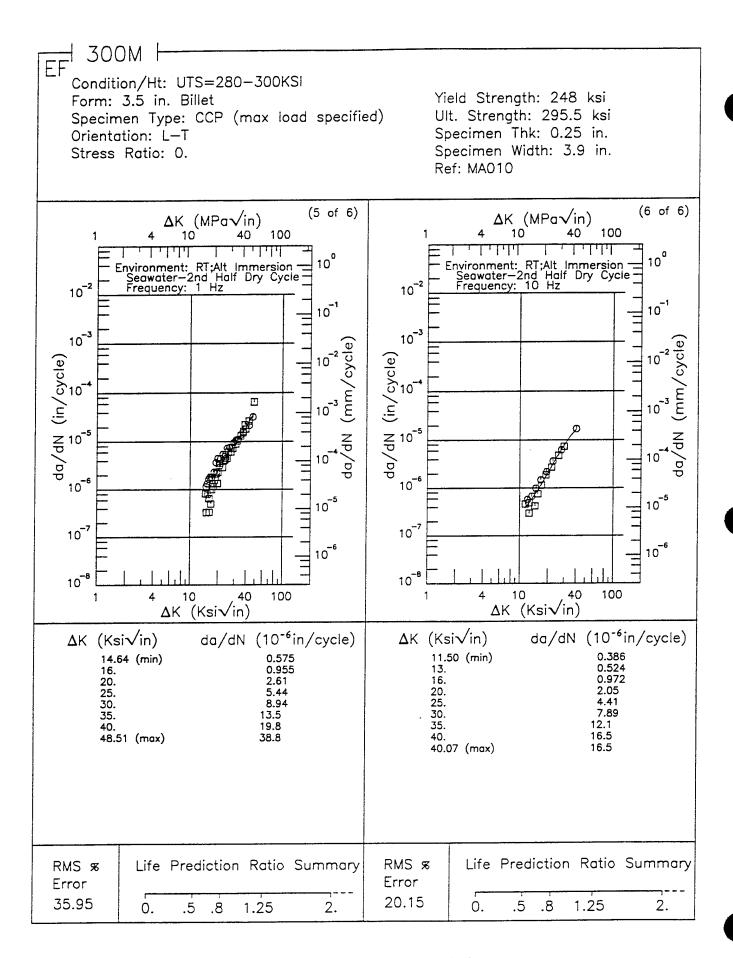


Figure 3.13.3.1.7 (Concluded)

1 300M F

Condition/Ht: UTS=280-300KSI

Form: 3.5 in. Billet

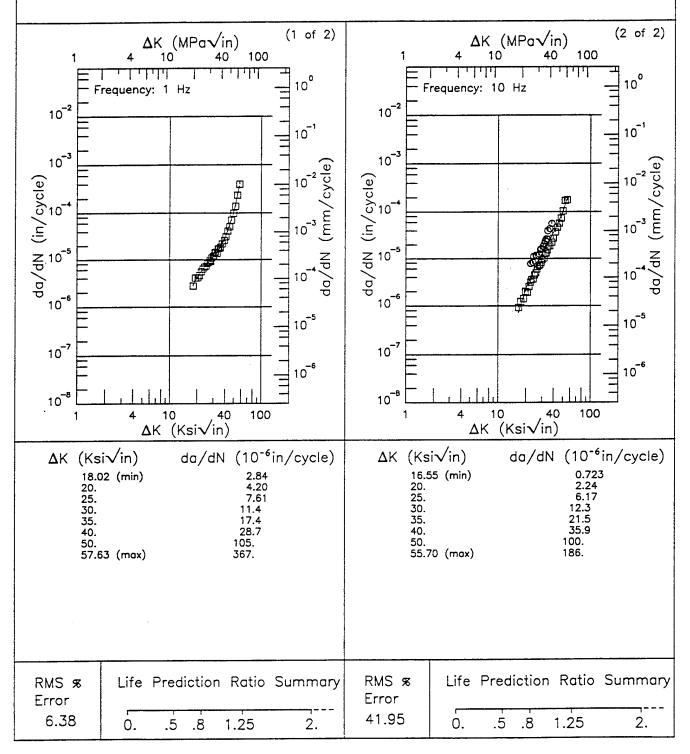
Specimen Type: CCP (max load specified)

Orientation: L-T Stress Ratio: 0.

Environment: 3.5% NACL; RT

Yield Strength: 250 ksi Ult. Strength: 298 ksi Specimen Thk: 0.25 in. Specimen Width: 4 in.

Ref: MA007



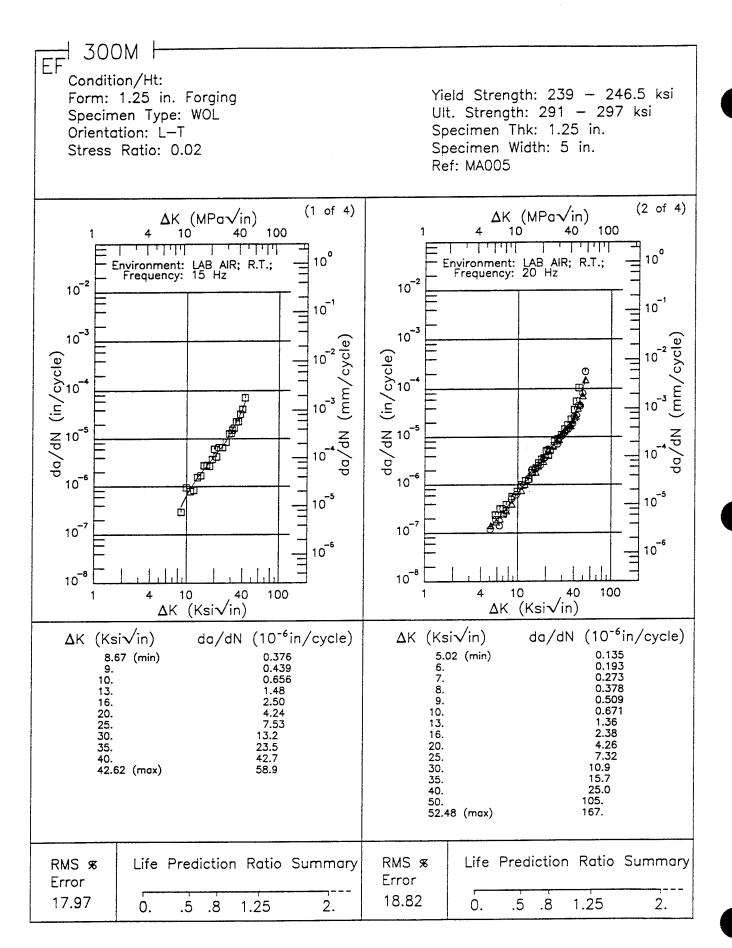


Figure 3.13.3.1.9

1 300M | EF

Condition/Ht:

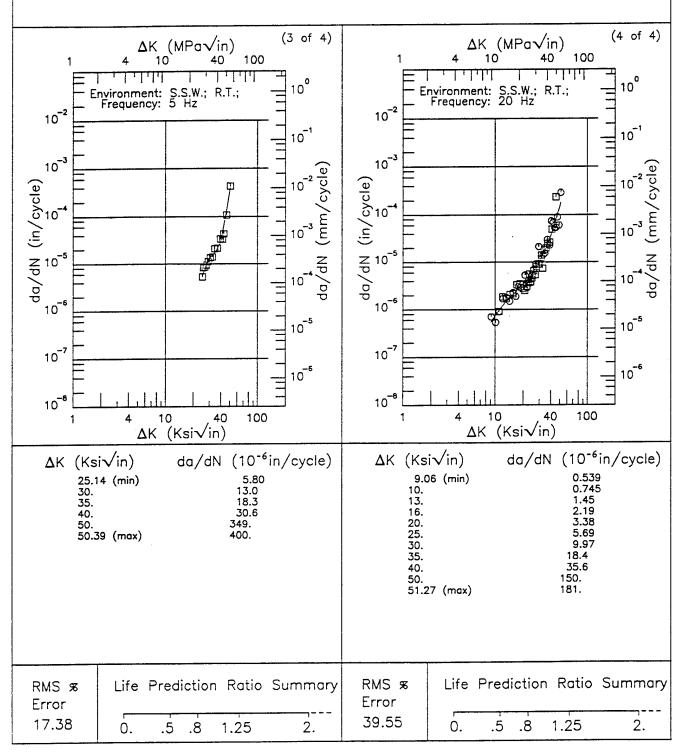
Form: 1.25 in. Forging Specimen Type: WOL Orientation: L—T

Stress Ratio: 0.02

Yield Strength: 239 - 246.5 ksi Ult. Strength: 291 - 297 ksi

Specimen Thk: 1.25 in. Specimen Width: 5 in.

Ref: MA005



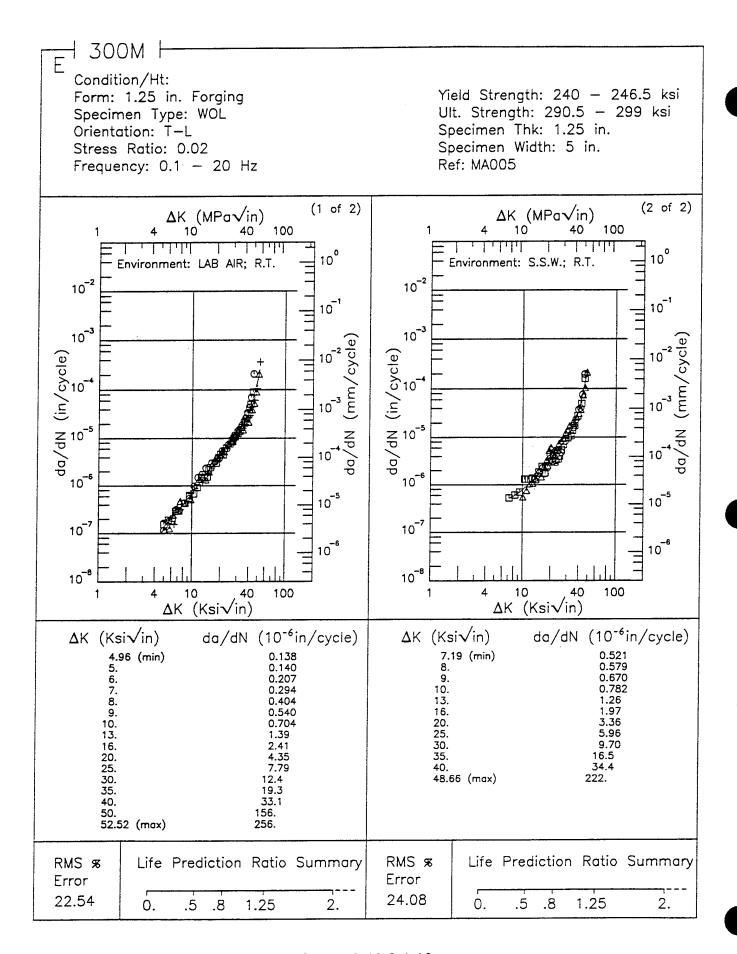


Figure 3.13.3.1.10

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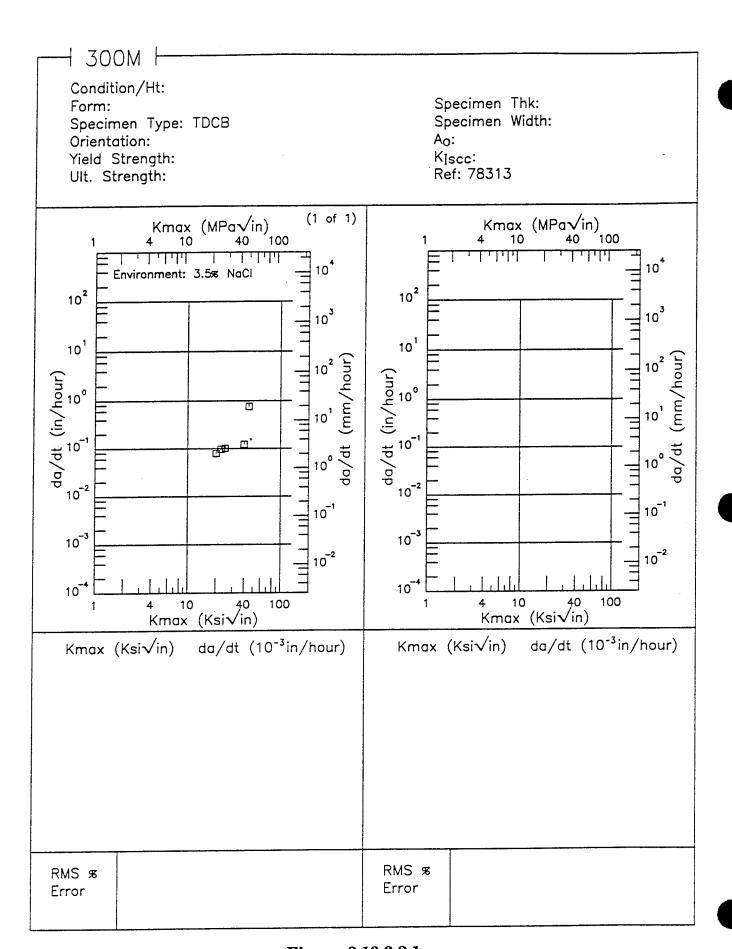


Figure 3.13.3.2.1

1 300M F Condition/Ht: 1600F OQ 575F 2+2HR Form: 0.1 in. Sheet Specimen Thk: 0.1 in. Specimen Type: DCB Specimen Width: Orientation: T-L Ao: Yield Strength: 245 ksi K_{Iscc}: Ref: 85545 Ult. Strength: (1 of 1) Kmax (MPa \sqrt{in}) Kmax (MPa√in) ∮ 10 40 1 100 100 10 40 11111 للبليا 104 Environment: Distilled Water 10² 10² 103 103 101 101 da/dt (mm/hour) da/dt (in/hour) da/dt (in/hour) 卢 10-2 10 -2 10-1 10-1 ⍗ 10⁻³ 10⁻³ 10-2 10⁻² 10 10 4 10 40 Kmax (Ksi√in) 4 10 40 Kmax (Ksi√in) 100 100 Kmax (Ksi√in) $da/dt (10^{-3}in/hour)$ Kmax (Ksi√in) $da/dt (10^{-3}in/hour)$ 12.80 (min) 13. 16. 20. 25. 30. 35. 40. 50. 60. 70. 80. 82.00 (max) 5710. RMS % RMS % Error Error 52.15

Figure 3.13.3.2.2

TABLE 3.13.3.3

K_{Isce} SUMMARY FOR ALLOY STEEL 300M

		50000000	1	0000000							l
	Refer	84351	74302	MA005	MA005	MADOE	MADDE	78305	76305	78305	78305
1	Test Date	1971	1967	1977	1977	1977	1977	1970	1970	1970	1970
Test	Time (min)		i	86400	86400	86400	86400	l	į		1
	K _{le∞} (Ksi√in)	12	13	15.4	15.4	15.7	15.6	12	15	12	15
	Ko (Ksi√in)	89	92	i	***		i	36	42	09	26
	Crack (in)	0.3	i	1.35	1.35	1.36	1.37	l	i	ı	1
Prod	Thk (in)	i	0.48	1.25	1.25	1.25	1.25	0.56	0.56	0.56	0.56
	Thick (in)	0.5	0.48	1.242	1.247	1.249	1.251	0.5	9.6	0.5	0.5
Specimen	Width (in)	1.5	1.5	3.091	3.088	3.101	3.091	1.5	1.5	1.5	1.5
S	Design	CANT.	NB	BWOL	BWOL	BWOL	BWOL	CANT.	CANT.	CANT.	CANT
	Envir.	3.5% NaCl	3.5% NaCl		Sim. Sea	Water		3.5% NaCl	3.5% NaCl	3.5% NaCl	3.5% NaCl
Yield	Str (Ksi)	289	236		0 070	2.04.2		202	232	245	247
2	Spec Or.	**	r-s		Ę	Τ. Ω		:	:		
Test	Temp (°F)	R.T.	R.T.		Ę	; ;		R.T.	R.T.	R.T.	R.T.
	Form	P	Р		¢	4		Ъ	P	Ъ	Ь
Condition	Condition Heat Treat	Unspecified	Unspecified		Thancoiffed	namadeno		1500°F 0.5hr OQ; 400°F 2+2 hr (Coarse Grained Structure)	1500°F 0.5hr OQ; 550°F 2+2 hr (Coarse Grained Structure)	1500°F 0.5hr OQ; 400°F 2+2 hr (Fine Grained Structure)	1500°F 0.5hr OQ; 550°F 2+2 hr (Fine Grained Structure)

TABLE 3.13.3.3 (CONTINUED)

K_{Isc} SUMMARY FOR ALLOY STEEL 300M

Prod Test		Spec	Yield		is	Specimen			1000		7	Test	†20E	
Temp (°F)	Or. (Ksi)		Envir	.•	Design	Width (in)	Thick (in)	Thk (in)	(in)	(Ksi√in)	Rsi√in)	Time (min)	Date	Refer
P R.T 240 3.5% NaCl	240		3.5% Na(5	CANT.	1.5	0.5	0.56	l	53	15	l	1970	78305
P R.T 241 3.5% NaCl	241		3.5% Nat	- 5	CANT	1.5	0.5	0.56	1	53	1.6	i	1970	78305
P R.T 246 3.5% NaCl	246		3.5% NaC		CANT'	1.5	0.5	0.56	i	09	15	i	1970	78305
P R.T 248 3.5% NaCl	248		9.5% NaC	-	CANT	1.5	0.5	0.56	1	64	15	i	1970	78305
P R.T 220 3.5% NaCl	220		3.5% Na(5	CANT.	1.5	0.5	0.56	l	67	12	l	1970	78305
P R.T 232 3.5% NaCl	232		3.5% Na(5	CANT"	1.5	0.5	0.56	ı	65	12	-	1970	78305

(3 of 4)

TABLE 3.13.3.3 (CONTINUED

 $K_{\rm Isco}$ SUMMARY FOR ALLOY STEEL 300M

/==;+;[-==5,	D. J.	Test	0	Yield		S	Specimen		Prod			1	Test	·	
Condition Heat Treat	Form	Temp (°F)	or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)		(in)	Kai√in)	K _{lo} (Ksi√in)	Time (min)	Test Date	Refer
1600°F 0.5hr OQ 550°F 2+2 hr (Fine Grained Structure)	Ъ	R.T.		245	3.5% NaCl	CANT.	1.5	0.5	0.56	ı	65	12	l	1970	78305
1650°F 1525F OQ 600°F 2+2 hr	F	R.T.		247	Air-90% RH	DELG	1.5	0.48	ı,	9.14	73.9	11	i	1965	74718
1650°F 1600°F 1hr OQ 600°F 1+1 hr	F	R.T.	r-s	251.5	3.5% NaCl	CANT	1.5	0.48	4	-	63.5	19.6	l	1965	74718
1700°F 1.5hr AC 1600°F 1.5hr OQ 600°F 2+2hr	<u>[</u> -	R. F.	L-T	238	F.C.S. S.C.S.	DCB DCB DCB DCB DCB DCB DCB DCB					150 150 150 150 150 150	241 239 39 39 36 225 225 225 225	116760	1976 1976 1976 1976 1976 1976	R1006 R1006 R1006 R1006 R1006 R1006 R1006
			T-S	;	S.T.W.	DCB	2	1	3	:	150	16+	76200	1976	RI006
						DCB	2	1	က	i	150	15+	76200	1976	RI006

TABLE 3.13.3.3 (CONCLUDED)

K_{lsce} SUMMARY FOR ALLOY STEEL 300M

,	<u></u>	Test	5	Yield		20	Specimen		Prod		1	1	Test		
Condition/ Heat Treat	Form	$egin{array}{c c} Frod & Temp & Spec & Str \ (^oF) & Or. & (Ksi) \ \hline \end{array}$	Spec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)	Thk (in)	Crack (in)	hq (Ksi√in	(Ksivin)	Time (min)	Test Date	Refer
1710°F+1610°F AC 1600°F 1.5hr OQ 600°F 2+2hr	В	R.T.	T-T	250	3.5% NaCi	NB	1	9.0	6.63	i	58.9	81	i	1971	84087
			5	t .	N 20 0	NB	н	0.5	0.63	ij	59.8	17.6		1971	84087
			L-1	200	3.0% NaCi	NB	Н	0.5	0.63	1	54.7	16.7		1971	84087
1710°F+1610°F		Ę				LO		9.0	69.0	1	61.2	18.9		187.1	84087
610°F	9	F. I.	E	0 2 0	Dew Medi	LO	į	0.5	0.63	:	51.5	16.3		1971	84087
	· · ·		7-1	200	Davi a n.	CT	i	0.5	0.63	ŧ	55.5	18		1971	84087
						CT	-	0.8	0.63		65.9	17.3		1071	84087

 $^{+}$ specimen thickness does not meet minimum requirements of $2.5~(rac{K_{loo}}{\sigma_{ys}})^{2}$

* asterisk in specimen design column indicates that specimens are side-grooved

1 of 1

TABLE 3.14.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL 300M (AM) AT ROOM TEMPERATURE

Product					K_{Ic}	$K_{lc}~(ksi\!\sqrt{in})$	(a			
Form	Condition/Heat Treatment			S	pecime	Specimen Orientation	ntation			
			L-T			T-L			S-L	
		Mean K _i ,	Std Dev	ជ	Mean K _{lo}	Std Dev	u	Mean K _{le}	Std Dev	ч
Forging	1650F 1HR AC 1550F 1HR OQ -320F 0.5HR 600F 2+2HR AC	46.5	3.8	3	:	i	:	i	i	i

				7	ALLOY STEEL	STEEL	300M	300M (AM) K _I	اور						
	PRODUCT	UCT				- Gr	SPECIMEN		CRACK			K_{Ie}			
CONDITION	FORM	THICK (In.)	TERF TEMP (°F)	SPEC	YIBLD STR (KA)	WIDTH (In.)	THICK (in.)	DEBIGN	LENGTH (fb.) A	(fr., TYB)* (in.)	K. (K.d • Vin.)	K. MBAN	BTAN DEV	DATE	REFER
		4.00			262.0	1.800	0.900	NB NB	1	0.07	43.60			1968	73300
1650F 1 HR AC 1650F 1 HR OQ -320F 0.5 HR 600F 2+2 HR AC	Forging	4.00	R.T.	ż	262.0	1.800	0.900	NB	1	0.07	45.10	46.5	80	1968	13300
		4.00			262.0	1.800	0.900	NB NB	1	0.08	60.80			1968	73300

TABLE 3.15.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL 300M (VAR) AT ROOM TEMPERATURE

			ď	:
		S-L	Std Dev	:
			Mean K _{le}	!
<u>n</u>)	ntation		u	ŀ
$K_{Ic}~(ksi\!\sqrt{in})$	Specimen Orientation	T.L	Std Dev	!
K_{Ic}	pecime		Mean K _{le}	l
	S		E	4
	is		Std Dev	1.3
			Mean K _{te}	52.2
	Condition/Heat Treatment			1650F 1HR AC 1550F 1HR OQ -320F 0.5HR 600F 2+2HR AC
Product	Form			Forging

				A	ALLOY STEEL	TEEL	300M (VAR)	VAR)	K _{fe}						
	PROI	PRODUCT					SPECIMEN	7	CRACK			Kı			
СОИВІТІОН	FORM	THICK (fm.)	TEMP TEMP (°F)	SPEC	YIRLD STR (Kal)	WIDTH (In.)	THICK (in.) B	DEBIGN	LENGTH (In.) A	(K. TYS)* (in.)	K. (Kal •	K. MBAN	etan DEV	DATE	RBFER
		4.50		1	259.0	1.800	0.900	NB	-	0.10	61.10			1968	73300
1650F 1 HR AC 1550F 1 HR OQ	Į.	4.50	Ē		259.0	1.800	0.900	NB	ı	0.11	63.60			1968	73300
-320F 0.5 HR 600F 2+2 HR AC	Lorging.	4.50	1	3	259.0	1.800	0.900	NB	ı	0.11	63.00	62.2	1.3	1968	73300
		4.50			259.0	1.800	0.900	NB	1	0.10	61.20			1968	73300

TABLE 3.16.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL 300 (VM) AT ROOM TEMPERATURE

5					K_{Ic}	$K_{Ic}~(ksi\!\sqrt{in})$	<u>િ</u>			
Form	Condition/Heat Treatment			S	Specimen Orientation	n Orier	itation			
			LT			T-T			S-L	
		Mean K _{le}	Std Dev	u	Mean K _{le}	Std Dev	u	Mean K _{ie}	Std Dev	п
	1500F OQ 400F 2+2HR	48	17.	2	:	:	ı	i	ŧ	:
Plate	1500F OQ 550F 2+2HR	49.5	10.6	2					:	:
	1550F OQ 550F 2+2HR	62.5	3.5	2			:	:	•	÷
	1700F AC 1600F 1HR OQ 550F 2+2HR	:	:	••	55.3	0.3	3		••	•••
Billet	1700F AC 1600F 1HR SQ 400F AC 550F 2+2HR	:	-	***	58.	3.4	3			:
	1700F AC 1600F 1HR SQ 976F OQ 576F 2+2HR	i	**	:	58.6	2.2	3		•	:

				1	ALLOY	ALLOY STEEL	300M(VM)		K _{Io}							
	PROI	PRODUCT				_	SPECIMEN	7	CRACK			K _I °				7
CONDITION	FORM	THICK (In.)	TEST TEMP (F)	SPEC OR	YIRLD STR (Kal)	WIDTH (in.) W	THICK (lb.) B	DESIGN	LENGTH (in.) A	(K _w ,TY8) ² (in.)	K. (Kel •	K. MEAN	BTAN	DATE	REFER	
1500B OO 400B 9.9UB	Ē	0.56	£	l	202.0	1.500	0.500	NB	1	90'0	36.00			1970	78305	T
1000F ON 400F 2+211A	F1816	0.56	K.I.	3	245.0	1.500	0.500	NB	1	0.15	60.00	48.0	17.0	1970	78305 (1)	Г
ano a comp	Ē	0.56	£	1	233.0	1.500	0.500	NB	1	90'0	42.00			1970	78305	
1000 TO 1000 TO 1000	Filate	0.56	F. I.	3	248.0	1.500	0.500	NB	1	61.0	67.00	49.5	10.6	1970	78305 (1)	$\overline{}$
1550F OQ 400F 2+2HR	Plate	0.56	R.T.	፤	242.0	1.500	0.500	NB		0.12	53.00	I	1	1970	78305	1
drie e don't co don't	Ē	0.56	E	I	248.0	1.500	0.500	NB	:	0.15	60.00			1970	78305	1
1990F Og 500F 2+2HK	Flate	0.56	.	I.	248.0	1.500	0.500	BN	1	0.17	65.00	62.5	3.5	1970	78305 (1)	1
1600F OQ 400F 2+2HR	Plate	0.56	R.T.	1.1	220.0	1.500	0.500	NB	1	0.22	66.00	i	i	1970	78305	1
1600F OQ 550F 2+2HR	Plate	0.56	R.T.	1.7	233.0	1.500	0.500	NB		0.20	66.00	i	!	1970	78305	_
		5.50		t	239.0	2.500	1.000	cT	:	0.14	65.60			1972	84278	1
1700F AC 1600F 1HR OQ 650F 2+2HR	Billet	6.60	R.T.	<u></u> -	239.0	2.500	1.000	CT	:	0.13	55.30	66.3	0.3	1972	84278	
		5.50			239.0	2.500	1.000	cr	**	0.13	65.00			1972	84278	=
		5.50		1	244.0	2.500	1.000	cr	ï	0.14	66.70			1972	84278	1
1700F AC 1600F 1HR SQ 400F AC 550F 2+2HR	Billet	6.50	R.T.	7 <u>.</u>	244.0	2.500	1.000	cT	***	0.16	61.80	28.0	89	1972	84278	1
		6.50			244.0	2.500	1.000	cr	:	0.13	55.40			1972	84278	
		6.50			242.0	2.500	1.000	cr		0.16	60.80			1972	84278	
1700F AC 1600F IHR SQ 976F OQ 575 2+21IR	Billet	6.50	R.T.	12	242.0	2.500	1.000	CT	:	0.14	56.40	68.6	2.2	1972	84278	
		5.60			242.0	2.500	1.000	CT	:	0.15	68.50			1972	84278	1

NOTES: (1) COLD ROLLED 60% WITH INTERMEDIATE ANNEALS AT 1276F TO GET FINE GRAIN SIZE

TABLE 3.17.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL 4140 AT ROOM TEMPERATURE

Product					K_{lc}	$K_{Ic}~(ksi\sqrt{in})$	<u>1</u>			
Form	Condition/Heat Treatment			S	Specimen Orientation	n Orier	ıtation			
			L-T			T-T			S-L	
		Mean K _I	Std Dev	ď	Mean K _{lo}	Std Dev	u	Mean K _{le}	Std Dev	£
Plate	1600F 1HR 1550F 1HR OQ AT 150-175F 900F 1HR			:	72	18.8	2	:	:	;
	2010F 1 HR OQ 475F 1HR	52.1	7.4	2		i	:	:	ŀ	;
Forged Bar	2190F 1 HR OQ 400F 1HR	81.1	13.2	2	•••	i	i	ŀ	:	:
	2190F 1 HR OQ 475F 1HR	66.1	2.7	2	***	ŀ	:	:	;	j

					ALI	ALLOY STEEL		4140 K _{lo}							
	PRODUCT	JCT				_	SPECIMEN	7	CRACK	• ¥ 0		K_{I_o}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kal)	WIDTH (fn.)	THICK (in.) B	DESIGN	LENGTH (in.) A	(K_TYS)* (in.)	K. (Kei • /in.)	K. MEAN	BTAN	DATE	REFER
1600F 1 HR OQ 400F 1HR	Forged Bar	0.62	R.T.	LT	210.0	2.000	0.600	CT	1.000	0.09	39.90	i	;	1973	87241 (1)
1600F 1 HR OQ 635F 1HR	Forged Bar	0.62	R.T.	L-T	230.0	2.000	0.600	СТ	1.000	0.12	50.00	i	1	1973	87241 (1)
1600F 1 HR OQ 745F 1HR	Forged Bar	0.62	R.T.	L-T	220.0	2.000	0.600	CT	1.000	0.13	50.60	i	ï	1973	87241 (1)
1600F 1HR 1650F 1HR OG	Ĕ	1.00	ţ	Ė	198.1	2.001	0.994	CT	1.034	0.10	41.30			1980	MR002
AT 150-175F 800F 1HR	Fiate	1.00	ę	Tel	198.1	2.003	0.994	CT	1.065	60.0	38.90	40.1	1.7	1980	MR002
1600F 1HR 1550F 1HR OQ AT 150-176F 800F 1HR	Plate	1.00	R.T.	T-L	175.0	2.003	0.994	CT	1.040	0.28	58.70	ı	i	1980	MR002
1600F 1HR 1650F 1HR OQ	E	1.00		E	167.7	2.002	0.994	CT	1.045	0.44	71.10			1980	MR002
AT 150-175F 800F 1HR	Flate	1.00	166	7.7	167.7	2.000	066'0	CT	1.037	0.38	66.19	68.6	3.5	1980	MR002
1600F 1HR 1650F 1HR OQ		1.00	į	į	176.3	2.003	0.994	СТ	1.033	0.31	62.50			1980	MR002
AT 150-175F 900F 1HR	Flate	1.00	69-	Т·Г	176.3	2.002	0.994	CT	1.022	0.44	74.69	9.89	8.6	1980	MR002
1600F 1HR 1550F 1HR OQ AT 150-175F 900F 1HR	Plate	1.00	R.T.	T-L	159.4	2.003	96.0	CT	1.024	0.71	95.30	***	ı	1980	MR002
1600F 1HR 1550F 1HR OQ	E C	1.00	200	Ē	156.0	2.000	066'0	CT	0.991	0.73	84.40			1980	MR002
AT 150-175F 900F 1HR	Linte	1.00	8	1	156.0	1.998	0.994	CI	1.015	0.73	84.60	84.5	0.1	1980	MR002
2010F 1 HR OQ 400F 1HR	Forged Bar	0.62	R.T.	LT	200.0	2.000	0.600	CT	1.000	0.22	59.20	:	:	1973	87241 (1)
111 112 CO 111 1 110 CO	í	0.62	£	E	210.0	2.000	0.600	CT	1.000	0.12	46.80			1973	87241 (1)
Z010F 1 HK OQ 476F 1HK	rorged Bar	0.62	K.T.	7	210.0	2.000	0.600	CT	1.000	0.19	67.30	62.1	7.4	1973	87241 (1)
ant agos og an i agose	9 0	0.62	E	E	200.0	2.000	0.600	CT	1.000	0.51	90.40			1973	87241 (1)
ZISOF I DA ON TOOF IDA	rorged Dar	0.62	T.T.	5	200.0	2.000	0.600	CT	1.000	0.32	71.70	81.1	13.2	1973	87241 (1)
this trans contract	f	0.62	E	E	210.0	2.000	0.600	CT	1.000	0.26	68.00			1973	87241 (1)
And 1014 Vog 1/10 into	rorged Dar	0.62	Pri:	3	210.0	2.000	0.600	CT	1.000	0.23	64.20	66.1	2.7	1973	87241 (1)
2190F 1 HR OQ 615F 1HR	Forged Bar	0.62	R.T.	LT	206.0	2.000	0.600	CT	1.000	0.14	48.50	i		1973	87241 (1)
2190F 1 HR OQ 660F 1HR	Forged Bar	0.62	R.T.	LT	202.0	2.000	0.600	СT	1.000	0.17	63.20		-	1973	87241 (1)

NOTES: (1) COMPOSITION (WT PERCENT) 0.40C, 0.94Mn, 0.008P, 0.012S, 0.28SI, 0.09NI, 0.90Cr, 0.17Cu

TABLE 3.17.3.3

K_{Isce} SUMMARY FOR ALLOY STEEL 4140

Condition/ D	Desa	Test	ğ	Yield		S	Specimen		Prod		;	•	Test		
	Form	Temp Or. (K	or.	Str (Ksi)	Envir.	Design	Width Thick (in)	Thick (in)	Thk (in)	Crack (in)	(in) (Keivin) (Keivin)	K _{less} (Ksivin)	Time (min)	Test Date	Reference
	Ъ	R.T.	i	105	Water Sat H ₂ S	CT	8.25		į	-	:	36	ł	1972	84963
	ď	R.T.	I	147.5	Water Sat H ₂ S	CT	3.25	-	ŀ	. 🗖	l	17.5	I	1972	84963
	P	R.T.	-	195	Dist. Water	CANT	-	0.25	0.25	6.0	49.4	15	:	1965	63061
	ъ	R.T.	i	241	Dist. Water	CANT.	1	0.25	0.25	0.2	40.1	11	i	1965	63061

asterisk in specimen design column indicates that specimens are side-grooved

TABLE 3.18.3.3

K_{Isce} SUMMARY FOR ALLOY STEEL 4330V

Reference 84351 Test Date 1971 Test Time (min) į K_{los} (Ksivin) 25 K_q (Ksi√in) 103 Crack (in) 0.3 Prod Thk (in) 0.48 Thick (in) 0.48 Specimen Width (in) 1.5 Design NB 3.5% NaCl Envir. Yield Str (Ksi) 196 Spec Or. Ľs Test Temp (°F) R.T. Prod Form Д Quenched + Tempered at 500°F Condition/ Heat Treat

1 of 1

TABLE 3.19.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL 4330V MOD AT ROOM TEMPERATURE

Product					$K_{I\sigma}$	$K_{Ic}~(ksi\!\sqrt{in})$	િ			
Form	Condition/Heat Treatment			<i>S</i> 2	Specimen Orientation	n Orier	itation			
			LT			T·T			S-L	
		Mean K _{ie}	Std Dev	4	Mean K _{te}	Std Dev	u	Mean K _i	Std Dev	ч
Plate	HEAT TREATED TO 46 RC HARDNESS	;	:	ı	74.7	8.0	2	1	:	:
Forged Bar	1600F 1HR OQ 535F 1HR	96.7	3.8	2	:	:	1	:	:	i
Billet	1650F 1HR AC 1575F 1HR OQ 800F 2+2HR	86.4	9.7	6	:	i	:	:	:	:

TABLE 3.19.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 4330V (MOD) AT ROOM TEMPERATURE

ORIENTATION: L-T

ENVIRONMENT: Lab Air

9 0000000000000000000000000000000000000	
ę.	
100.0	
50.0 27.92	
<u> 7</u> 2	(e
AK Level (Kst/in) 10.0 20.0 1.8 7.29	PCGR (10 ⁻⁴ in/cycle)
3	Ô
Ksh, 20.0	'n
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- e	0
1.98	(I)
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y.	G
4	2
3.0 10.0 20.0 50.0 17.92 27.92	4
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HEAT TREATMENT UNSPECIFIED	
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					ALLOY STEEL	STEEL	4330V	4330V MOD	K _{Io}						
	PRODUCT	JCT					SPECIMEN		CRACK			K,			
CONDITION	FORM	THICK (In.)	TEST TEMP (°F)	SPEC	YTELD STR (Kel)	WIDTH (In.)	THICK (in.) B	DRBIGN	LENGTH (in.) A	(K _w TYS)* (In.)	R. (Red •	E. MEAN	BTAN DRV	DATE	REFER
	į	2.20	;		194.5	2.502	1.259	СТ	1.166	0.14	45.30			1974	MA011
	Dillet	2.20	\$	14	194.5	2.507	1.260	СТ	1.163	0.13	44.30	44.8	0.7	1974	MA011
	Billet	2.20	R.T.	LT	194.5	2.504	1.253	СT	1.164	0.43	80.70	i	1	1974	MA011
1600F 1 HR OQ 400F 1 HR	Forged Bar	0.62	R.T.	LT	198.0	2.000	0.600	CT	1.000	0.49	88.00	į	ł	1973	87241 (1)
THE CHAPT OF THE PROPERTY OF T	e e	0.62	į		202.0	2.000	0.600	cr	1.000	0.60	99.40			1973	87241 (1)
1900F I HK OQ BOOF I HK	rorged Bar	0.62	K.T.	1	202.0	2.000	0.600	CT	1.000	0.54	94.00	96.7	8.8	1973	87241 (1)
		6.00			203.0	2.500	1.000	CT	1.400	0.34	77.50			1972	84277
		6.00			203.0	2.500	1.000	СT	1.400	0.48	84.20			1972	84277
1650F 1 HR AC 1576F 1	i i	6.00	Ē		203.0	2.500	1.000	CT	1.400	0.38	81.60			1972	84277
525F 2+2 HR		6.00	; 4	3	203.0	2.500	1.000	cr	1.400	0.45	81.20	81.6	2.3	1972	84277
	••••	9:00			203.0	2.500	1.000	C.	1.400	0.46	82.20			1972	84277
		6.00			203.0	2.500	1.000	ст	1.400	0.39	82.80			1972	84277
1 GEOR 1 UD AC 1675B1		6.00			191.0	2.500	1.000	CT	1.400	0.68	99.70			1972	11218
HR OQ	Billet	6.00	R.T.	7	191.0	2.500	1.000	CT	1.400	0.60	93.80	96.1	9.2	1972	84277
200 675 111		6.00			191.0	2.500	1.000	СŢ	1.400	0.61	94.70			1972	84277
HEAT TREATED TO 46 RC	Ē	0.62	Ę	Ē	193.0	1.602	0.750	NB	0.762	0.38	75.20			1971	84029
HARDNESS	FINE	0.62	R. I.	7-1	193.0	1.498	0.750	NB	0.758	0.37	74.10	74.6	9.0	161	84029

NOTES: (1) COMPOSITION (WT PERCENT) 0.28C, 1.02Mn, 0.0069, 0.0068, 0.2881, 1.80NI, 0.85Cr, 0.07V, 0.01Cu

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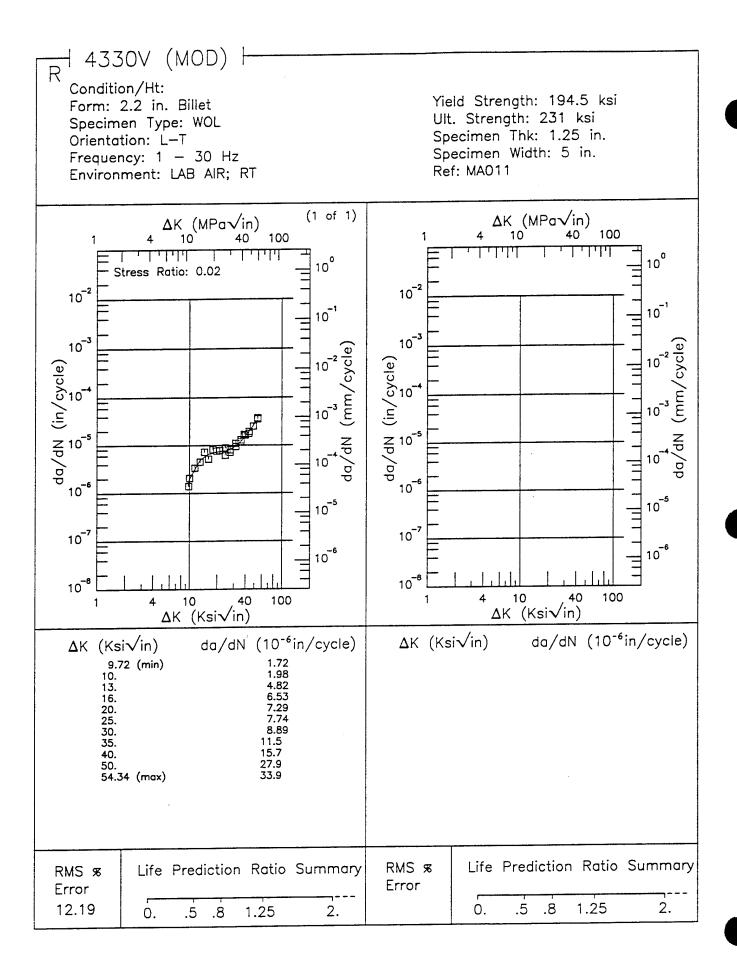


Figure 3.19.3.1

TABLE 3.20.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL 4340 AT ROOM TEMPERATURE

Product Condition/Hes Form 1550F OQ TEN 1560F OQ TEN 1600F 1HR 1525F 2.5HH 1600F 1HR 1625F 2.5HH 1600F 1HR O 1600F 1HR FC TO 1600F 1600F 1HR PC TO 1600F	Heat Treatment				K_{Ic}	$K_{Ic}~(ksi\sqrt{in})$	<u>ા</u>			
	<u> </u>			\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	pecime	Specimen Orientation	itation			
	L		L-T			T-T			S-L	
		Mean K _{lo}	Std Dev	E	Mean K _{le}	Std Dev	E	Mean K ₁₀	Std Dev	ď
	1550F OQ TEMPERED 500F	45.3	2.9	4	÷	i	:	i	;	:
	1550F OQ TEMPERED 800F	76.6	4.6	2	:	:	:	;	:	ŀ
	1600F 1HR 1525F 2.5HR OQ AT 150-175F 900F 1HR	1		i	88.2	1.5	2	i	i	i
	HEAT TREATED TO 51 RC HARDNESS	:			51.7	1.3	2	:	:	:
<u> </u>	IR 0Q 535F 1HR	6.09	9.0	2	••	÷	ŀ	i	ı	i
	2190F 1HR FC TO 1600F HOLD 0.5HR 400F 1HR	76.8	0.1	2	•		:	:		:
ZIBUE IMK FC 10 ISOUE	2190F 1HR FC TO 1600F HOLD 0.5HR 535F 1HR	60.1	3.2	2		:	;	:		:
2190F 1HR FC TO 1600F	2190F 1HR FC TO 1600F HOLD 0.5HR 660F 1HR	8.09	0.8	2		:	:	:	•••	i
Billet 1650F 1HR AC 1525F	1650F 1HR AC 1525F 1HR OQ 800F 2HR	76.3	3.6	9	•••		i	·	:	:

TABLE 3.20.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 4340 AT ROOM TEMPERATURE

ORIENTATION: L-T	i: L-T	ENA	ENVIRONMENT: Distilled Water	: Distilled	d Water	£.	
CONDITION/	PRODITET	FREG	I	FCGR (10 ⁴ in/cycle)	⁸ in/cyc.	la)	
HEAT TREATMENT	FORM	R (Hz)	AA 8.9	AK Level (Kst/in)	(Ksk/ir	0.07	l g
MARTEMPERED	PLATE	0.02		0.48	3.43	24.63	154.57

TABLE 3.20.1.2.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 4340 AT ROOM TEMPERATURE

ORIENTATION: L-T

ENVIRONMENT: H.H.A.

				2		
				100.0		
				60.0	17.78	
~				¥	17	
FCGR (10 ⁴ in/cycle)		ΔK Level (Ksivln)	``			
6		3		20.0	4	ø
3		× 2		8	2.94	3.78
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2		9		10.0		_
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124				6.0		
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		(Hz)			က	3
	25	=				
		¥			0.05	9.0
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		2		∭		<u> </u>
	EON	TRE			į)8[=8[.
	HONO	TTRE			i I	U18=180-200KSI
	CONDI	SAT TRE				0.15=180
	CONDI	HEAT TRE			ž i	0.15=180
	CONDI	HEAT TREATMENT			2000	0.12=180

TABLE 3.20.1.2.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK 4340 AT ROOM TEMPERATURE

ORIENTATION: L-T	: L-T		Œ	ENVIRONMENT: Lab Air	NMEN	T: Lab	Air		
CONDITION	PRODUCT		Odla		PC	FCGR (10 ^d in/cycle)	⁸ in/cyc	(9)	
HEAT TREATMENT	FORM	R	(HZ)		VI	AK Level (Ksivin)	(Ksivin	1)	
				2.5	6,6	10.0	20.0	60.0	100.0
MARTEMPERED	PLATE	2 0'0				0.52	3.06	22.96	115.4
TWG_IEAVOI	FORGING	0.1	30		0.02	0.28	2.44		
015=100031	UNSPECIFIED	-0.1	2-5			0.44			
		0.1	7				2.47		
UTS=160KSI	ROUND BAR	0.5	L		60:0				
		0.5	7			0.61	3.6		
		0.1	20				2.69	30.66	
UTS=160-180KSI	BAR	0.5	20		0.09	0.64	3.9	34.11	
		0.8	20			0.68	4.16		
	CMICGOS	0.1	20-30		0.02	0.35	2.52		
	FONGING	0.5	30		90.0	0.58	3.4		
1970-1971		0.1	20				2.89	23.41	
101101-01	n va Charlon	0.1	30			0.42			
	MOOND BAR	0.5	7			0.65			
		0.5	7		0.09				

TABLE 3.20.1.2.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK

100.0 80.0 20.75 PCGR (10 8 in/cycle) ΔK Lovel (Ksivin) 90.06 3.16 2.93 **ENVIRONMENT: Argon** 10.0 0.0 4340 AT ROOM TEMPERATURE 10) (3) FREQ (Hz) 0.4 9.4 × PRODUCT UNSPECIFIED UNSPECIFIED FORM **ORIENTATION: Unspecified** HEAT TREATMENT CONDITION/ 450F TEMPER 750F TEMPER

TABLE 3.20.1.2.5

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK 4340 AT ROOM TEMPERATURE

ORIENTATION: Unspecified	specified		ENVIRON	ENVIRONMENT: Distilled Water	stilled W	/ater		
CONTRIBUTION	HEATTAN	į	Ş	FCG	FCGR (10 ⁴ in/cycle)	/cyale	6	
HEAT TREATMENT	FORM	R EE (H	FKEQ (Hz)	ΔK	ΔK Løvel (Ksiγin)	sh(in)		
			2.5	6.0	10.0	20.0	50.0	100.0
450F TEMPER	UNSPECIFIED)	0.4		274	274.31	443.28	
		0	0.04		451	451.68		
750F TEMPER	UNSPECIFIED	5	0.2		106	105.97	171.95	
)	0.4		39	65.04	143.63	

TABLE 3.20.1.2.6

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 4340 AT ROOM TEMPERATURE

T: H.H.A.	FCGR (10 ⁻⁸ in/cycle) AK Level (Ksi/in) 10.0 20.0 80.0 100.0	2.68	46.14
ENVIRONMENT: H.H.A.	FREQ (HZ) AK	10	10
	В	0.	0.5
specified	PRODUCT FORM	24 A	FLAIE
ORIENTATION: Unspe	CONDITION/ HEAT TREATMENT	1971AAA OOL SIIITI	U 15=160-200A51

					ALL	ALLOY STEEL		4340 K ₁₀							
	PRODUCT	UCT					SPECIMEN	7	CRACK			K _{Io}			
CONDITION	FORM	THICK (ln.)	TEST TEMP (F)	SPEC	YIELD STR (Kal)	WIDTH (in.)	THICK (In.)	DESIGN	LENGTH (in.) A	#.6 (K.,,TYB)* (in.)	K. (Ked •	K. MBAN	STAN	DATE	REFER
		1.00			238.0	0.160	0.800	CT	0.800	1	48.00			1971	86582
awa dadadwat oo dossi	Ē	1.00	£		238.0	0.160	0.800	ст	0.800		45.80			1971	86582
1000 Ce temperation	91813	1.00	R. I.	<u>.</u>	238.0	0.160	0.800	CT	0.800	1	46.00	45.3	2.9	1971	86582
		1.00			238.0	0.160	0.800	LO	0.800	60.0	41.20			1971	86582
TOO TO TO TO		1.00	í		206.0	0.160	008'0	L	0.800	1	79.80			1971	86582
1000F OF LEMPERED BOOF	Flate	1.00	K.T.	LT	206.0	0.160	0.800	CT	0.800	0.37	73.30	76.6	4.6	1971	86582
1600F 1 HR OQ 400F 1 HR	Forged Bar	0.62	R.T.	LT	195.0	2.000	0.600	CT	1.000	0.23	59.50	i	j	1973	87241 (1)
un tassa con amer	9	0.62	Ē		218.0	2.000	0.600	cr	1.000	0.19	61.40			1973	87241 (1)
1000 TO WILL TOO	rorged Dar	0.62	R. I.	1.7	218.0	2.000	0.600	CT	1.000	0.19	06.03	6.09	9.9	1973	87241 (1)
1600F 1 HR OQ 660F 1 HR	Forged Bar	0.62	R.T.	LT	217.0	2.000	0.600	ст	1.000	16.0	79.80	-	i	1973	87241 (1)
1600F 1 HR OQ 745F 1 HR	Forged Bar	0.62	R.T.	L-T	210.0	2.000	0.600	ст	1.000	0.47	91.20		i	1973	87241 (1)
1600F 1HR 1525F 2.5 HR	Ē	1.00	ţ		190.3	1.998	1.004	CT	1.022	79'0	89.19			1980	MR002
OQ AT 150-175F 900F 1 HR	F1816	1.00	Ģ	7: -	190.3	1.997	1.004	CT	1.026	29'0	91.00	90.1	1.3	1980	MR002
1600F 1HR 1525F 2.5 HR	Ē	1.00	Ē	į	179.4	2.000	1.030	CT	1.022	19'0	89.30			1980	MR002
OQ AT 150-175F 900F 1 HR	L. THEFE	1.00	n.i.	3	179.4	1.997	1.005	cr	1.027	69'0	87.19	88.2	1.6	1980	MR002
1600F 1HR 1525F 2.5 HR	Ē	1.00	į	Ė	171.1	1.999	0.994	CT	1.029	0.74	93.60			1980	MR002
OQ AT 150-175F 900F 1 HR	Figure	1.00	160	7:I	171.1	2.010	1.030	cr	066'0	99'0	80.50	87.1	9.3	1980	MR002

NOTES: (1) COMPOSITION (WT PERCENT) 0.40C, 0.80Mn, 0.010S. 0.24SI, 1.55NI, 0.72Cr, 0.24Mo, 0.19Cu

TABLE 3.20.2.1 (CONCLUDED)

					ALL	ALLOY STEEL		4340 K _{lo}							
	PRODUCT	ucr					SPECIMEN	z	CRACK			K _I °			
CONDITION	FORM	THICK (In.)	TEST TEMP (F)	SPEC	YIELD STR (Kal)	WIDTH (in.)	THICK (In.)	DESIGN	LENGTH (In.) A	(K _e ,TY8) ² (in.)	К. (Kel • √П.)	K. MEAN	STAN DEV	DATE	REFER
		10.00			197.0	2.500	1.000	СТ	1.400	0.37	75.80			1972	84277
		10.00			197.0	2.500	1.000	cr	1.400	0.38	76.50			1972	84277
1650F 1 HR AC	i	10.00	 S		197.0	2.500	1.000	СŢ	1.400	0.41	79.70			1972	84277
1525F 1 HR OQ 800F 2 HR		10.00		3	211.0	2.500	1.000	CT	1.400	06'0	73.00	76.3	3.6	1972	84277
		10.00			211.0	2.500	1.000	cT	1.400	0.37	81.10			1972	84277
		10.00			211.0	2.500	1.000	СТ	1.400	0.29	71.90			1972	84277
2190F 1HR FC TO 1600F	9	0.62	Ę	E	195.0	2.000	0.600	CT	1.000	0.39	76.70			1973	87241 (1)
HOLD 0.5HR 400F 1HR	rotged Dar	0.62		1.5	195.0	2.000	0.600	CT	1.000	0.39	76.90	76.8	0.1	1973	87241 (1)
2190F 1HR FC TO 1600F	1	0.62	E		202.0	2.000	0.600	CT	1.000	0.20	67.80			1973	87241 (1)
HOLD 0.5HR 535F HIR	rorged Dar	0.62	F. J.	151	202.0	2.000	0.600	CT	1.000	0.24	62.30	60.1	3.2	1973	87241 (1)
2190F 1HR PC TO 1600F		0.62	Ē		200.0	2.000	0.600	CŢ	1.000	0.24	61.40			1973	87241 (1)
HOLD 0.5HR 660F 1HR	rorged Dar	0.62	F. I.	3	200.0	2.000	0.600	CT	1.000	0.23	60.20	8.09	9.0	1973	87241 (1)
2190F 1HR OQ 476F 1HR	Forged Bar	0.62	R.T.	1.7	200.0	2.000	0.600	СT	1.000	0.42	82.40	i	ı	1973	87241 (1)
2190F HIR OQ 536F HIR	Forged Bar	0.62	R.T.	1.1	202.0	2.000	0.600	cī	1.000	0.24	62.80	1	ı	1973	(1) 18241
HEAT TREATED TO	Ē	0.62	ē	Ē	220.0	0.999	0.499	NB	0.540	0.14	62.60			1871	84029
61 RC HARDNESS	riate	0.62	i.i.	<u>.</u>	220.0	0.998	0.498	NB	0.534	0.13	60.80	61.7	1.3	1971	84029
UTS = 180 KSI	Round Bar	4.50	R.T.	1.1	192.9	2.007	0.992	CT	0.933	0.77	107.20		ı	1979	DA001

NOTES: (1) COMPOSITION (WT PERCENT) 0.40C, 0.80Mn, 0.010S. 0.24SI, 1.65NI, 0.72Cr, 0.24Mo, 0.19Cu

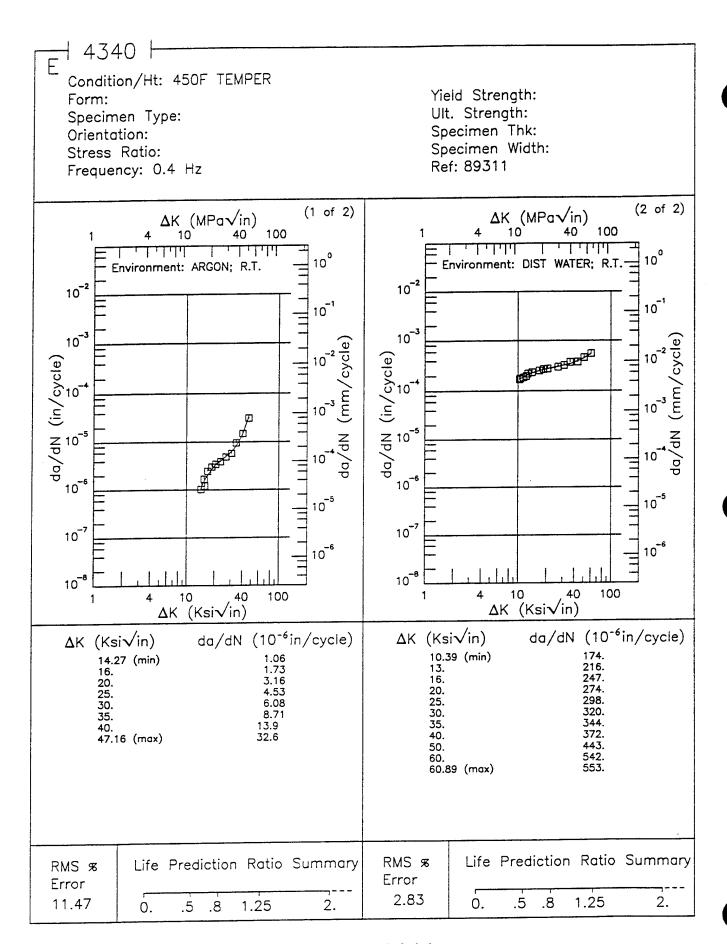


Figure 3.20.3.1.1

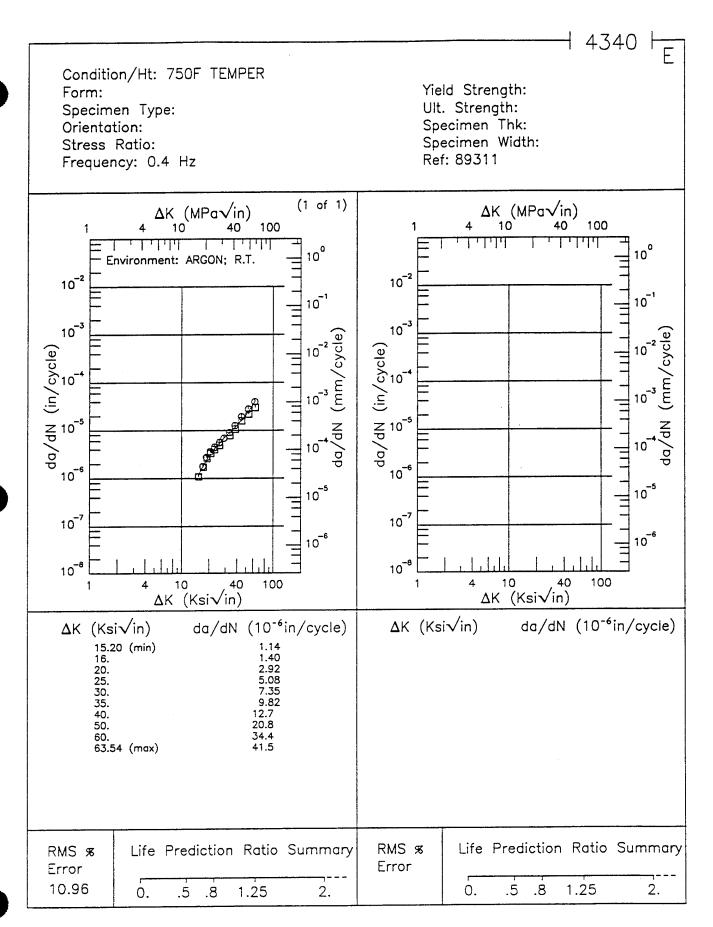


Figure 3.20.3.1.2

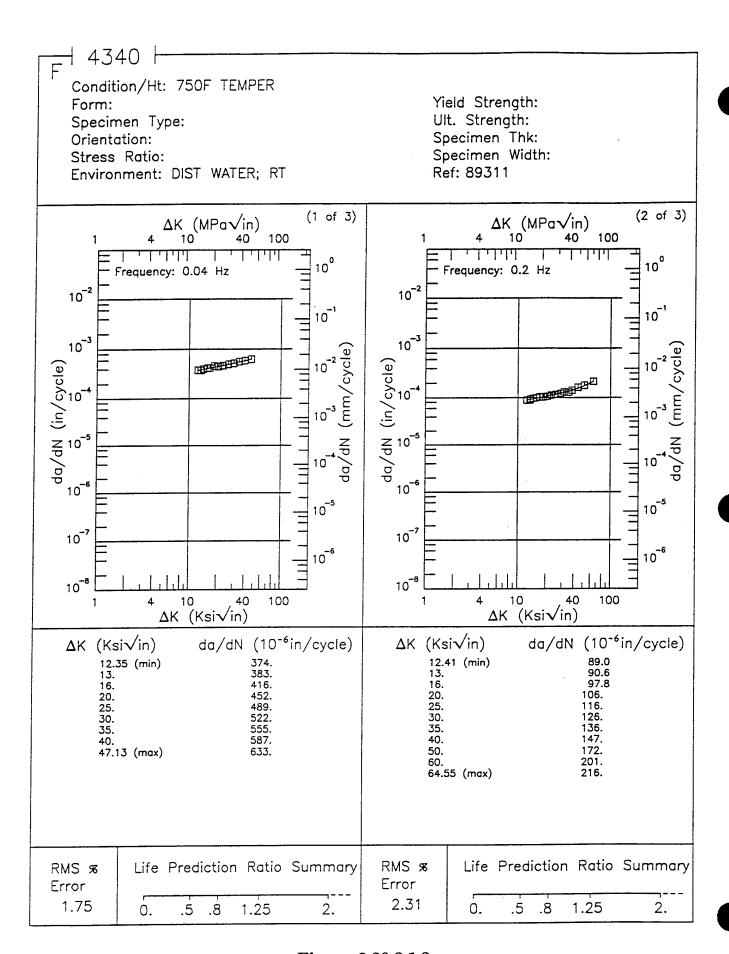


Figure 3.20.3.1.3

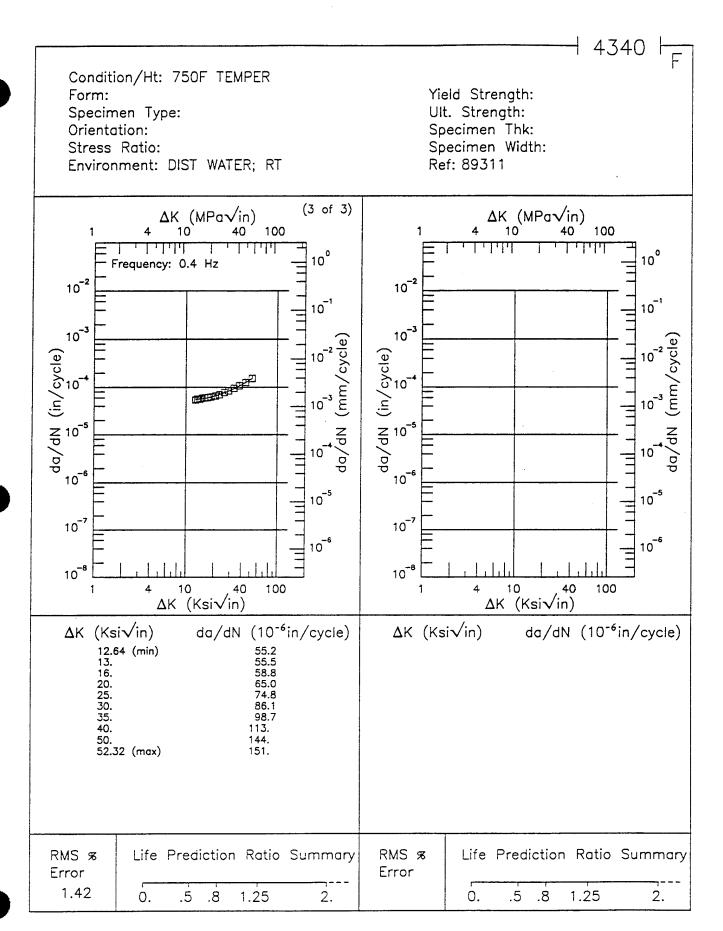


Figure 3.20.3.1.3 (Concluded)

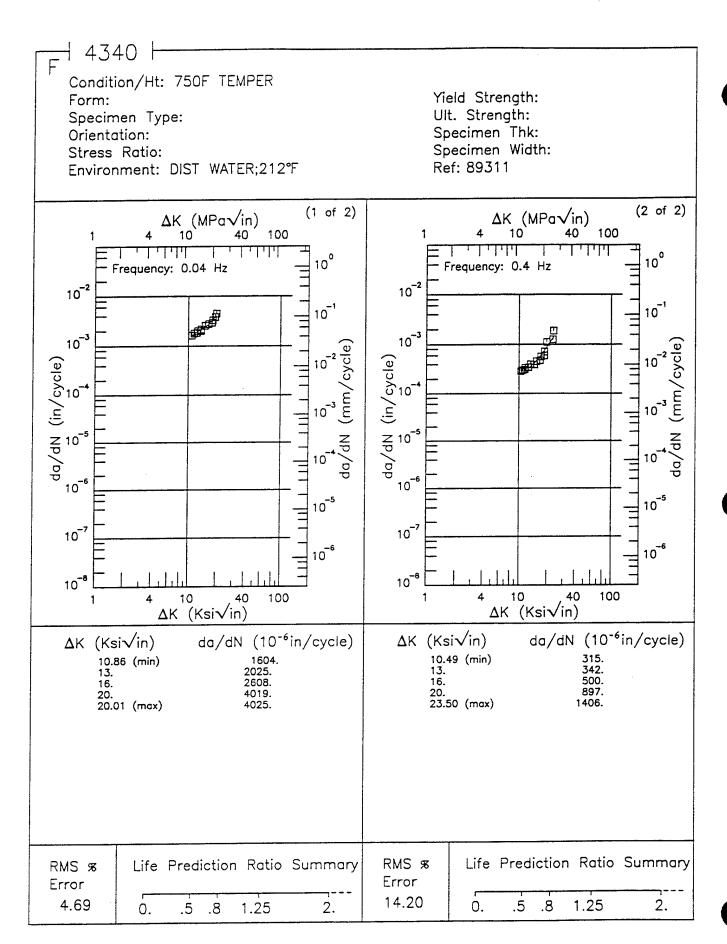


Figure 3.30.3.1.4

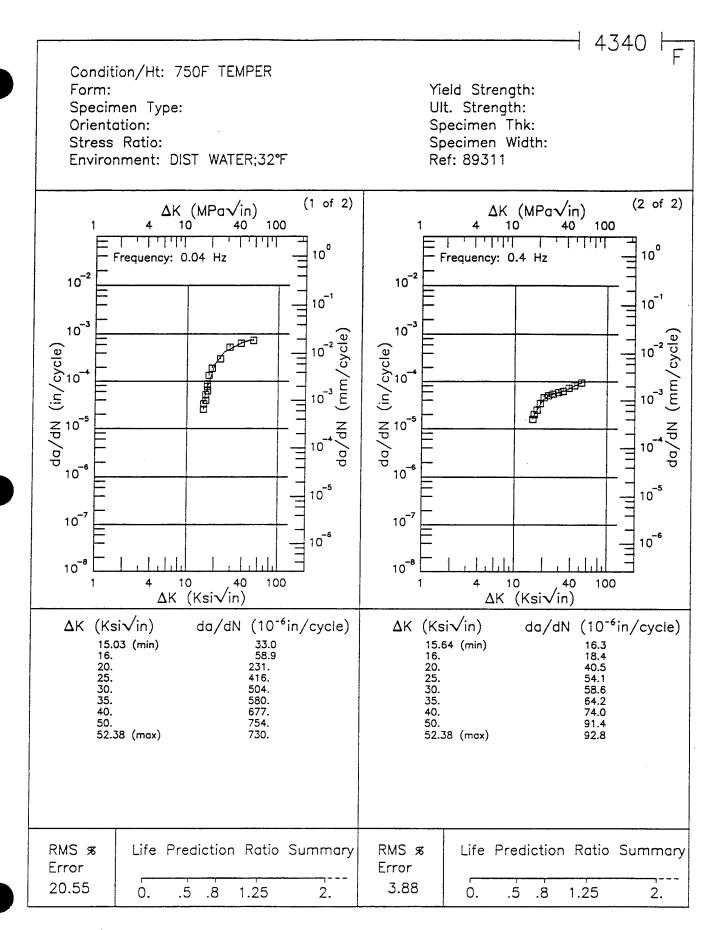


Figure 3.20.3.1.5

4340 Condition/Ht: MARTEMPERED Yield Strength: 191 - 201.5 ksi Form: 0.5 in. Plate Ult. Strength: 196 - 209 ksi Specimen Type: CCP (max stress specified) Specimen Thk: 0.246 - 0.251 in. Orientation: L-T Specimen Width: Stress Ratio: 0.02 Ref: MA012 Frequency: (2 of 2) (1 of 2)ΔK (MPa√in) $\Delta K (MPa\sqrt{in})$ 100 10 40 10 40 100 <u>, 1,1,1,1,1</u> 11111 11111 10° Environment: DIST WATER; R.T. Environment: LAB AIR; R.T. 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10-6 10⁻⁵ 10 -5 **A**E 10⁻⁷ 10-7 10-6 10-6 10 8 100 10 40 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) Δ K (Ksi \sqrt{in}) Δ K (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) 8.73 (min) 7.13 (min) 0.329 9. 8. 10. 9. 13. 10. 16. 13. 20. 16. 20. 25. 30. 40. 50. 60. 80. 60. 66.7 100. 160. 130. 189.12 (max) 160. 188.45 (max) Life Prediction Ratio Summary RMS &

Figure 3.20.3.1.6

2.

Error

23.03

.5

.8

0.

1.25

2.

Life Prediction Ratio Summary

1.25

RMS %

Error

23.49

0.

.5 .8

Condition/Ht: UTS=150KSI Yield Strength: 150 ksi Form: Specimen Type: CCP (max load specified) Ult. Strength: Specimen Thk: 0.25 in. Orientation: L-T Specimen Width: 3.9 in. Frequency: 2 - 5 Hz Ref: WL005 Environment: LAB AIR; RT (1 of 1)ΔK (MPa√in) Δ K (MPa \sqrt{in}) 10 100 100 10 40 11111 10° 10° Stress Ratio: -0.1 10-2 10-2 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10⁻⁶ 10 -5 10⁻⁵ 10⁻⁷ 10⁻⁷ 10 6 10⁻⁶ 10 -8 10-8 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) da/dN (10⁻⁶in/cycle) ΔK (Ksi \sqrt{in}) ΔK (Ksi√in) 5.69 (min) 6. 7. 8. 0.0450 9. 10. 13. 15.54 (max) RMS & Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % Error Error 54.59 .5 .8 1.25 .5 0. 2. .8 1.25 0. 2.

H 4340 H

4340 Condition/Ht: UTS=150KSI Yield Strength: 150 ksi Form: Forging Ult. Strength: Specimen Type: CT Specimen Thk: 0.25 - 0.251 in. Orientation: L-T Specimen Width: 2 - 2.003 in. Frequency: 30 Hz Ref: SW001 Environment: LAB AIR; RT (1 of 1) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 10 40 100 100 10 40 10° Stress Ratio: 0.1 10-2 10⁻² 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10-6 10 -5 10 -5 10⁻⁷ 10⁻⁷ 10⁻⁶ 10⁻⁶ 10 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) $\Delta K (Ksi\sqrt{in})$ da/dN ($10^{-6}in/cycle$) ΔK (Ksi√in) 0.0112 4.55 (min) 0.0180 5. 6. 7. 8. 9. 13. 16. 20. 21.97 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS & Error Error 31.84 2. 1.25 .5 .8 1.25 2. 0. .5 8. ٥.

Figure 3.20.3.1.8

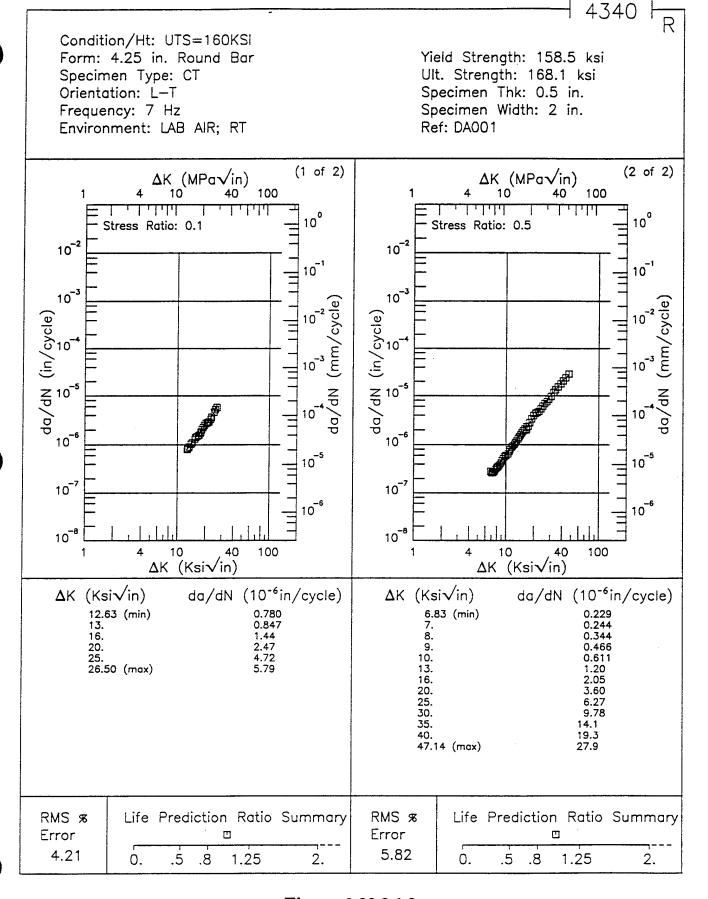


Figure 3.20.3.1.9

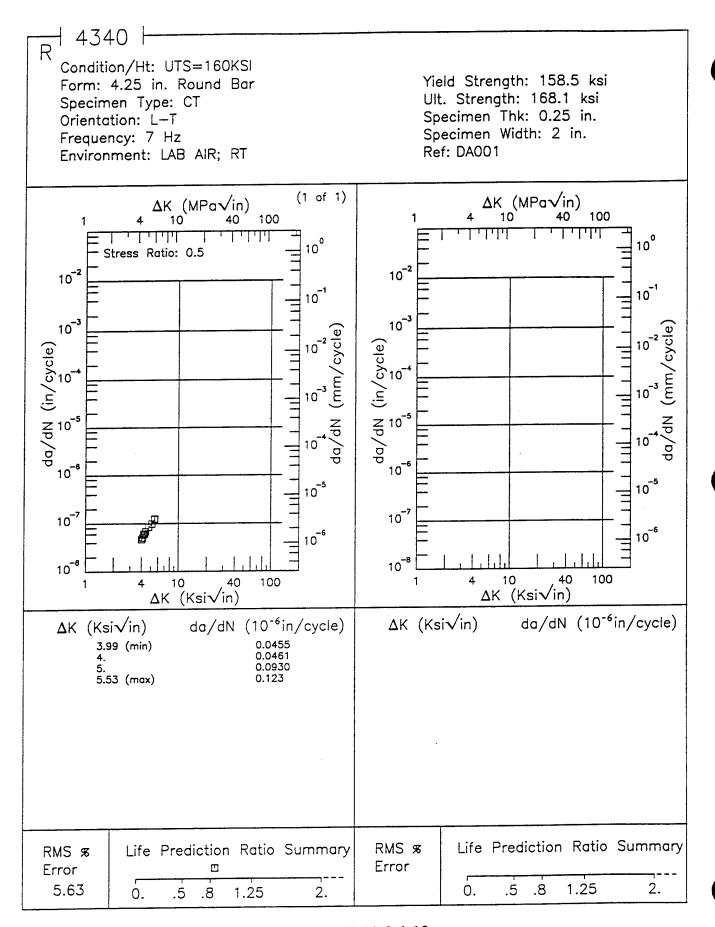


Figure 3.20.3.1.10

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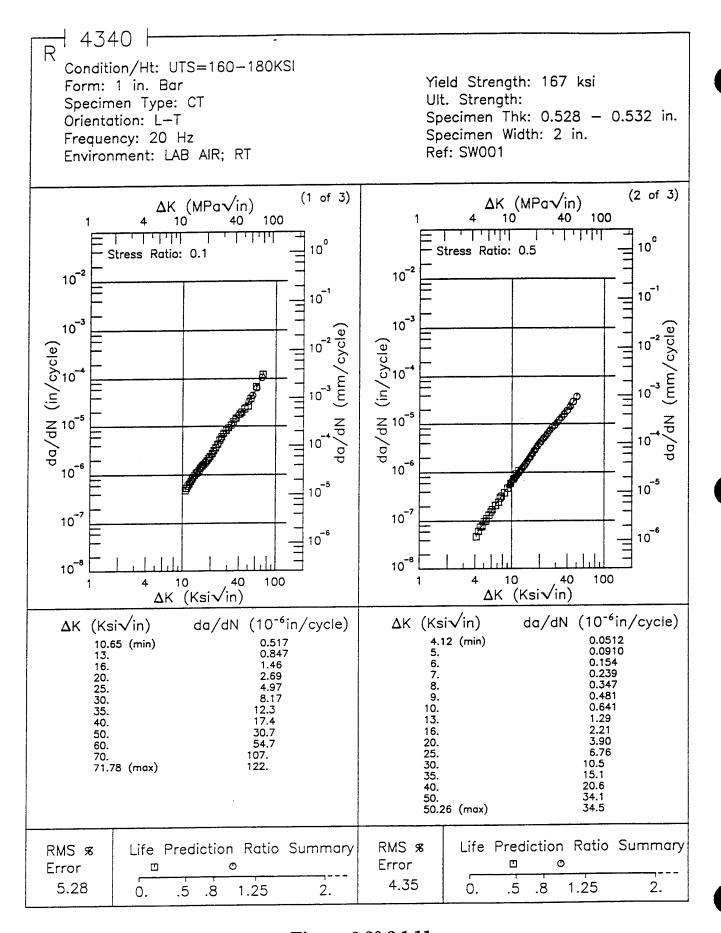


Figure 3.20.3.1.11

1 4340 H Condition/Ht: UTS=160-180KSI Yield Strength: 167 ksi Form: 1 in. Bar Specimen Type: CT Ult. Strength: Specimen Thk: 0.528 - 0.532 in. Orientation: L-T Specimen Width: 2 in. Frequency: 20 Hz Ref: SW001 Environment: LAB AIR; RT (3 of 3) Δ K (MPa \sqrt{in}) ΔK (MPa√in) 100 10 40 100 10 40 77144 Lilia 10⁰ 10° Stress Ratio: 0.8 10-2 10⁻² 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10⁻⁶ 10 -5 10⁻⁷ 10⁻⁷ 10 -6 10-6 10-8 10⁻⁸ 40 100 10 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) da/dN ($10^{-6}in/cycle$) ΔK (Ksi√in) ΔK (Ksi√in) 6.01 (min) 7. 8. 0.396 0.527 9. 13. 16. 20. 23.09 (max) 4.16 Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error 2.26 .5 .8 1.25 2. .5 1.25 2. 0. .8 0.

Figure 3.20.3.1.11 (Concluded)

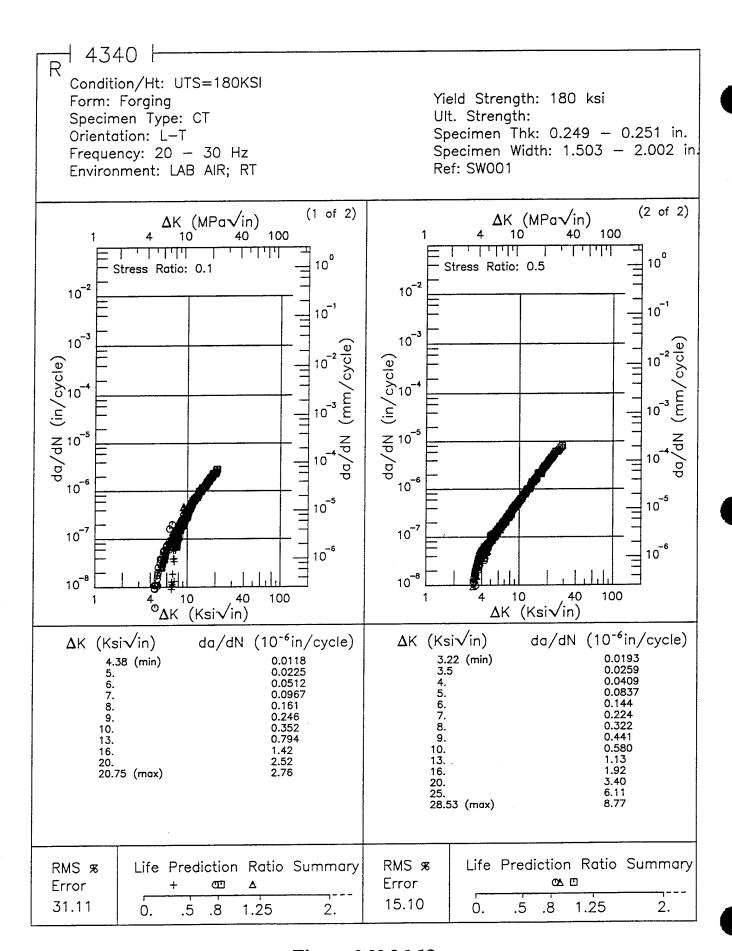


Figure 3.20.3.1.12

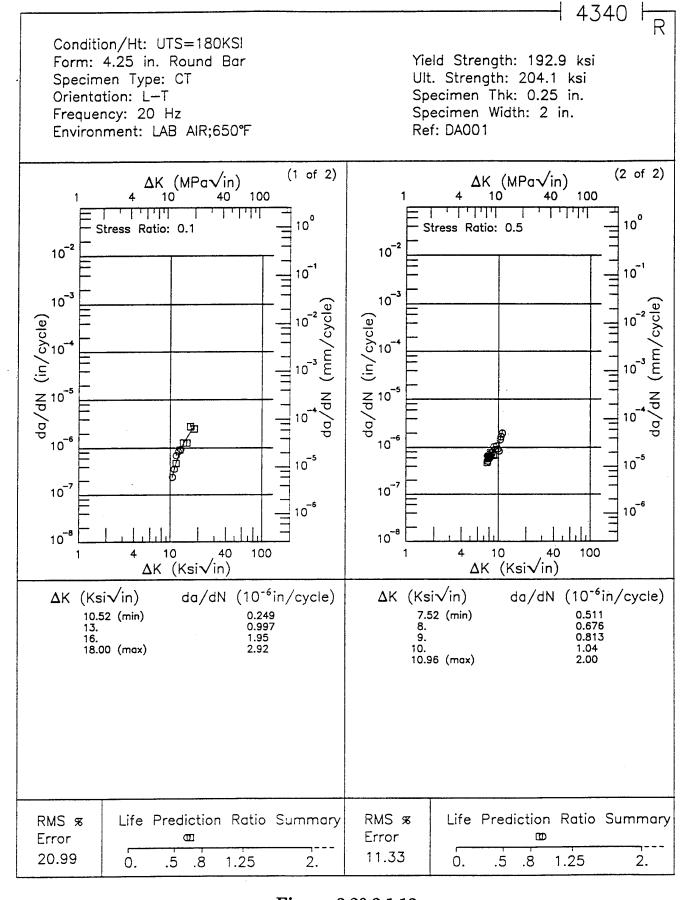


Figure 3.20.3.1.13

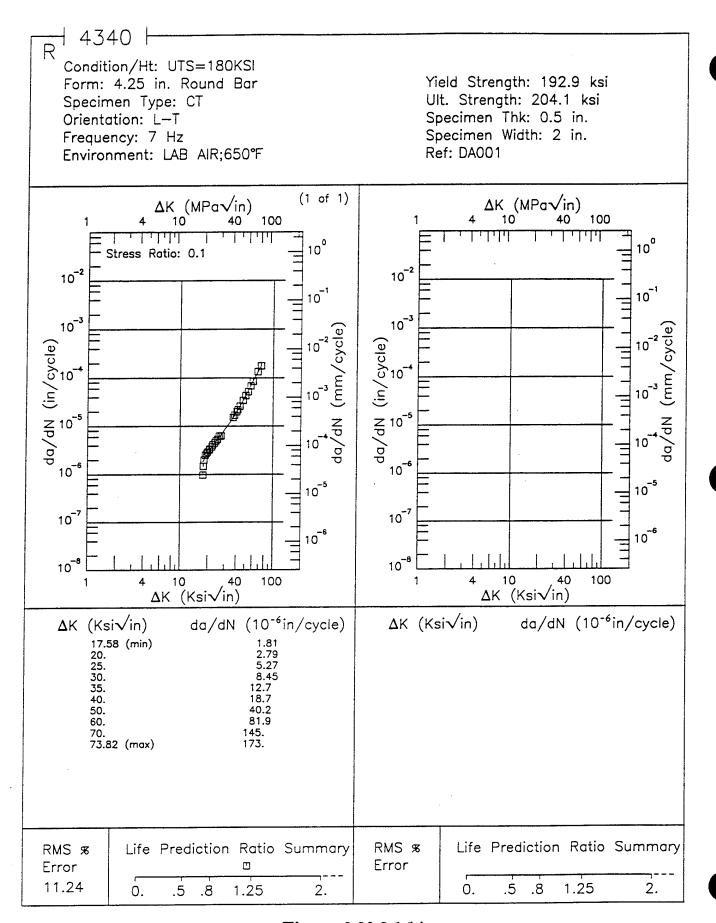
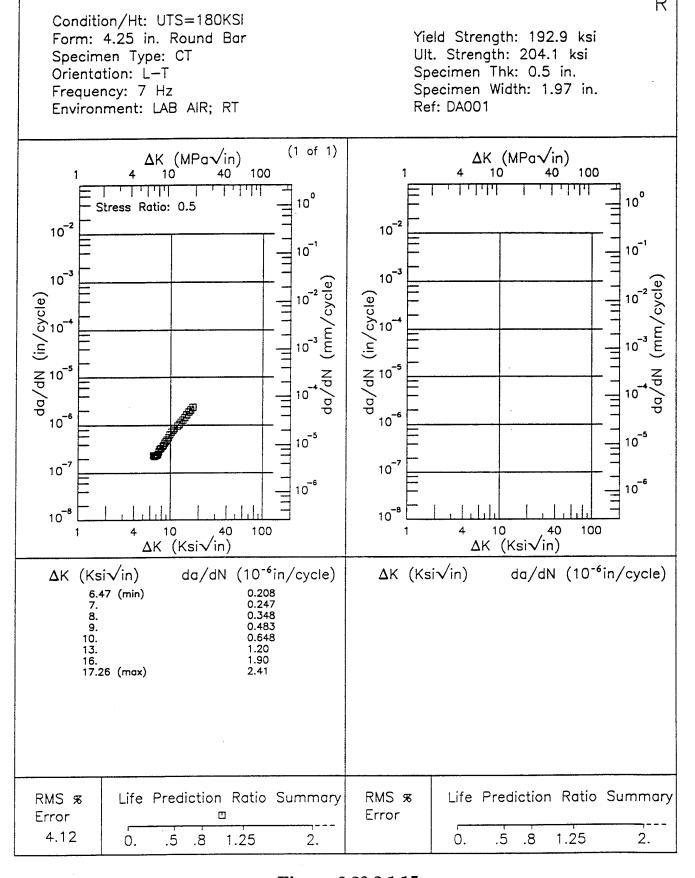


Figure 3.20.3.1.14



4340

Figure 3.20.3.1.15

Condition/Ht: UTS=180KSI Form: 4.25 in. Round Bar Yield Strength: 192.9 ksi Ult. Strength: 204.1 ksi Specimen Type: CT Specimen Thk: 0.25 - 0.375 in. Orientation: L-T Specimen Width: 1.5 - 2 in. Stress Ratio: 0.5 Ref: DA001 Frequency: 7 Hz (2 of 2) (1 of 2) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 100 10 40 10 40 100 - 1 1 1 1 1 1 111111 11111 10° 10° Environment: LAB AIR; 650°F Environment: LAB AIR; R.T. 10-2 10-2 10-1 10⁻¹ 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10 10-6 10-6 10 -5 10⁻⁵ 10⁻⁷ 10⁻⁷ 10 6 10⁻⁶ 10⁻⁸ 10 -8 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) $da/dN (10^{-6}in/cycle)$ da/dN (10⁻⁶in/cycle) ΔK (Ksi \sqrt{in}) ΔK (Ksi√in) 5.72 (min) 4.08 (min) 0.0528 6. 7. 8. 9. 0.0924 5. 0.178 0.454 6.20 (max) 0.224 13. 20. 22.85 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS & RMS % Error Error 4.72 0. .5 .8 1.25 2. 11.20 .5 .8 1.25 2. 0.

Figure 3.20.3.1.16

Condition/Ht: UTS=180KSI Yield Strength: 192.9 ksi Form: 4.25 in. Round Bar Specimen Type: CT Ult. Strength: 204.1 ksi Specimen Thk: 0.251 - 0.501 in. Orientation: L-T Stress Ratio: 0.1 Specimen Width: 1.975 - 1.978 in Ref: DA001 Environment: LAB AIR; RT (1 of 2)(2 of 2) Δ K (MPa \sqrt{in}) ΔK (MPa√in) 100 40 100 10 40 10 11111 10° 10° Frequency: 20 Hz Frequency: 30 Hz 10-2 10 2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10⁻⁶ 10 10 10⁻⁷ 10⁻⁷ 10-6 10-6 10 8 10-8 10 10 40 100 40 100 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) da/dN (10⁻⁶in/cycle) 11.85 (min) 13. 16. 5.69 (min) 6. 7. 8. 0.736 0.0156 0.969 0.0395 0.185 1.69 20. 25. 0.286 9. 0.330 10. 11.14 (max) 40. 50. 64.66 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error 47.81 11.24 . 5 0. .5 .8 1.25 2. 0. 8. 1.25 2.

1 4340 h

Figure 3.20.3.1.17

4340 Condition/Ht: UTS=180-200KSI Yield Strength: Form: 1 in. Plate Specimen Type: CCP (max stress specified) Ult. Strength: Specimen Thk: 0.163 in. Orientation: Specimen Width: 5 in. Frequency: 10 Hz Ref: BW002 Environment: H.H.A.; RT (2 of 2)(1 of 2) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 100 100 10 10 40 10° 10° Stress Ratio: 0.5 Stress Ratio: 0. 10 -2 10-2 10⁻¹ 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10⁻⁶ 10⁻⁵ 10 -5 10⁻⁷ 10⁻⁷ 10 6 10-6 10 -8 10 40 100 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) Δ K (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 2.60 2.68 3.87 22.90 (min) 18.90 (min) 20. 25. 30. 35. 25. 30. 35. 40. 6.12 8.98 50. 11.6 60. 44.30 (max) 12.8 214. 66.10 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error

Figure 3.20.3.1.18

2.

1.25

9.51

0.

.5 .8

10.70

1.25

.5

.8

0.

2.

4340 R

Condition/Ht: UTS=180-200KSI

Form: 1 in. Bar

Specimen Type: CCP (max stress specified)

Orientation: L-T Frequency: 3 Hz

Environment: H.H.A.; RT

Yield Strength: 182.5 ksi Ult. Strength: 193.7 ksi Specimen Thk: 0.4 in. Specimen Width: 4 in.

Ref: BW001

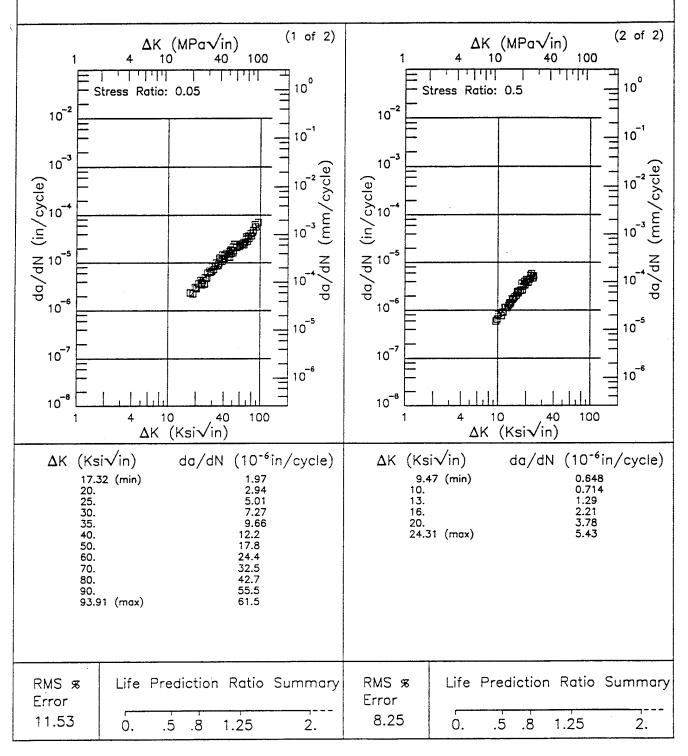


Figure 3.20.3.1.19

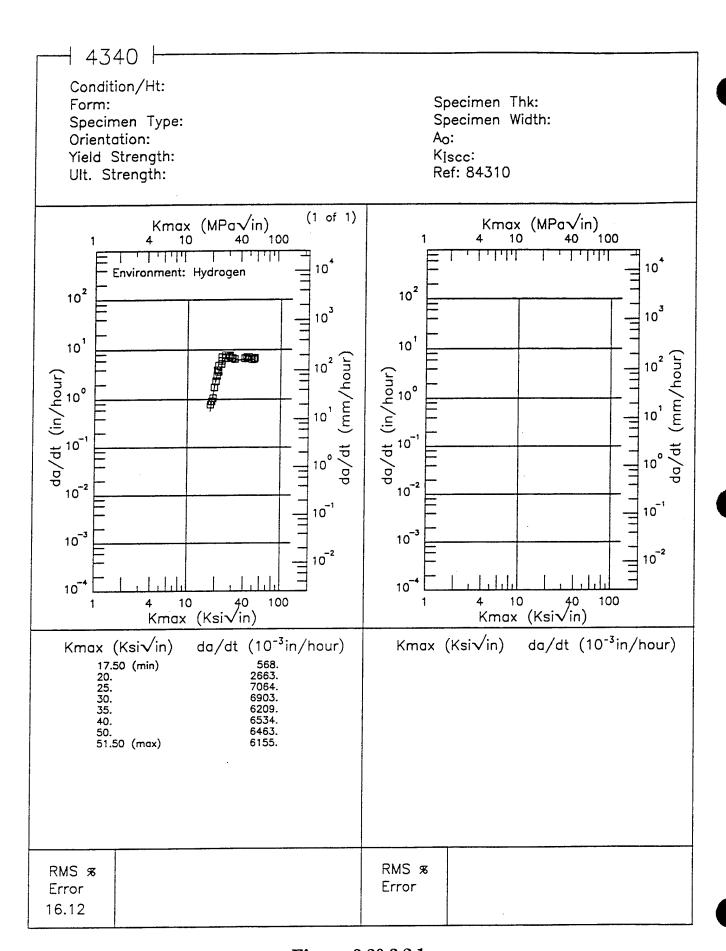


Figure 3.20.3.2.1

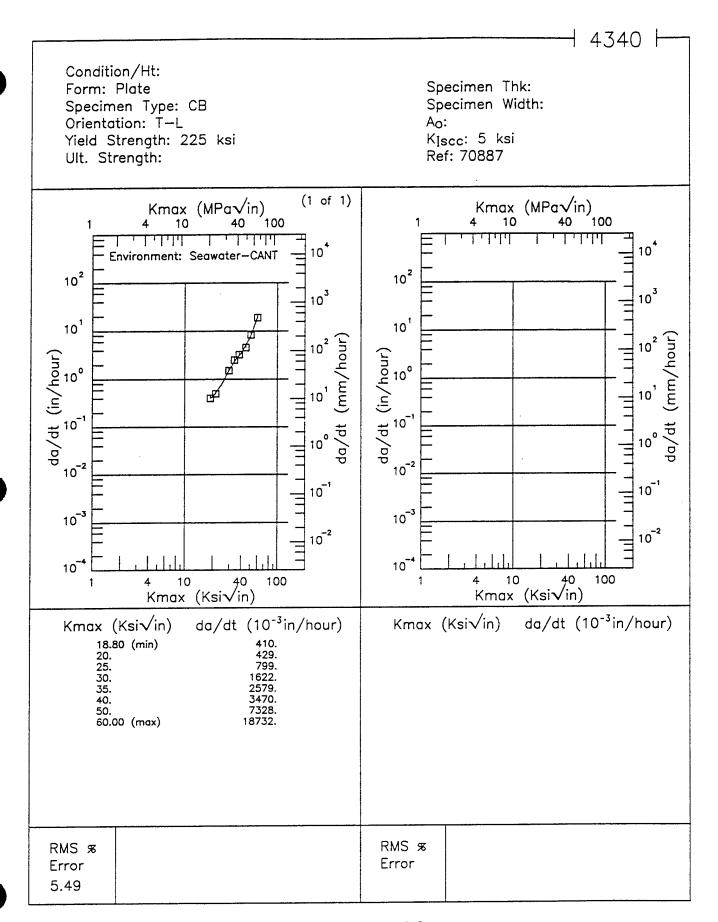


Figure 3.20.3.2.2

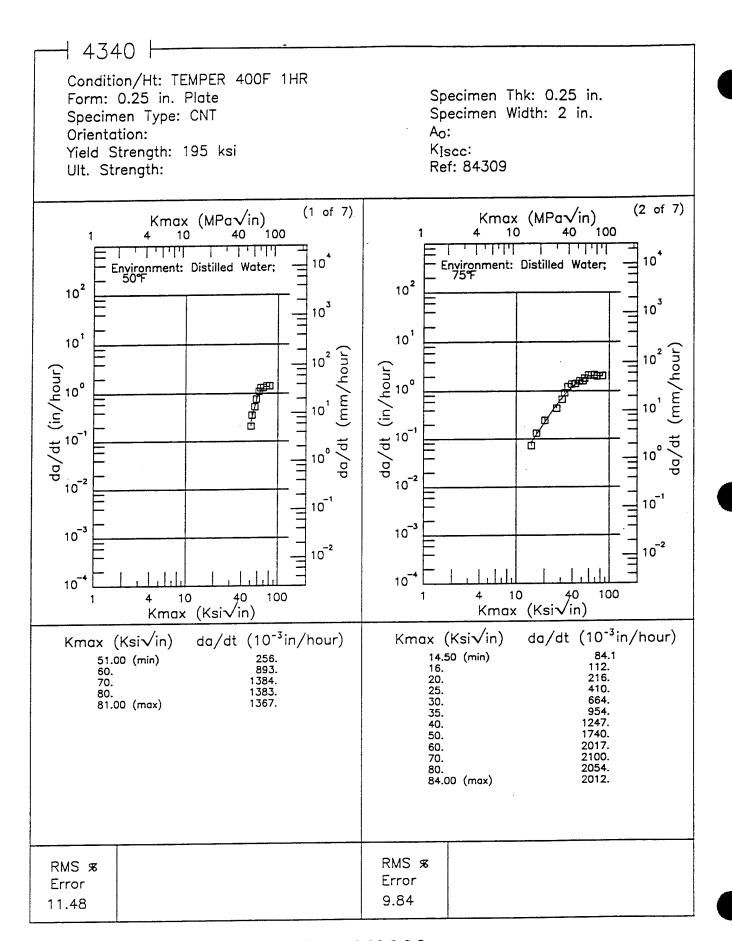


Figure 3.20.3.2.3

1 4340 H Condition/Ht: TEMPER 400F 1HR Form: 0.25 in. Plate Specimen Thk: 0.25 in. Specimen Type: CNT Specimen Width: 2 in. Orientation: Ao: Yield Strength: 195 ksi Kiscc: Ref: 84309 Ult. Strength: (3 of 7)(4 of 7)Kmax (MPa√in) Kmax (MPa√in) 100 10 40 10 40 100 1 1 1 1 1 1 1 الملتليل 11111 $\frac{1}{1}$ 10 10⁴ Environment: Distilled Water; 127°F Environment: Distilled Water; 10² 10² 103 103 101 10 102 da/dt (in/hour) da/dt (in/hour) 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ 10 -2 10-2 10-4 10-1 4 10 40 Kmax (Ksi√in) 4 10 40 Kmax (Ksi√in) 100 100 Kmax (Ksi√in) $da/dt (10^{-3}in/hour)$ Kmax (Ksi√in) $da/dt (10^{-3}in/hour)$ 26.00 (min) 30. 35. 40. 22.50 (min) 25. 30. 35. 2009. 5804. 3961. 8072. 5371. 5821. 12816. 50. 40. 6726. 13293. 50. 60. 7564. 13718. 7151. 60. 80.00 (max) 64.00 (max) 7333. 16594. RMS % RMS % Error Error 10.02 9.89

Figure 3.20.3.2.3 (Continued)

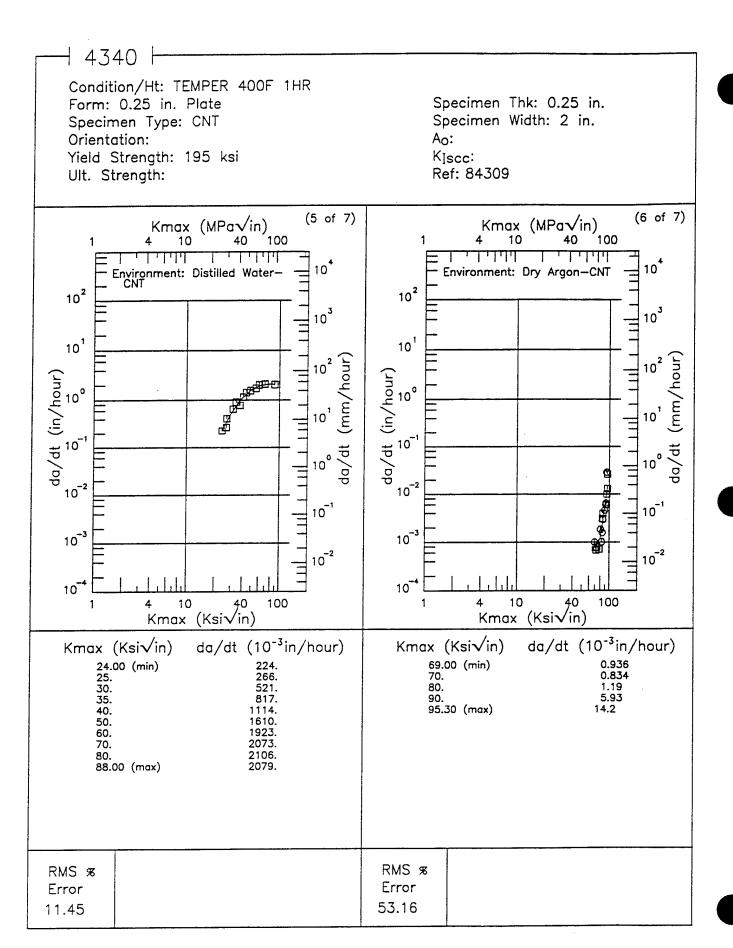


Figure 3.20.3.2.3 (Continued)

1 4340 H Condition/Ht: TEMPER 400F 1HR Form: 0.25 in. Plate Specimen Thk: 0.25 in. Specimen Type: CNT Specimen Width: 2 in. Orientation: Ao: Yield Strength: 195 ksi Kiscc: Ult. Strength: Ref: 84309 (7 of 7)Kmax (MPa√in) Kmax (MPa√in) 40 40 100 10 10 الليليل 11111 10⁴ 10⁴ Environment: Dry Hydrogen-CNT 10² 10² 103 103 101 101 10² (mm/hour) da/dt (in/hour) da/dt (in/hour) 10 da/dt 10-2 10-2 10-1 10-1 10⁻³ 10-3 10-2 10-2 10 10 40 4 10 40 Kmax (Ksi√in) 10 100 100 Kmax (Ksi√in) Kmax (Ksi√in) $da/dt (10^{-3}in/hour)$ Kmax (Ksi√in) $da/dt (10^{-3}in/hour)$ 24.00 (min) 25. 30. 35. 40. 8872. 50. 53.00 (max) 13608. 14919. RMS % RMS %

Figure 3.20.3.2.3 (Concluded)

Error

Error

5.4

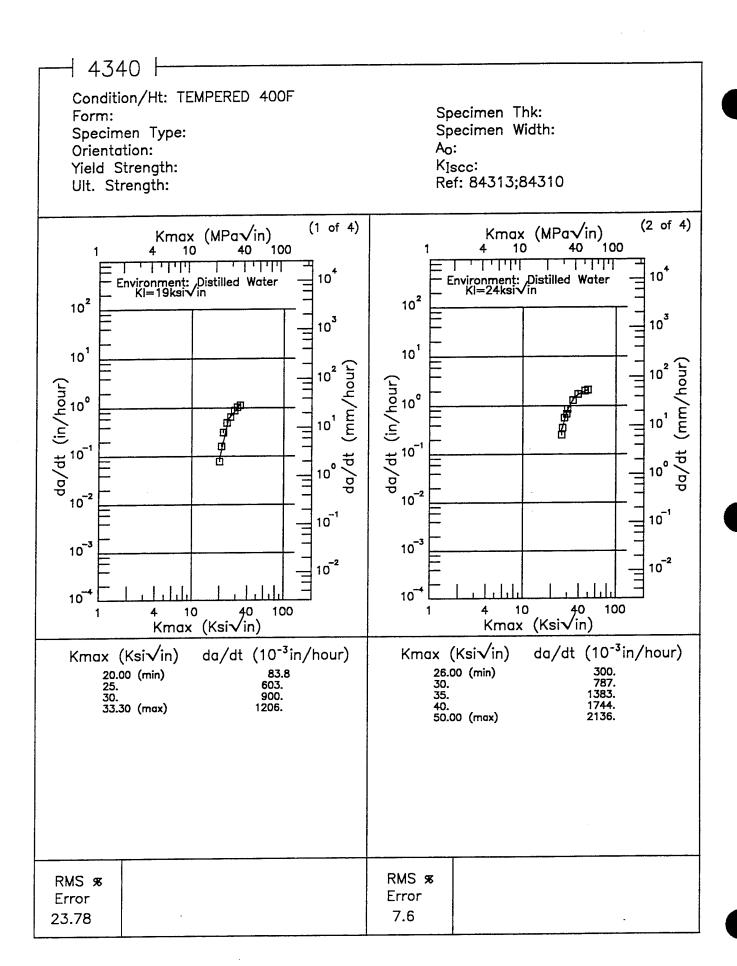


Figure 3.20.3.2.4

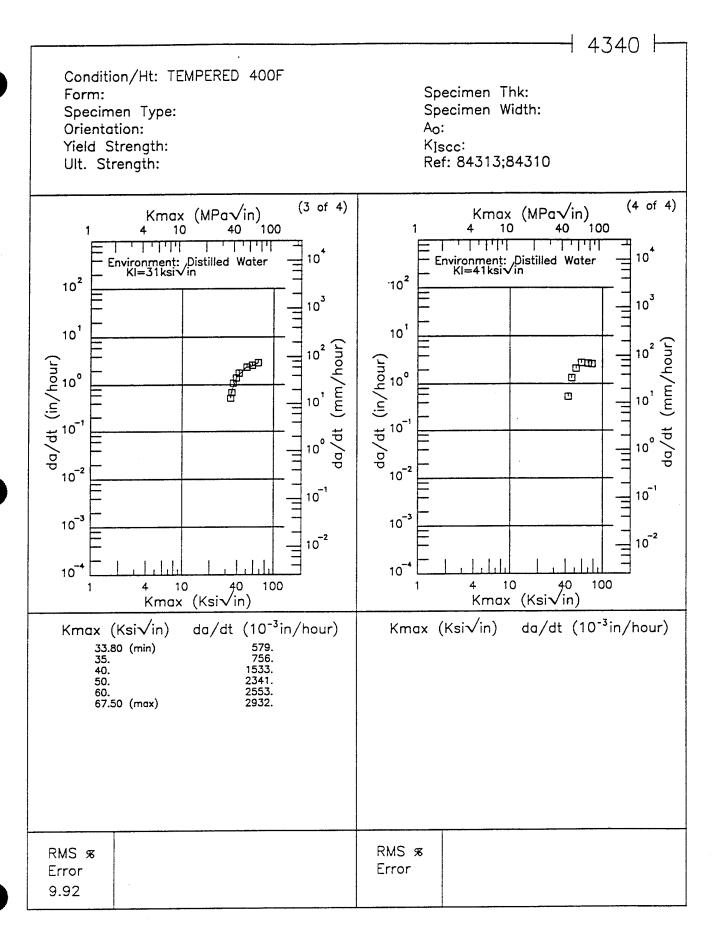


Figure 3.20.3.2.4 (Concluded)

┧ 4340 ト Condition/Ht: TYS=200-240KSI Specimen Thk: 0.48 in. Form: 1.5 in. Extrusion Specimen Width: 1.5 in. Specimen Type: NB - 3 pt Ao: Orientation: L-S K_{Iscc}: 13 - 16 ksi Yield Strength: 202 - 240 ksi Ref: 74718 Ult. Strength: Kmax (MPa√in) 40 100 (2 of 4) (1 of 4)Kmax (MPa√in) 10 40 1 1 1 111 11111 10⁴ 10 Environment: 3.5% NaCl — 0.09 wts Si Environment: 3.5% NaCl — 0.54 wt% Si 10² 10² 103 103 101 10 9 102 da/dt (in/hour) da/dt (in/hour) 10° 10⁻² 10-2 10⁻¹ 10-1 10⁻³ 10⁻³ 10-2 10-2 10-4 10 4 10 40 Kmax (Ksi√in) 100 4 10 40 Kmax (Ksi√in) 100 $da/dt (10^{-3}in/hour)$ $da/dt (10^{-3}in/hour)$ Kmax (Ksi√in) Kmax (Ksi√in) RMS % RMS % Error Error

Figure 3.20.3.2.5

1 4340 H

Condition/Ht: TYS=200-240KSI

Form: 1.5 in. Extrusion Specimen Type: NB - 3 pt

Orientation: L-S

Yield Strength: 202 - 240 ksi

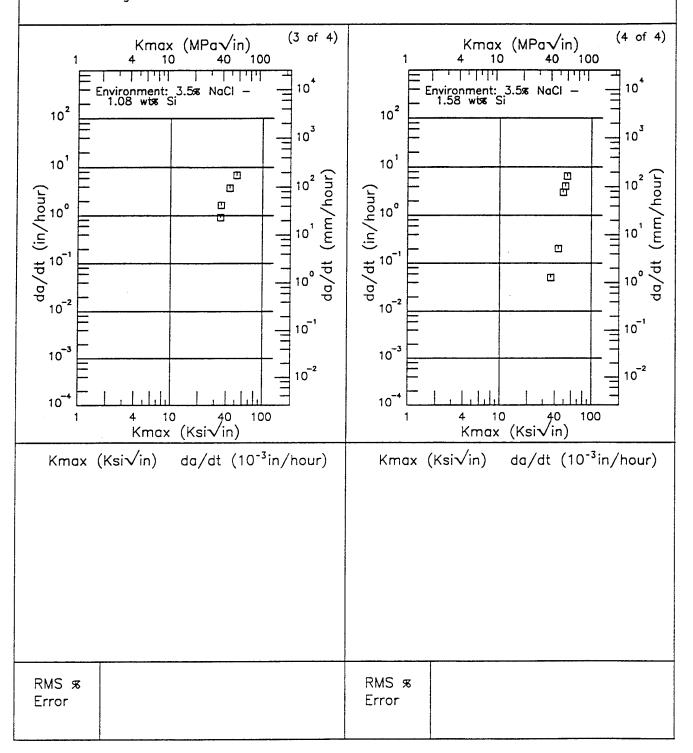
Ult. Strength:

Specimen Thk: 0.48 in. Specimen Width: 1.5 in.

Ao:

K_{Iscc}: 13 - 16 ksi

Ref: 74718



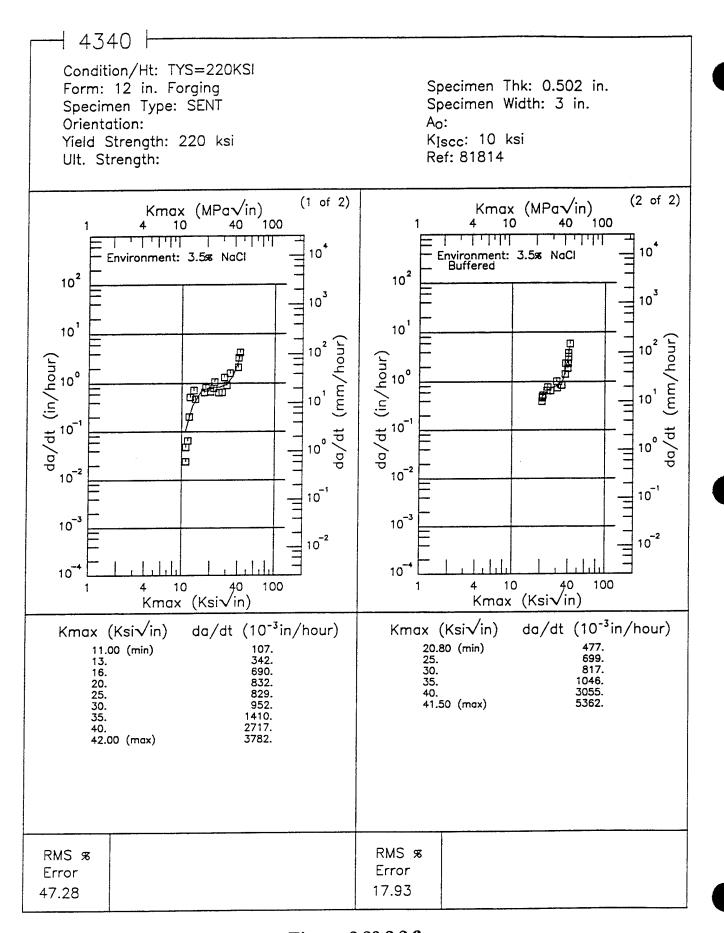


Figure 3.20.3.2.6

TABLE 3.20.3.3

K_{Isce} SUMMARY FOR ALLOY STEEL 4340

	f	Test		Yield		S	Specimen		Prod	1	;	;	Test		
Condition/ Heat Treat	Form	Temp (°F)	Spec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)		Crack (in)	Kq (Ksi√in)	K _{leo} (Ksivin)	Time (min)	Test Date	Reference
Unspecified	S	R.T.		I	3.5% NaCl	CNT	****	i	i i	1 1	80	10	i	1968	84290
•	Ь	R.T.	L-T		3.5% NaCl	CANT	:	1			57	10	:	1968	84290
Unspecified	拓	R.T.	÷	200	Dist Water	CANT	0.394	0.394	0.4	i	88	45	48800	1969	76972
1350°F OQ; 750°F 1.25hr	d	R.T.	T-S	194	3.5% NaCl	CANT	-	0.4	П	1	72.2	8.5	20000	1970	78761
1550° F OQ; 750° F Crack Prestressed to 80% KIC	Ь	R.T.		194.2	3.5% NaCl	NB*	1	0.5	1	•	72.2	24	20000	1972	84356
1550° F OQ; 750° F Crack Prestressed to 60% KIC	P	R.T.	-	194.2	3.5% NaCl	NB.	1	0.5	-	ŀ	72.2	23	20000	1972	84356
1550° F OQ; 750° F 1hr Crack Prestressed to 20% KIC	ď	R.T.	ŀ	194.2	3.5% NaCi	NB*	1	0.5	1	i.	72.2	8	20000	1972	84356
1550° F OQ; 750° F Crack Prestressed to 40% KIC	ď	R.T.	:	194.2	3.5% NaCl	NB.	. 1	0.5		i	72.2	17	20000	1972	84356
1550° F OQ; 750° F Crack Prestressed to 20% KIC	P	R.T.	i	194.2	3 5% NaCl	NB.	1	0.5	1	1	72.2	12	20000	1972	84356
1575°F OQ; 675°F 4hr	Ь	R.T.	!	209.6	Dist Water	CANT.	0.665	0.25	0.75	0.13	48.8	9.8	7500	1965	63061

(2 of 3)

TABLE 3.20.3.3 (CONTINUED)

K_{lsc} SUMMARY FOR ALLOY STEEL 4340

)		Test	7	Yield		İS	Specimen		Prod				Tog		
Condition Heat Treat	Form	Temp (°F)	Spec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)		Crack (in)	Kaivin)	K _{lace} (Ksi√in)	Time (min)	Test Date	Reference
1575°F OQ; 800°F 4hr	P	R.T.	l	222.4	Dist Water	CANT	0.665	0.25	0.75	0.13	48.6	8:6	2640	1965	19089
1600°F 1hr OQ; 600°F 1+1hr	F	R.T.	I	220	3.5% NaCl	SENT	က	0.502	12	9.0	I	10	-	1971	81814
1625°F Q; 1525°F OQ;	ß	E		212.2	Air 90% PH	PTSC	1.5	0.48	æ	0.14	63	27	1	1965	74718
400 f z+znr; 1625°F Q; 1525°F OQ	¥	K.1.		220.8	Air 90% PH	PTSC	1.5	0.48	8	0.14	63.6	57	1200	1965	74718
1650°F 1hr AC; 1680°F 2hr OQ; LN 0.25hr; 400°F 1+1hr OQ	В	R.T.	L-T	245	3.5% NaCl	CANT"	1.45	0.575	ii.	1	51	15	3500	1969	75025
1650°F 1hr AC; 1480°F 2hr OQ; LN 0.25hr; 400°F 1+1hr OQ	В	R.T.	L-T	249	3.5% NaCl	CANT.	1.45	0.575	1.5	l	51	15	1800	1969	75025
1700°F 0.25hr AC;	σ	т а		906	3.5% NaCl	CNT	2	0.05	90'0	:		29	1000	1968	72283
600°F 1+1hr	2	14: 1:		700	Dist Water	CNT	2	0.05	0.08	ı	1	29	1000	1968	72283
						CANT	1	1	1	÷	82	25		1071	80423
1800°F Q;	ß	£	ت -	010	O KO MAC	CANT	ī	1	п	1	82	30		1071	80423
600°F 1+1hr	4		3	017		CANT	1	1	-	į	78	22	i	17.61	80423
						CANT	1	1	-	i	78	24	ï	1971	80423

TABLE 3.20.3.3 (CONCLUDED)

Kisce SUMMARY FOR ALLOY STEEL 4340

	e e	Test	5	Yield		S	Specimen		Prod		;	,	Test		
Condition/ Heat Treat	Form	Temp (°F)	Spec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)		Crack (in)	Kai√in)	K _{law} (Ksi√in)	Time (min)	Test Date	Reference
						CANT	-	1	-		78	23	1	1971	80423
						CANT	-	1	1	ï	78	24	***	1971	80423
						CANT	1	1	F	į	78	25	•••	1671	80423
1800° F Q;	댠	R.T.	L-S		3.5% NaCi	CANT	-	-	1	i	82	25		1971	80423
contd)	(cont'd)	(contd) (contd)	(cont'd)		(confd)	CANT	П	1	1	÷	82	24	****	1971	80423
						CANT	T	1	1	i	78	26	•	1971	80423
						CANT	1	1	1	i	82	31	ı	1971	80423
						CANT	1	1	1	***	82	23	•	1971	80423
TYS=125KSI	P	R.T.	T-L	125	Seawater	CANT	-				89	+0.4	-	1961	70887
TYS=150KSI	P	R.T.	T-L	150	Seawater	CANT					85	59	:	1961	7887
TYS=175KSI	P	R.T.	T-L	175	Seawater	CANT		***			75	27	:	1961	70887
TYS=200KSI	P	R.T.	T-T	200	Seawater	CANT					- 29	10		1961	70887
TYS=225KSI	Ъ	R.T.	T-L	225	Seawater	CANT					63	5	1200	1961	78807

 $^{+}$ crack length and/or specimen thickness does not meet minimum requirements of $2.5~(rac{K_{loo}}{\sigma_{ys}})^{2}$

^{*} asterisk in specimen design column indicates that specimens are side-grooved

1 of 1

TABLE 3.21.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL 4340 (AM) AT ROOM TEMPERATURE

			ď	
		S-L	Std Dev	:
			Mean K _{lo}	* ;
<u>a</u>)	ntation		п	:
$K_{Ic}~(ksi\sqrt{in})$	n Orie	T-L	Std Dev	:
K_{Ic}	Specimen Orientation		Mean K _{le}	
	<i>6</i> 2		ď	3
		L-T	Std Dev	0.5
			Mean Std K _{lc} Dev	40.5
	Condition/Heat Treatment			1600F 1HR AC 1550F 1HR OQ -320F 0.5HR 400F 2HR AC
Product	Form			Forging

TABLE 3.21.2.1

					ALLOY	ALLOY STEEL	4340 (4340 (AM) K _{lo}	, II						
	PRO	PRODUCT					SPECIMEN	7	CRACK			K			
CONDITION	FORM	THICK (in.)	TEST TEMP (*F)	SPEC	YIRLD STR (Kal)	WIDTH (in.)	THICK (IL.) B	DEBIGN	LENGTH (in.) A	E.S. (fn.)	K (Kal	K. MBAN	BTAN	DATE	REFER
		4.00			241.0	1.800	0.900	NB	!	0.07	41.00			1968	73300
1600F 1 HR AC 1550F 1 HR 0Q -320F 0.5 HR 400F 2 HR AC	Forging	4.00	R.T.	5	241.0	1.800	0.900	NB	-	0.07	40.60	40.5	5	1968	73300
		4.00			241.0	1.800	0.800	NB NB	ı	0.07	40.00	!	}	1968	73300

TABLE 3.22.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL 4340 (DH) AT ROOM TEMPERATURE

			u	i	i
		S-L	Std Dev	i	:
	·		Mean K _{ie}	i	1
a)	ntation		u		4
$K_{lc}~(ksi\!\sqrt{in})$	n Orie	T-L	Std Dev		6.2
K_{Ic}	Specimen Orientation		Mean K _{lo}	l	66.3
	S		ď	L	i
		L-T	Std Dev	œ.	i
			Mean K _{le}	51	į
	Condition/Heat Treatment			1600F 1HR AC 1550F 1HR OQ -320F 0.5HR 400F 2HR AC	1550F OQ 900F 1HR
Product	Form			Forging	Billet

TABLE 3.22.2.1

					ALLOY STEEL	STEEL	4340 (DH)		K _{Io}						
	PROI	PRODUCT				92	SPECIMEN	7	CRACK			K _{Ie}			
CONDITION	FORM	THICK (In.)	TERF TEMP (°F)	SPRC	YIELD STR (Kal)	WIDTH (fn.) W	THICK (in.) B	DESIGN	LENGTH (in.) A	(K _w ,TYS)* (in.)	K. (Kei •	K. MEAN	STAN DRV	DATE	REFER
		1.00			:	2.000	1.000	CT	1.023		88.00			1970	84280
dire door oo dosse		1.00		I	:	2.000	1.000	CT	1.030	:	103.00			1970	84280
1990F OG BOOF IRK	Billet	1.00	901-		ı	2.000	1.000	cr	1.030		109.00	98.6	8.9	1970	84280
		1.00			ı	2.000	1.000	cr	1.026		94.00			1970	84280
1660F OQ 900F 1HR	Billet	1.00	-77-	I-T	:	2.000	1.000	CT	1.045		107.00		:	1970	84280
		1.00		1	ı	2.000	1.000	cr	1.015		62.00			1970	84280
1550F OQ 900F 1HR	Billet	1.00	8	15	:	2.000	1.000	CT	1.000	:	62.00	60.3	2.9	1970	84280
		1.00			ı	2.000	1.000	CT	1.005	•	57.00			1970	84280
		1.00			1	2.000	1.000	CT	1.000		75.00			1970	84280
TITE TOOK OO TOTAL		1.00	E		!	2.000	1.000	CT	1.025	:	66.00			1970	84280
TODAL OF BOARD	Dillet	1.00	r. I.	1	ı	2.000	1.000	CT	1.010	ï	63.00	66.3	6.2	1970	84280
		1.00			-	2.000	1.000	CT	1.020	ŀ	61.00			1970	84280
		4.00			229.0	1.800	0.900	NB NB	i	0.12	61.10			1968	73300
		4.00			229.0	1.800	0.900	NB BB	:	0.14	64.30			1968	73300
		4.00		I	229.0	1.800	0.900	NB NB	:	0.15	65.30			1968	73300
1600F 1 HR AC 1550F 1HR OQ -320F 0.5HR 400F 2HR AC	Forging	4.00	R.T.		229.0	1.800	0.900	NB NB	:	0.12	51.30	61.0	3.0	1968	73300
		4.00			231.0	1.800	0.900	NB .	:	0.12	49.70			1968	73300
		4.00		1	231.0	1.800	0.900	NB NB	i	0.10	46.90			1968	73300
		4.00			231.0	1.800	0.900	NB NB	:	0.11	48.40			1968	73300
		4.00			233.0	1.800	0.800	NB	:	0.13	62.50			1968	73300
1600F 1 HR AC 1550F 1HR OQ -320F 0.5HR 400F 2HR AC	Forging	4.00	R.T.	s.	233.0	1.800	0.900	NB	i	0.13	62.50	62.5	0.0	1968	73300
		4.00			233.0	1.800	0.900	NB NB	1	0.13	62.50			1968	73300

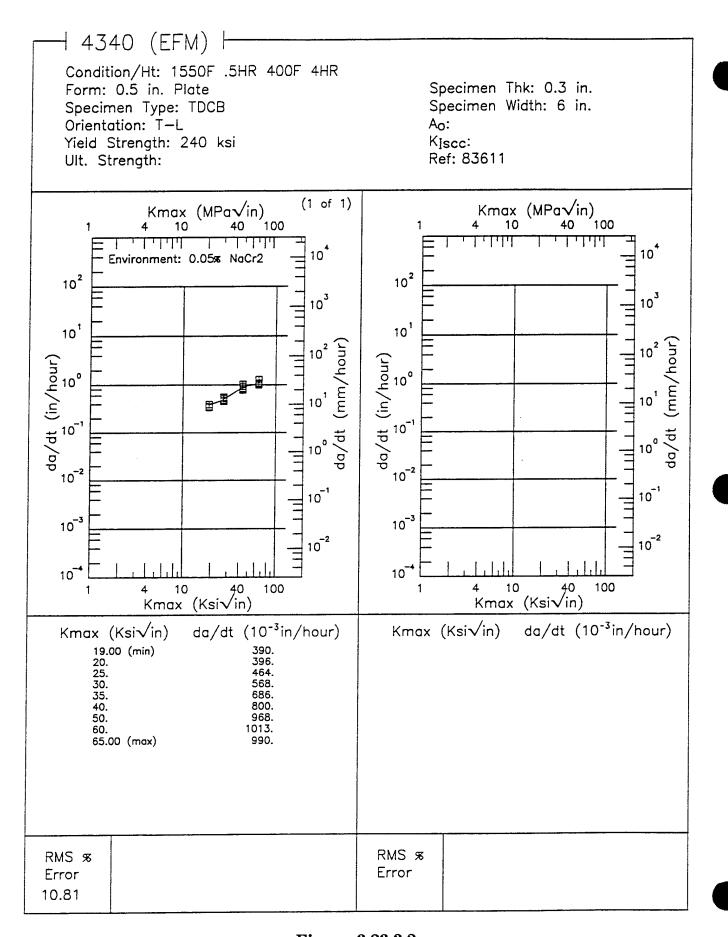


Figure 3.23.3.2

TABLE 3.24.3.3

Klecc SUMMARY FOR ALLOY STEEL 4340(MOD)

D. J. J. J. J. J. J. J. J. J. J. J. J. J.	2	Test	Č	Yield		S	Specimen		Prod		;	,	Test	1	
Condition Heat Treat	Form	Temp (°F)	Spec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)	Thk (in)	Crack (in)	Ko (Ksi√in)	K _{leo} (Ksivin)	Time (min)	Test Date	Reference
1650°F 1hr;	f	Ę		201.8	3.5% NaCl	CANT	1.5	0.48	1.5	i	73	13	5000	1965	74718
1600°F Ihr OQ 1+1 600°F (0.09 SI)	27	K.T.	T-L	204.2	3.5% NaCl	CANT	1.5	0.48	1.5	i	78	18	5000	1965	74718
1800°F Q; 460°F 1+1hr (0.20C)	댅	R.T.	S-T	195	3.6% NaCl	CANT	1	ı	1	i	87	56	į	1971	80423
1800°F Q; 500°F 1+1hr (0.21C)	F	R.T.	S-T	195	3.5% NaCl	CANT	1	1	1	ļ	87	52	į	1971	80423
1800°F Q; 600°F 1hr (0.20C)	F	R.T.	r-s	195	3.5% NaCl	CANT	1	1	1		86	72	1	1971	80423
1800°F Q; 650°F 1hr (0.24C)	F	R.T.	r-s	195	3.5% NaCl	CANT	1	1	1		92	62		1971	80423
1800°F Q; 650°F 1+1hr (0.28C)	F	R.T.	r-s	195	3.5% NaCl	CANT	1	1	1		87	35		1971	80423
1800°F Q; 700°F 1hr (0.21C)	F	R.T.	L-S	195	3.5% NaCl	CANT	Ħ	1	1		85	42		1971	80423
1800°F Q; 780°F 1+1hr (0.33C)	F	R.T.	r-s	195	3.5% NaCl	CANT	1	1	-	•	87	32		1831	80423
1800°F Q; 800°F 1hr (0.46C)	F	R.T.	r-s	195	3.5% NaCl	CANT		1	1		78	20		1971	80423
1800°F Q; 900°F 1hr (0.64C)	ᄕᅫ	R.T.	L-S	195	3.5% NaCl	CANT	-	1	-	i	65	30	i	1971	80423
1800°F Q; 925°F 1+1hr (0.53C)	F	R.T.	L-S	195	3.5% NaCl	CANT	-	1	1		87	42	1	1971	80423

TABLE 3.25.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL 4340 (VAR) AT ROOM TEMPERATURE

Product					K_{Le}	$K_{Ic}~(ksi\!\sqrt{in})$	<u>a</u>)			
Form	Condition/Heat Treatment			S	pecime	Specimen Orientation	ıtation			
			L-T			T-T			\mathbf{S} - $\mathbf{\Gamma}$	
		Mean K _{le}	Std Dev	4	Mean K ₁₆	Std Dev	и	Mean K,	Std Dev	u
Forging	1600F 1HR AC 1550F 1HR OQ -320F 0.5HR 400F 2HR AC	55.	4.4	80	i	i	:	i	i	i

			-	1	XOTIV	ALLOY STEEL	4340 (VAR)	1 1	K_{lo}						
	PROI	PRODUCT				-	SPECIMEN	z	CRACK			K _{Io}			
CONDITION	FORM	THICK (in.)	TEBT TEMP (°F)	SPEC OR	YIELD STR (Kel)	WIDTH (la.) W	THICK (la.) B	DESIGN	LENGTH (ln.) A	(K., TYS)* (in.)	K. (Kel • √∏.)	K. MEAN	BTAN	DATE	RRFER
		4.00			240.0	1.800	0.900	NB	i	0.13	65.00			1968	73300 (1)
		4.00			240.0	1.800	0.900	NB	ł	0.16	61.30			1968	73300 (1)
		4.00			240.0	1.800	0.900	NB	:	0.12	61.80			1968	73300 (1)
1600F 1 HR AC 1550F 1 HR OQ		4.00	E	E	240.0	1.800	0.900	NB	:	0.15	69.20			1968	73300 (1)
-320F 0.5 HR 400F 2 HR AC	Forging	4.00		<u>.</u>	241.0	1.800	0.900	NB NB	i	0.10	48.60	0.99	7.7	1968	73300
		4.00			241.0	1.800	0.900	NB BN	i	0.13	64.60			1968	00002
		4.00			241.0	1.800	0.900	NB NB	ï	0.11	61.10			1968	73300
		4.00			241.0	1.800	0.800	NB		0.15	68.60			1968	73300

NOTES: (1) COMPOSITION (WT PERCENT) 0.42C, 0.81Mn, 0.008P, 0.0048, 0.368i, 1.63Ni, 0.84Cr, 0.22Ma, 0.001Al, 0.002Ca, 0.002ZN

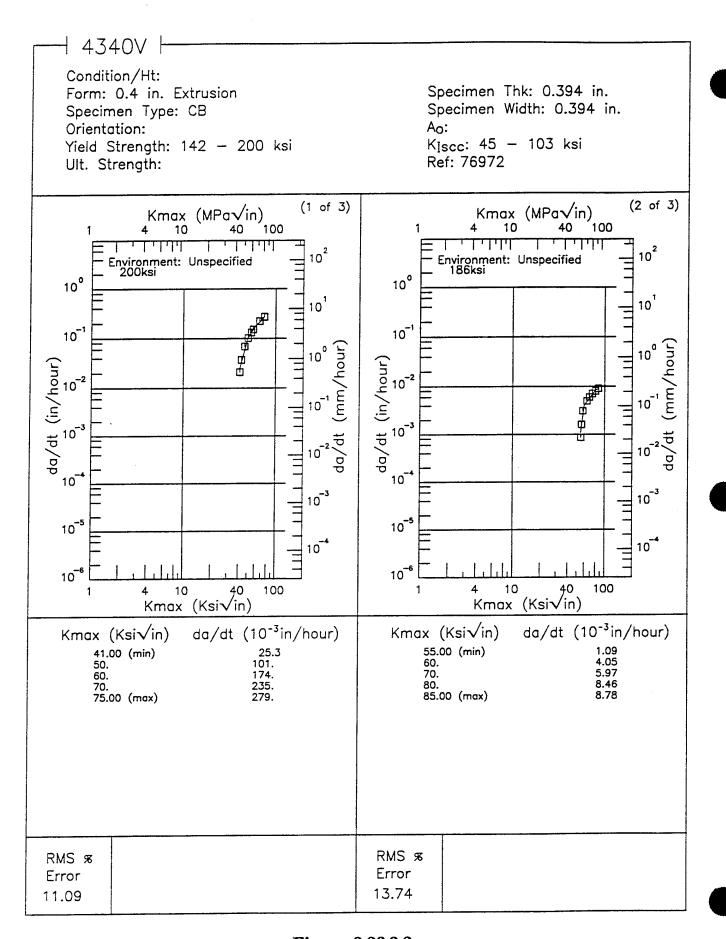


Figure 3.26.3.2

Condition/Ht:

Form: 0.4 in. Extrusion Specimen Type: CB

Orientation:

Yield Strength: 142 - 200 ksi

Ult. Strength:

Specimen Thk: 0.394 in. Specimen Width: 0.394 in.

Ao:

K_{Iscc}: 45 - 103 ksi

Ref: 76972

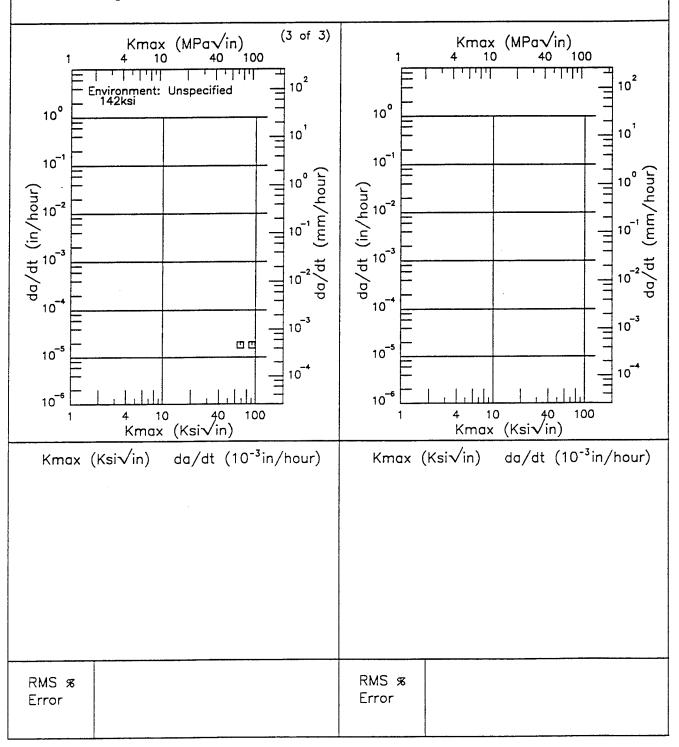


TABLE 3.27.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK A286 AT ROOM TEMPERATURE

ORIENTATION: L-T

	106.0	
	80.0	31.48
Air	ZR (10 ⁻⁸ in/cyc [Lovel (Kst/ii 10.0 20.0	1.59
ENVIRONMENT: Lab Air		
NIME	FCO AV	
NVIR	5 9	
<u>.</u>	FREQ (Hz)	3
	R	0.05
	UCT.	TE
L-T	PRODUCT	PLATE
ORIENTATION: L-T	INI	SHR AC
ORIENT	CONDITION/ HEAT TREATMENT	1800F 0.5-1.0 HR WQ 1325F 16HR AC
	CONT	0.5-1.0 HR
	H	1800F

TABLE 3.27.1.2.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK AZ86 AT ROOM TEMPERATURE

	1900	
	0'0	
ENVIRONMENT: Lab Air	FCGR (10 ⁻⁸ in/cycle) ΔK Level (Ksi/in) 0 100 200 t	1.82
DNMENT	6.1	
NVIR	2.5	
	FREQ (Hz)	8
	R	90'0
: T-L	PRODUCT FORM	PLATE
ORIENTATION: T-L	CONDITION/ HEAT TREATMENT	1800F 0.5-1.0 HR WQ 1325F 16HR AC

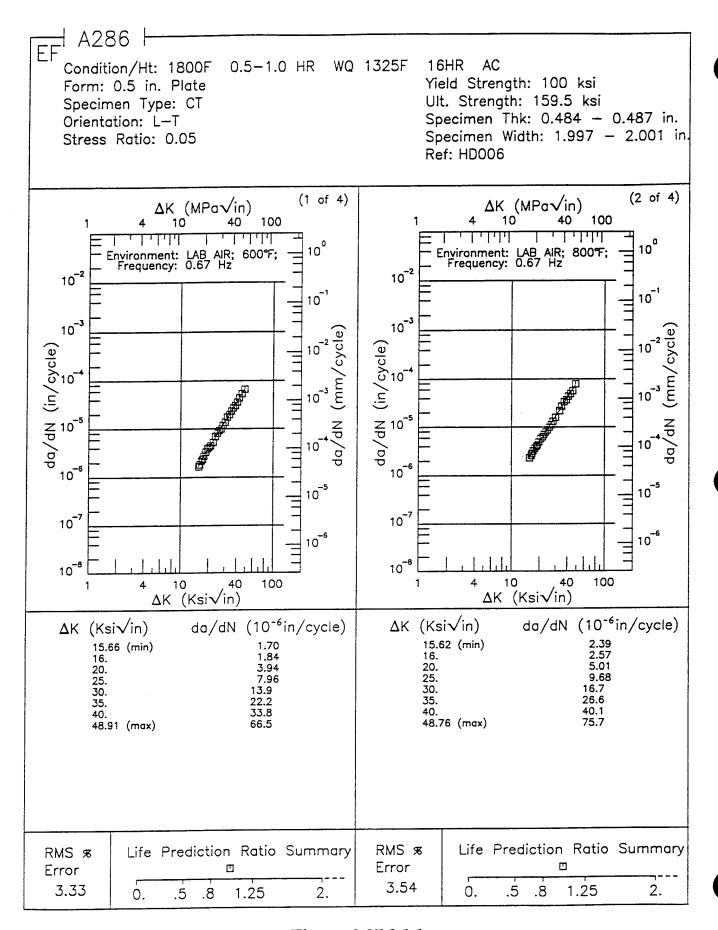


Figure 3.27.3.1.1

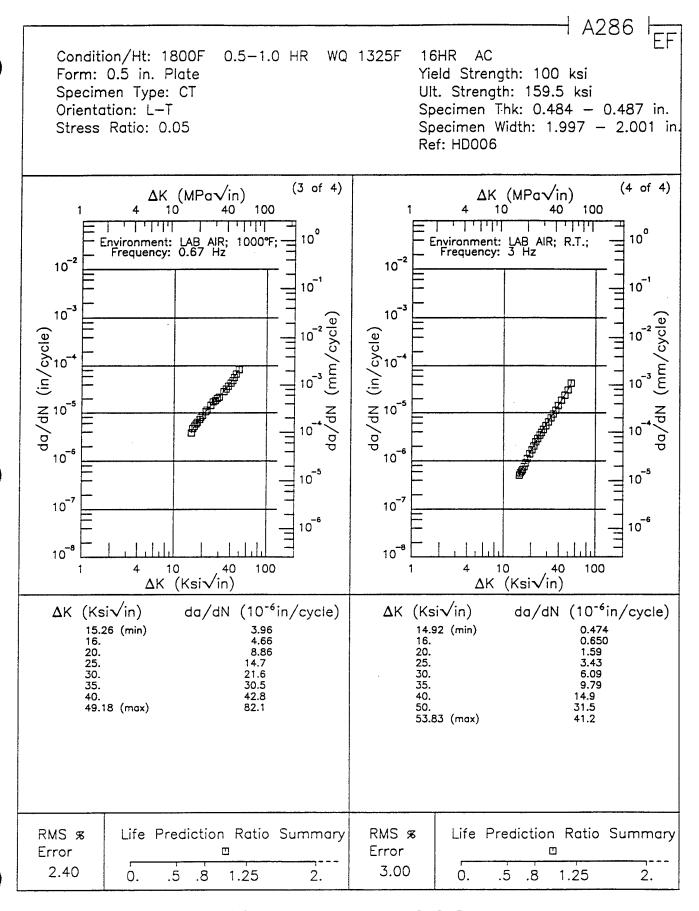


Figure 3.27.3.1.1 (Concluded)

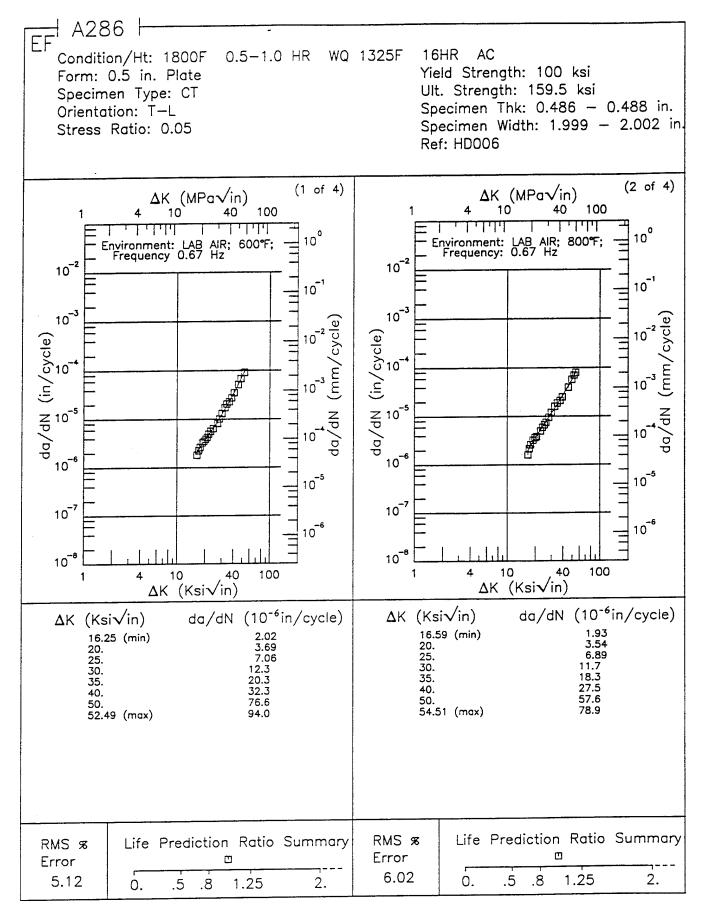


Figure 3.27.3.1.2

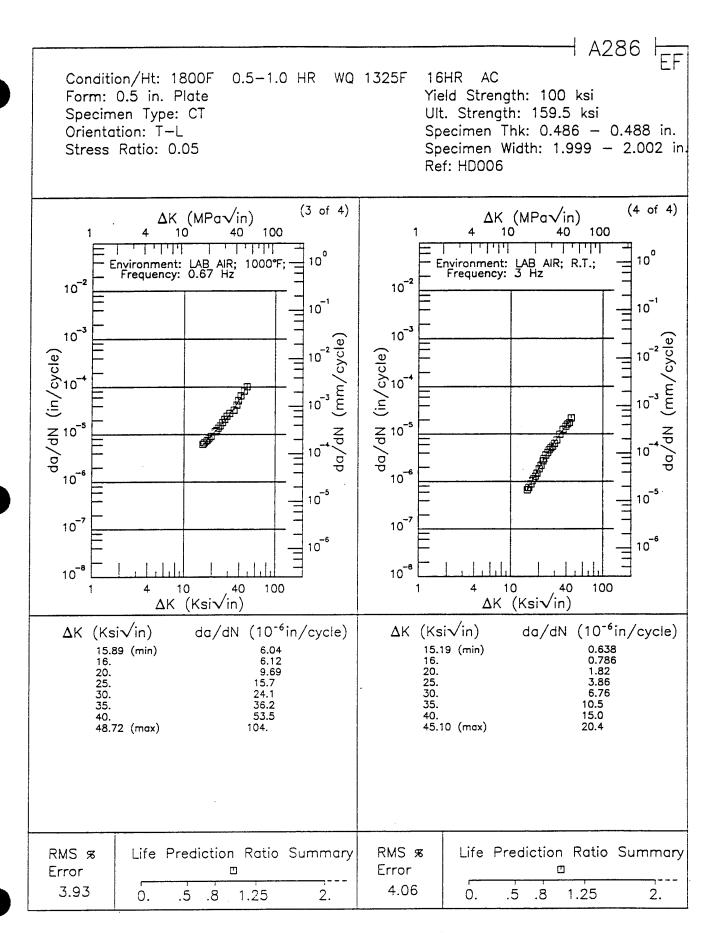


Figure 3.27.3.1.2 (Concluded)

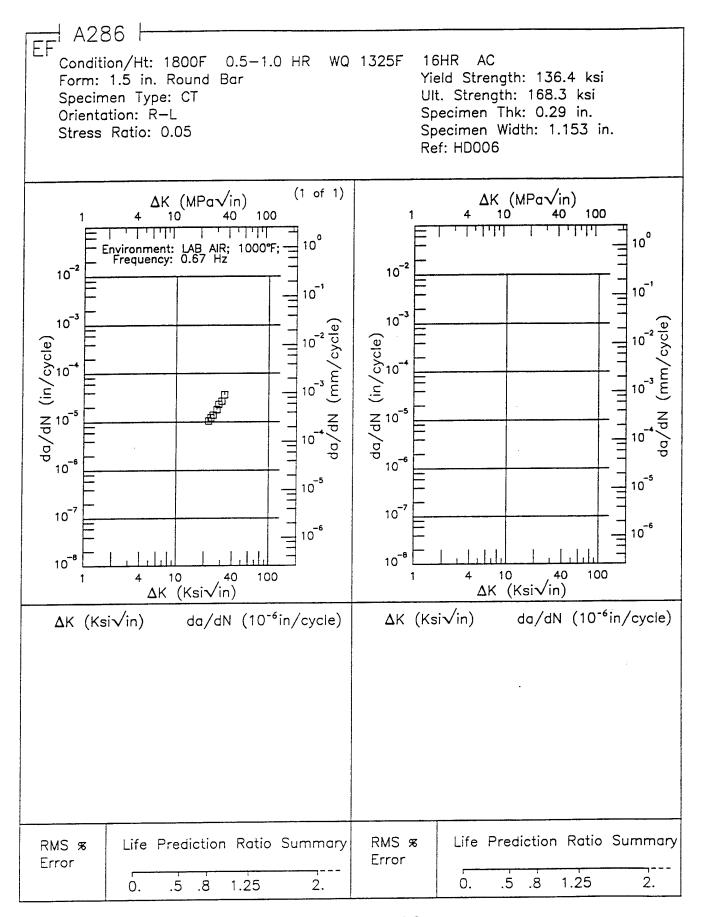


Figure 3.27.3.1.3

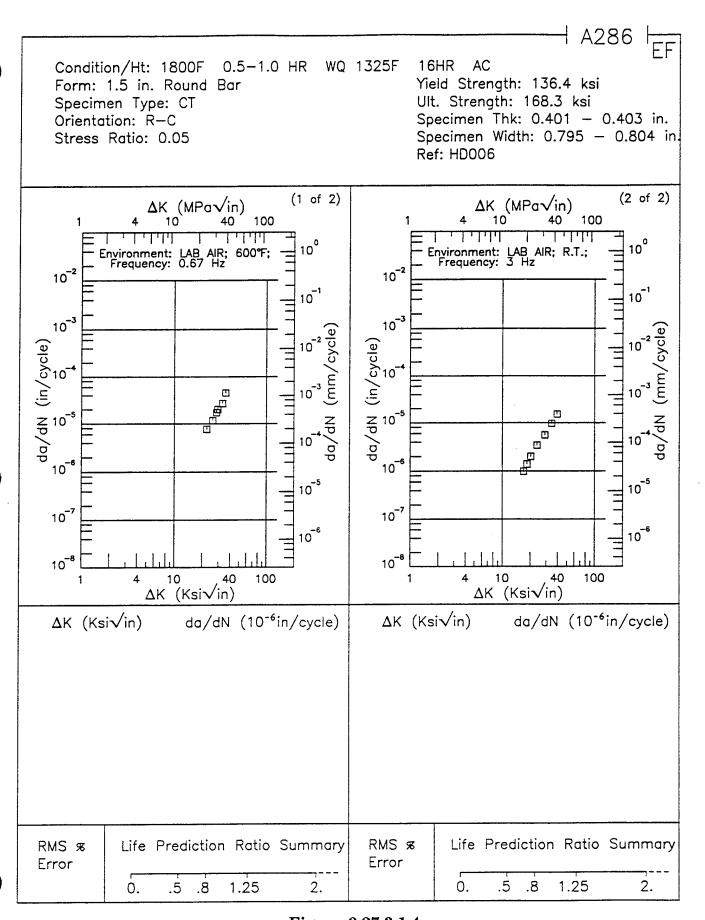


Figure 3.27.3.1.4

TABLE 3.28.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL AF 1410 AT ROOM TEMPERATURE

Product					K_{Ie}	$K_{Ic}~(ksi\sqrt{in})$	<u>'</u> @			
Form	Condition/Heat Treatment			S	Specimen Orientation	n Orie	ntation			
			L-T			T-L			S-L	
		Mean K _{Ie}	Std Dev	u	Mean K _{to}	Std Dev	u	Mean K _{io}	Std Dev	ď
Plate	1650F 1HR WQ 1500F 1HR WQ 950F 5HR AC	139.6	11.7	2	136.7	7.4	2	ŀ	i	:
Forging	Unspecified	98.7	11.3	9	105.6	4.8	3	:	i	:

TABLE 3.28.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK AF1410 AT ROOM TEMPERATURE

ORIENTATION: L-T

ENVIRONMENT: Lab Air

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15	₩Z#		
151.39	100.0		

	50.0		
32.69			
39	₩ ₹₩		
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673	******		FCGR (10 ⁻⁸ in/cycle)

	**************************************	ΔK Løvel (Ksi√in)	. U
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3.6	₩ =8		

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950F		ME	Z
AC 950F		TME	NO
1 AC 950F		ATME	TON
HR AC 950F		SATME	HOLL
1HR AC 950F		EATME	NOLL
F 1HR AC 950F		REATME	DIFFOR
00F 1HR AC 950F		ireatme	DIFFION
-100F 1HR AC 950F		TREATME	NOELIGN
100F 1HR AC 950F		I TREATME	NOLLIGNO
AC -100F 1HR AC 950F		VI TREATME	MOLLIONOS
3 AC -100F 1HR AC 950F		AT TREATME	CONDITION
HR AC -100F 1HR AC 950F		BAT TREATME	CONDITION
1HR AC -100F 1HR AC 950F		HEAT TREATME	CONDITION
F 1HR AC -100F 1HR AC 950F		HEAT TREATMENT	CONDITION
25F 1HR AC -100F 1HR AC 950F		HEAT TREATME	CONDITION
1526F 1HR AC -100F 1HR AC 950F 5HRS AC		HEAT TREATME	CONDITION

TABLE 3.28.1.2.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK AF1410 AT ROOM TEMPERATURE

ORIENTATION: T-1	i: T-L		A	ENVIRONMENT: Lab Air	NMEN	T: Lab	Air		
CONDITION	PRODUCT	ş	FREG		PC	FCGR (10 ⁻⁸ in/cycle)	⁸ in/cyc	(e)	
HEAT TREATMENT	FORM	ı	(Hz)		ΔF	ΔK Level (Kst/in)	(Ksi√ii	ı)	
				2.5	6.0	10.0	20.0	60.0	100.0
1525F 1HR AC -100F 1HR AC 950F 5HRS AC	ROUND BAR	0.02	0.1-30		0.11	99.0	3.64	31.7	172.61

TABLE 3.28.1.2.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK AF1410 AT ROOM TEMPERATURE

ORIENTATION: Unspecified

ENVIRONMENT: Lab Air

100.0		
cle) (n)	37.13	31
in/cyr (Ksi/);	4.2	4.4
CR (10.6) K Lovel		
9		
8.8		
FREQ (Hz)	10-30	1-30
Ж	0.08	0.08
PRODUCT FORM	PLATE	PLATE
CONDITION/ HEAT TREATMENT	AIR QUENCHED	OIL QUENCHED

	K _{ie}	K. K. STAN DATE REPER	96.50 MA018	105.40 MA018	77.10 MA018	107.80 98.7 11.3 1990 MA018	103.20 MA018	102.40 MA018	104.50 MA018	110.90 105.6 4.8 1990 MA018		79.40 1990 MA018	133.20 1990 MA018	131.60 1990 MA018	133.50 1990 MA018	146.50 1990 MA018	123.40 1990 MA018	109.90 1977 RI001	
2.6 • K.,TYS)* K. (R., (In.) (In.)				0.45 105	0.24 77.	0.46	0.41 103	0.40	0.47 104	0.62 110	0.42 101	0.26 79	0.69	0.67	0.71 138	0.87	0.69 128	0.54 108	0.49 111.10
	CRACK	LENGTH (In.) A	1.273	1.260	1.293	1.329	1.354	1.323	1.306	1.276	1.370	1.275	1.267	1.273	1.293	1.275	1.270	1	•
	7	DESIGN	CT	CT	CT	CT	CT	CT	CT	CT	CT	cr	CT	CT	L	Ç	CT	СТ	CT
	SPECIMEN	THICK (in.)	1.249	1.265	1.262	1.249	1.269	1.266	1.252	1.251	1.251	1.250	1.252	1.262	1.283	1.251	1.266	1.750	1.760
	.	WIDTH (In.)	2.499	2.492	2.512	2.503	2.526	2.511	2.502	2.501	2.502	2.500	2.499	2.501	1.277	2.503	2.503	3.500	3.500
		YIELD STR (Kei)	240.0	248.0	249.0	251.0	256.0	257.0	240.0	243.0	247.0	247.1	252.9	253.9	250.6	248.3	263.2	235.7	248.6
		SPEC				<u> </u>				T:L		R-L	T-T	T-L	LT	LT	LT	LT	T-T
		TREST TEMP (°F)			Ē	<u> </u>				R.T.		R.T.	R.T.	R.T.	R.T.	R.T.	R.T.	99-	
	oucr	THICK (fn.)	6.76	6.76	5.75	5.75	5.75	5.75	5.75	5.76	6.76	5.76	6.50	6.50	6.50	6.50	6.50	2.00	2.00
	PRODUCT	FORM			, in	Surging.				Forging		Forging	Forging	Forging	Forging	Forging	Forging	Plate	Plate
		CONDITION			:	i				ı		ï	1675 FOR 1HR; -100F FOR 3HR; 926F FOR 6 HR	1675 FOR 2HR; -100F FOR 3HR; 926F FOR 6 HR	1676F FOR 1HR AIR COOLED; 1676F FOR 1HR; -100F FOR 3HR; 926F 6 HR	1676F FOR 1HR AIWFAN COOLED; -100F FOR 3HR; AIR WARMED 926F FOR 6 HR	1676F FOR 2HR AIR COOLED; -100F FOR 3HR; 926F 6HR	1650F 1HR WQ 1500F 1HR WQ 950F 5HRS AC	1650F 1HR WQ 1600F 1HR WQ 950F 6HRS AC

TABLE 3.28.2.1 (CONCLUDED)

					ALLO	ALLOY STEEL	, AF 1410	1410 K _{Io}							
	PROI	PRODUCT				***	SPECIMEN	z	CRACK			K _{Ie}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (in.) W	THICK (in.) B	DESIGN	LENGTH (fn.) A	(K. TYS)* (In.)	K (Kei •	K. MEAN	STAN	DATE	REFER
1650F 1HR WQ 1500F 1HR WQ	Ē	2:00	Ē		228.4	3,500	1.750	CT		1.04	147.80			1977	RI001
950F 5HRS AC	Flate	2:00	R.T.	3	228.4	3.500	1.750	CT	-	0.82	131.30	139.6	11.7	1977	RI001
1650F 1HR WQ 1500F 1HR WQ	ŀ	2.00	Ş		228.4	3.500	1.750	LO	1	96.0	141.90			1977	RI001
950F 5HRS AC	Fiate	2.00	K.T.	7	228.4	3.500	1.750	CT	ì	0.82	131.40	136.7	7.4	1977	RI001
1650F FOR 2HR AIR COOLED; 1250F FOR 8HR; 1676 FOR 1HR; -100F FOR 3HR; 925 FOR 6 HR	Forging	6.50	R.T.	T-L	250.8	2.497	1.267	CT	1.266	0.77	139.40	i	ŀ	1990	MA018
1650F FOR 2HR AIR COOLED; 1250F FOR 8HR; 1676 FOR 1HR; -100F FOR 8HR; 925 FOR 6 HR	Forging	6.50	R.T.	L-T	251.5	20.504	1.256	cr	1.301	0.67	129.90	1	ŀ	1990	MA018
ACED AT GOAD EXILE	 6	3,25	E	:	241.5	2.494	1.250	cT	1.277	0.40	97.20			1990	MA018
AGED AL SOOF FOR SHOOKS	Jag	3.25	.T.T.	7	251.4	2.494	1.248	CT	1.308	0.19	70.20	83.7	19.1	1990	MA018
AGED AT 900P FOR 5 HOURS	Bar	3.26	R.T.	R-L	246.5	2.499	1.254	cr	1.304	0.19	67.30			1990	MA018
AGED AT 925F FOR 5 HOURS	Bar	3.26	R.T.	R-L	242.6	2.549	1.246	c1	1.354	0.35	90.60		:	1990	MA018
REAGED AT 925F FOR 10 HOURS	Forging	6.50	R.T.	T.L	246.3	2.501	1.254	cr	1.296	0.78	137.40		:	1990	MA018
REAGED AT 925F FOR 10 HOURS	Bar	3.25	R.T.	r.	239.7	2.529	1.313	CT	1.384	0.37	92.00		1	1990	MA018
REAGED AT 925F FOR 7.5 HOURS	Bar	3.25	R.T.	R.L	249.7	2.503	1.260	CT	1.292	0.22	73.90		:	1990	MA018

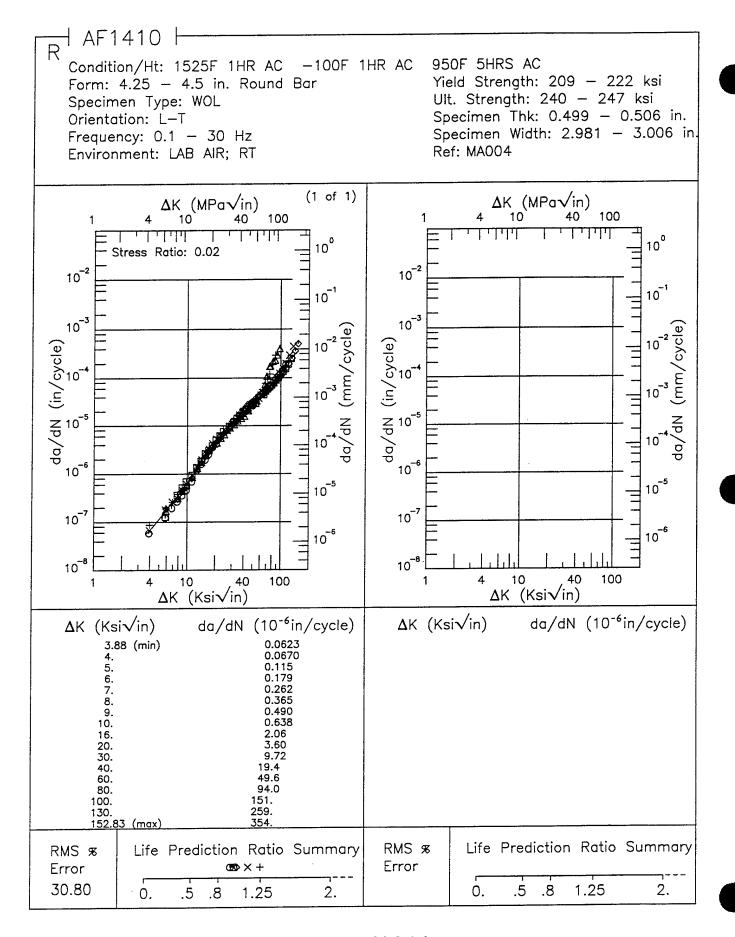


Figure 3.28.3.1.1

Yield Strength: 211 - 221 ksi Form: 4.25 - 4.5 in. Round Bar Specimen Type: WOL Ult. Strength: 243 - 249 ksi Orientation: T-L Specimen Thk: 0.498 - 0.506 in. Frequency: 0.1 - 30 Hz Specimen Width: 2.979 - 2.995 in. Environment: LAB AIR; RT Ref: MA004 (1 of 1) Δ K (MPa \sqrt{in}) ΔK (MPa√in) 10 40 100 10 40 100 1 1 1 1 1 1 1 1 10° 10° Stress Ratio: 0.02 10-2 10-2 10-1 10 -1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10⁻⁶ 10⁻⁵ 10⁻⁵ 10⁻⁷ 10⁻⁷ 10⁻⁶ 10 6 10 8 10 8 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) **Δ**K (Ksi√in) Δ K (Ksi \sqrt{in}) da/dN ($10^{-6}in/cycle$) 3.92 (min) 0.0583 4. 5. 6. 7. 8. 9. 0.0617 0.185 10. 16. 20. 30. 40. 60. 80. 98.9 100. 130. 135.83 (max) Life Prediction Ratio Summary RMS % RMS % Life Prediction Ratio Summary Error Error 40.12 0. .5 1.25 1.25 .8 2. 0. .5 8. 2.

-100F 1HR AC

950F 5HRS AC

Condition/Ht: 1525F 1HR AC

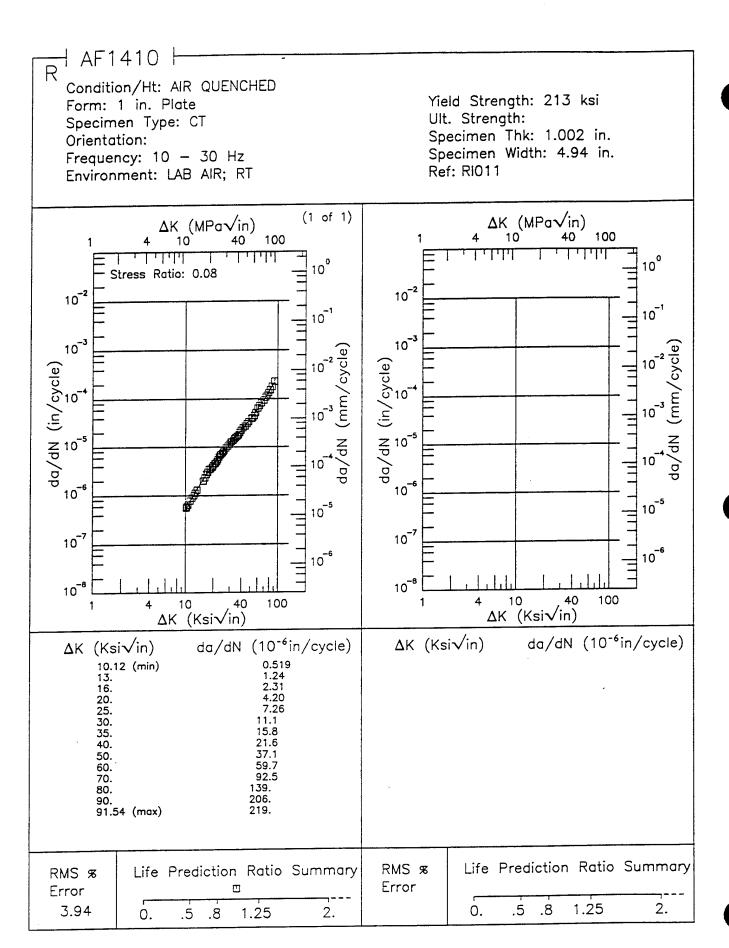


Figure 3.28.3.1.3

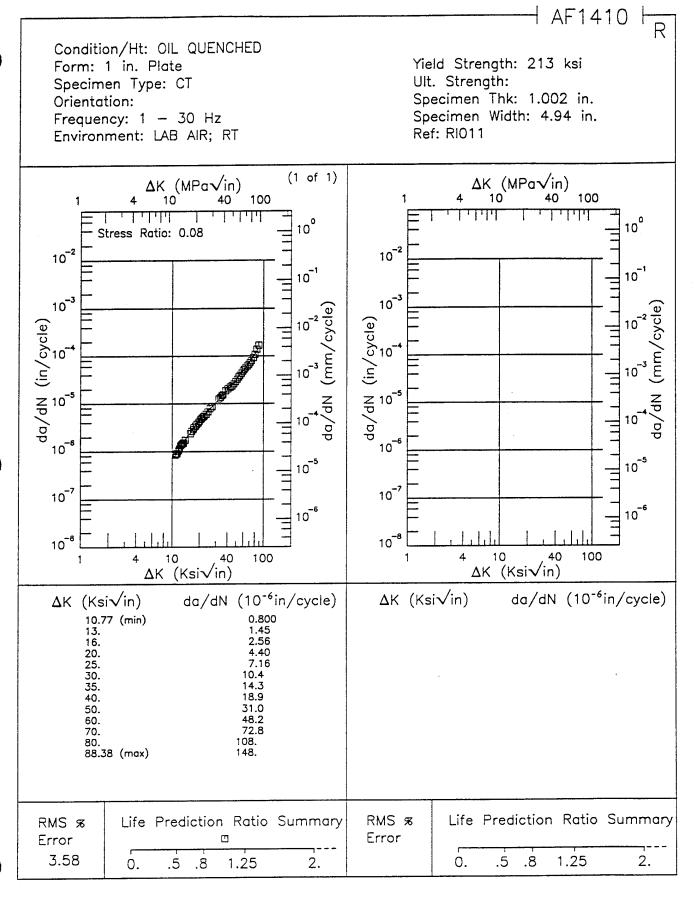


Figure 3.28.3.1.4

TABLE 3.29.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK AF1410(VIM-VAR) AT ROOM TEMPERATURE

		ANTE	THE THEORY INTERIOR PARTY	: Lab Air		
CONDITION/ HEAT TREATMENT FORM	icr f	FREQ (Hz)	PCC AA AB 80	FCGR (10 d in/cycle) AK Level (Kst/in)	000	\$ 1
1650F 1HR WQ 1500F 1HR WQ 950F 5HRS AC	0.08	30		0.65 3.88	27.26	

TABLE 3.29.1.2.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK AF1410(VIM-VAR) AT ROOM TEMPERATURE

ENVIRONMENT: S.T.W.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.08 1-30 6.63	0.08 1-30 6.53
ION: L-T	PRODUCT	RS Dr Ames	Librit
ORIENTATION: I	CONDITION/ HEAT TREATMENT	1650F 1HR WQ 1500F 1HR WQ 950F 5HRS	AC

TABLE 3.29.1.2.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK AF1410(VIM-VAR) AT ROOM TEMPERATURE

ORIENTATION: T-L

ENVIRONMENT: 3.5% NaCl

		100.0				
(ep	(a	50.0	29.51	29.51	39.21	39.21
⁶ in/cm	l (Ksk/i	20.0	4.97	4.97	80.9	6.08
FCGR (10 ⁻⁶ in/cycle)	AK Lovel (Keivin)	10.0				
FC	77	5.0				
		2.5				
	FREQ.		1-30	1-30	1-30	1-30
	æ		80.0	80.0	0.3	0.3
	PRODUCT FORM			- I		
	CONDITION HEAT TREATMENT			1650F 1HR WQ 1500F 1HR WQ 950F 5HRS	AC	

TABLE 3.29.1.2.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK AF1410(VIM-VAR) AT ROOM TEMPERATURE

ORIENTATION: T-L

ENVIRONMENT: Lab Air

		100.0				
(ejp	n)	60.0	29.34	29.34	36.14	36.14
in/cyt	ľ (Ksiv'i	20.0	3.95	3.95	5.35	5.35
PCGR (10 ^d in/cycle)	AK Lovel (Ket/in)	10.0	0.71	0.71	1.11	1.11
MC	Δ.	8.0				
		2.5				
Caga	(Hz)		1-30	1-30	10-30	10-30
	æ		90.0	90.0	0.3	0.3
DBODIEST	FORM			DI AMB	aiuni	
CONDITION	HEAT TREATMENT			1660F 1HR WQ 1500F 1HR WQ 950F 5HRS	AC	

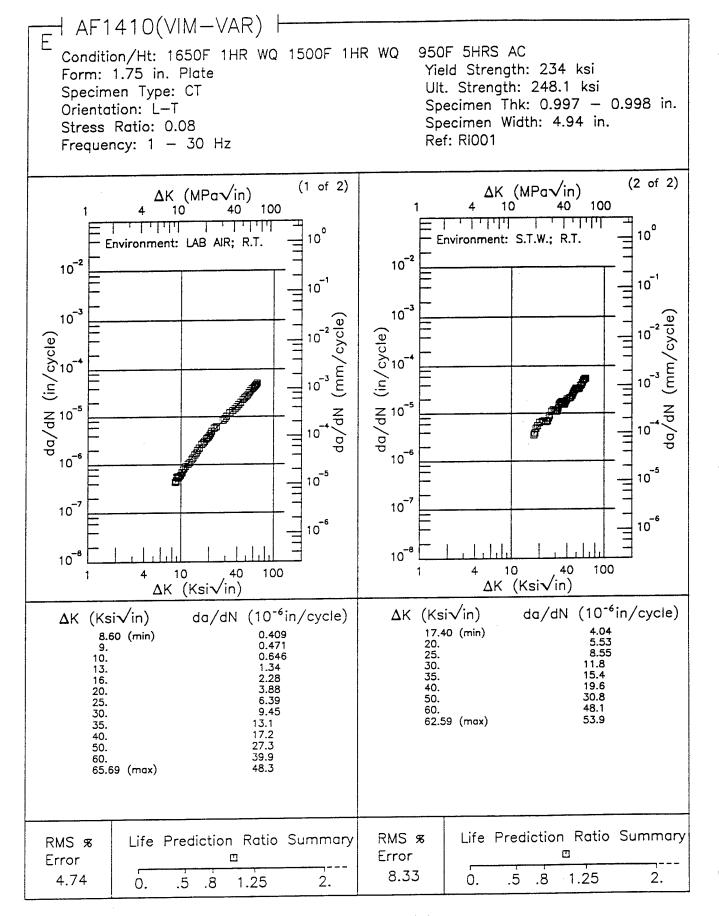


Figure 3.29.3.1.1

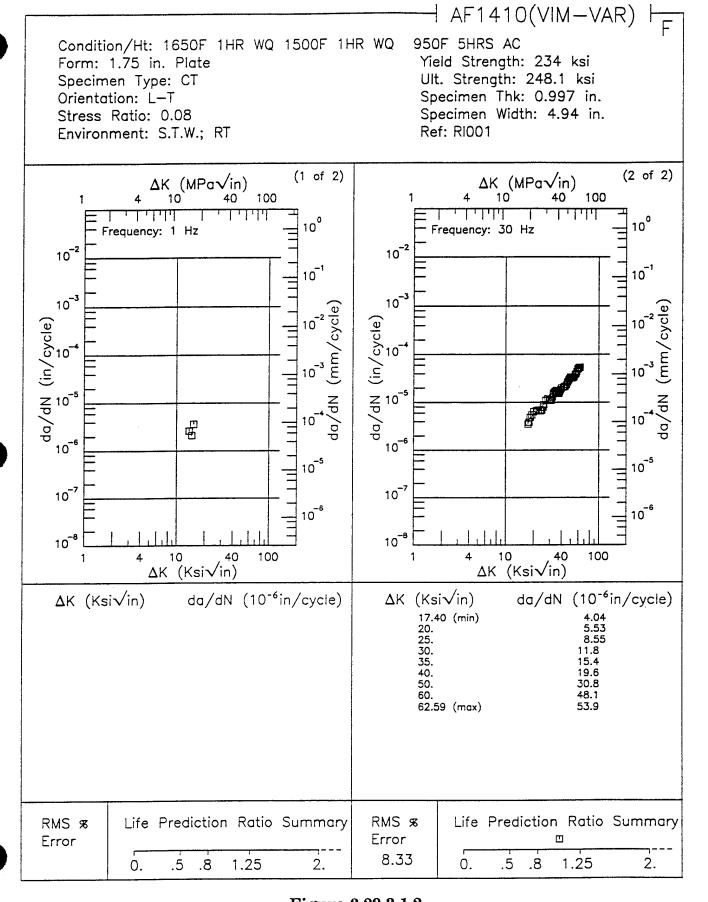


Figure 3.29.3.1.2

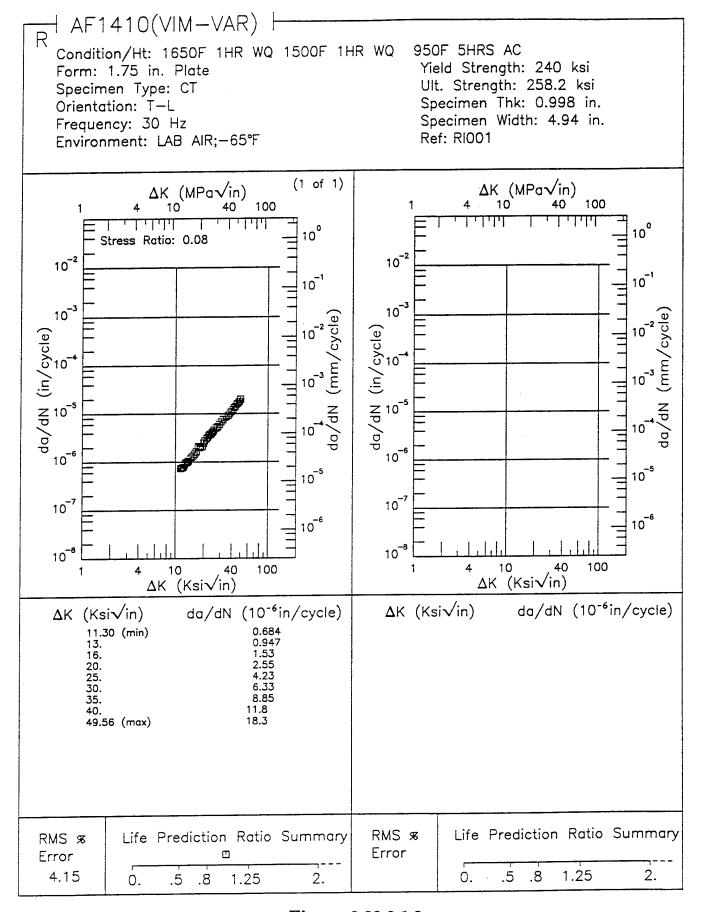


Figure 3.29.3.1.3

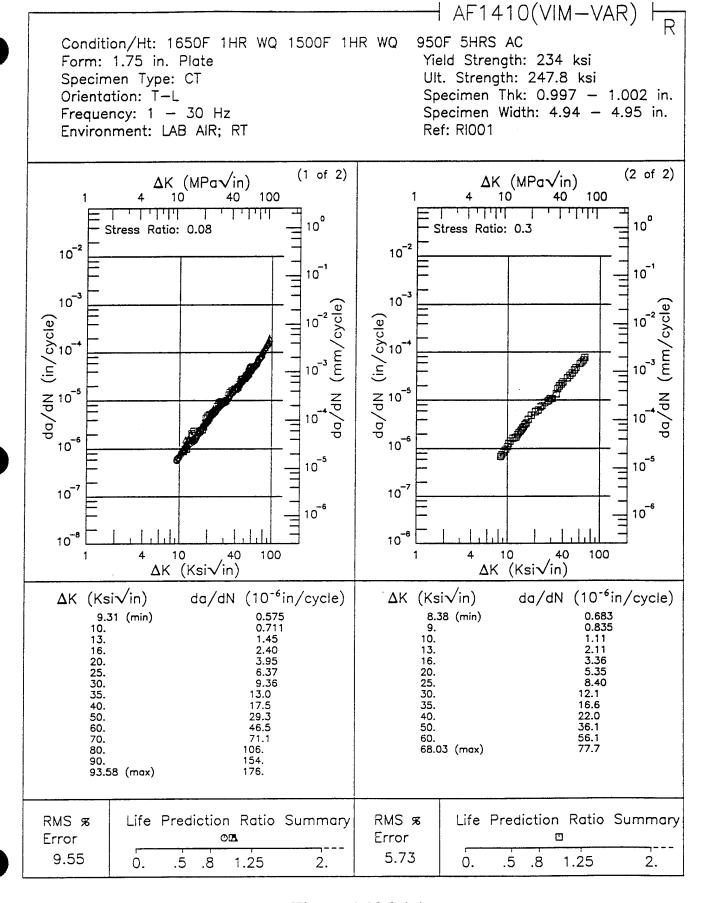


Figure 3.29.3.1.4

+ AF1410(VIM-VAR) Condition/Ht: 1650F 1HR WQ 1500F 1HR WQ 950F 5HRS AC Yield Strength: 234 ksi Form: 1.75 in. Plate Ult. Strength: 247.8 ksi Specimen Type: CT Specimen Thk: 0.998 - 1.001 in. Orientation: T-L Specimen Width: 4.94 in. Frequency: 1 - 30 Hz Environment: 3.5% NACL; RT Ref: RI001 (2 of 2) (1 of 2)ΔK (MPa√in) $\Delta K (MPa\sqrt{in})$ 10 100 100 10 40 10° 10° Stress Ratio: 0.08 Stress Ratio: 0.3 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) 10-2 da/dN (in/cycle) 10 10⁻⁶ 10-6 10 -5 10 -5 10⁻⁷ 10⁻⁷ 10 6 10 -6 10-8 10⁻⁸ 100 10 40 100 10 40 ΔK (Ksi√in) ΔK (Ksi√in) $da/dN (10^{-6}in/cycle)$ da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) ΔK (Ksi√in) 15.28 (min) 16. 19.33 (min) 5.79 6.08 20. 25. 30. 35. 40. 20. 25. 30. 18.5 10.5 35. 29.5 47.1 56.41 (max) 50. 70.51 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % 0 🗉 Error Error 12.77 2. 16.30 1.25 .5 0. .5 .8 1.25 2. .8

Figure 3.29.3.1.5

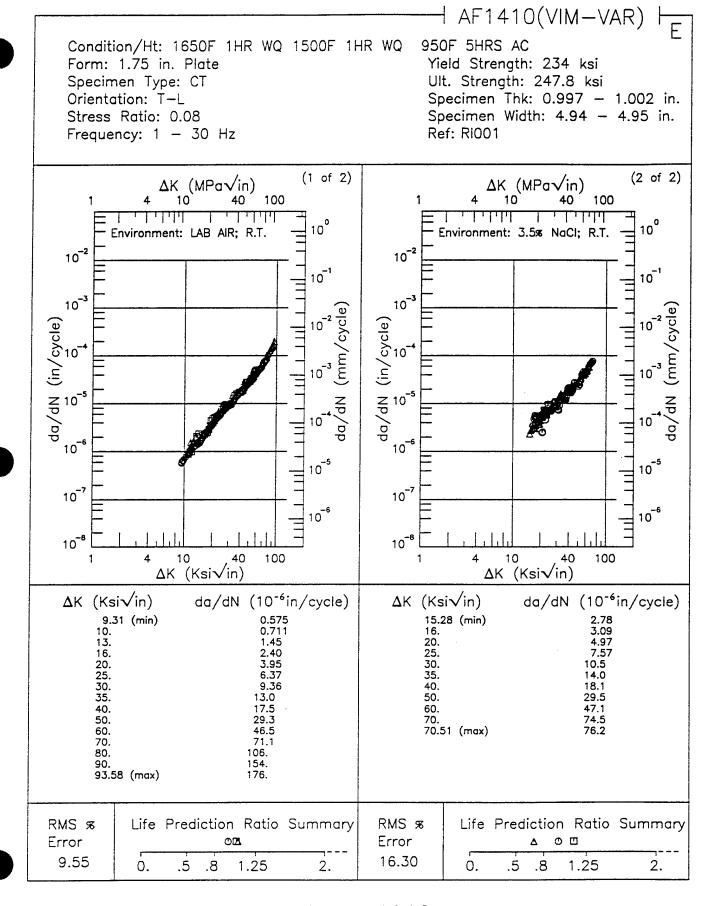


Figure 3.29.3.1.6

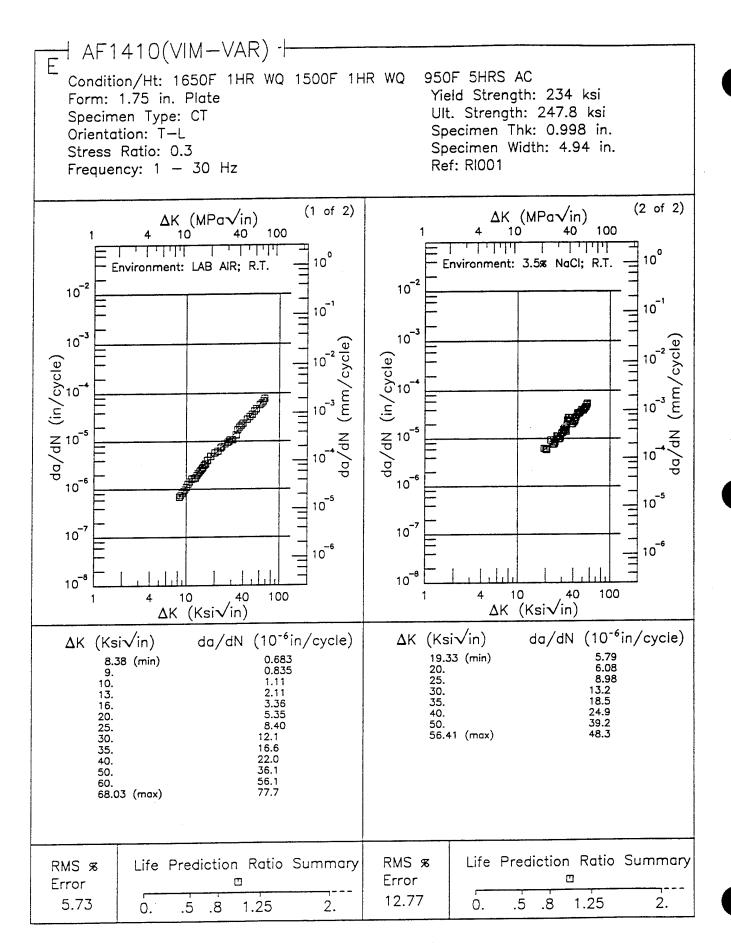


Figure 3.29.3.1.7

TABLE 3.30.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL D6AC AT ROOM TEMPERATURE

,	•				K_{L_0}	$K_{I_c}~(ksiar{in})$	<u>a</u>)			
Form	Condition/Heat Treatment				pecime	Specimen Orientation	itation			
			L-T			T-T			S-L	
		Mean K _{ie}	Std Dev	u	Mean K _{le}	Std Dev	ď	Mean K _{ie}	Std Dev	u
	1650F AUS-BAY QUENCH 976F SQ 1000F 2+2HR	6.99	18.7	7		i	:		:	:
	1650F AUS-BAY QUENCH 975F SQ 325F 1000F 2+2HR	62.2	14.	19	:	•••	i	ł	i	i
Plate	1650F AUS-BAY QUENCH 975F SQ 400F 1000F 2+2HR	64.4	12.1	103	•••	i	ŀ	ŀ	:	i
	1700F AUS-BAY QUENCH 975F OQ 140F 1000F 2+2HR	92.	8.2	30	:	ı		ŀ	i	i
	HEAT TREATED TO 46 RC HARDNESS	:	:		85.8	1.8	2	***		:
	1615F 2.25HR A-BQ 325F AC 310-345F 3HR 1080F 6-6.5HR	i e e	:	:	78.4	15.1	9	6.88	14.8	52
Forging	1650F AUS-BAY QUENCH 975F SQ 375F 1000F 2+2HR	46.	4.2	8	;	:	:	1	i	i
	1650F AUS-BAY QUENCH 975F SQ 400F 1000F 2+2HR	66.2	12.3	53	:	•••	-	:	;	ı

TABLE 3.30.1.1 (CONCLUDED)

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL D6AC AT ROOM TEMPERATURE

					K_{Ic}	$K_{Ic}~(ksi\sqrt{in})$	<u>(c</u>			
Foduct Form	Condition/Heat Treatment			S	pecime	Specimen Orientation	itation			
			L-T			T-L			S-L	
		Mean K _{te}	Std Dev	u	Mean K _{le}	Std Dev	п	Mean K _{to}	Std Dev	u
Forging (Cont'd)	1700F AUS-BAY QUENCH 975F OQ 140F 1000F 2+2HR	95.2	6.4	34		•	:	:	:	
	1650F 1HR FC 1650F 1HR OQ 1025F 2+2HR	78.5	4.7	2		:	:		•	•
	1650F 1HR FC TO 960F OQ AT 150F AC 1000F 2+2HR	80.3	0.8	2	-	-	i		-	:
	1700F 1HR FC TO 960F OQ AT 150F AC 1000F 2+2HR	80.3	4.3	3	-	•••	•		:	
	1700F 1HR OC 1025F 2+2HR	77.3	2.6	9	i		÷	:	i	:
Billet	1726F 1HR AC 1700F 1HR OQ 1000F 1HR 1016F 1HR	77.2	2.7	3	ì	:	***	1	:	ł
	1725F 1HR AC 1700F 1HR OQ 1026F 2+2HR	74.4	6.2	9	:	***	-	•		•
	1725F 1HR AC 1700F 1HR OQ 1100F 2+2HR	101.2	6.1	9	:	i	i	i	i	1
	1725F 1HR AC 1750F 1HR FC TO 960F SQ 350F 0.5HR AC 1025F 22HR	75.1	10.1	ಣ _.	:		1	ŀ	;	ŀ

TABLE 3.30.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK D6AC AT ROOM TEMPERATURE

ORIENTATION: L-T

ENVIRONMENT: Distilled Water

rele)	(17,	50.0 100.0										
^в ш/сэ	I (Ksiv)	0.88	11.48	25.41	10.68	5.88	12.23	8.56	15.73	9.61	89.9	11.44
FCGR (10 ⁻⁸ in/cycle)	ΔK Løvel (Ksiγin)	10.0	1.02				2.33	1.43				
FC	Ψ.	0.8										
		8.9										
FREG	(Hz)		1	0.1	1	3	1	3	0.1	1	က	
ı	¥		0.1	0.11	0.11	0.11	0.5	0.5	0.1	0.1	0.1	0.48
PRODUCT	FORM		FORGING			PLATE				Since	Chaine	
CONDITION	HEAT TREATMENT		1650F A-BQ AT 975F SQ AT 375F 1000F 2+2HR					1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS				

TABLE 3.30.1.2.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK D6AC AT ROOM TEMPERATURE

ORIENTATION: L-T

ENVIRONMENT: Dry Air

FCGR (10" INCOME)	(Hz) $\Delta K Level (Ksiv/in)$	2.5 5.0 10.0 20.0	0.1 5.58	1 5.24	3 5.43	0.1 5.28	1 5.66	3 4.86
	# H		60.0	60.0	60:0	0.1	0.1	0.1
PRODUKT	FORM			PLATE			PLATE	
CONDITION	HEAT TREATMENT			1650F A-BQ AT 975F SQ AT 400F 1000F 2+2HR			1700F A-BQ AT 97EF OQ AT 140F 1000F 2+2HRS	

TABLE 3.30.1.2.3

 $\Delta \mathbf{K}$

FATIGUE CRACK GROWTH	VTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK D6AC AT ROOM TEMPERATURE	FINED LOOM TE	EVELS C MPERAT	F STRE URE	SS IN	TENS	ITY FA	CTOR	$\Delta \mathbf{K}$
ORIENTATION: L-T	4: L-T		ENV	ENVIRONMENT: JP-4 Jet Fuel	L:TNE	P-4 J	et Fuel		
CONDITTION	PRODICT		CHAR		FCG	4R (10	FCGR (10 ^d in/cycle)	<i>(6)</i>	
HEAT TREATMENT	FORM	Ħ	(HZ)		ΔK	Lovel	AK Level (Ksk/in)	1)	
				2.5	8.0	001	20.0	50.0	100.0
1650F A-BQ AT 975F SQ AT 375F 1000F 2+2HR	FORGING	0.1	1			0.65			
		0.1	0.1				10.42		
		0.1	1				7.44		
1650F A-BQ AT 975F SQ AT 400F 1000F	PLATE	0.1	3			0.74	5.31		
2+2HR		0.5	1			2.41	9.62		
		0.5	3			1.09	6.45		
	FORGING	0.6	1				9		
	210 4 112	0.5	1				8.95		
	FLAIB	0.5	3				6.73		
1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS		0.1	0.1				14.82	87.62	
	FORGING	0.1	1				8.37	37.44	
		0.1	က				3.73	39.44	

TABLE 3.30.1.2.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK

20.0 51.35 65.2 FCGR (10 ⁶ in/cycle) ΔK Level (Keiγin) 98 2.86 9.29 5.61 **ENVIRONMENT: Lab Air** 10.0 6.0 D6AC AT ROOM TEMPERATURE 10 64 FREQ (Hz) 0.1 = 0.1 0.1 0.5 0.1 PRODUCT FORM PLATE PLATE ORIENTATION: L-T 1650F A-BQ AT 975F SQ AT 400F 1000F 2+2HR 1700F A-BQ AT 97FF OQ AT 140F 1000F 2+2HRS HEAT TREATMENT CONDITION

0.001

TABLE 3.30.2.1

					AL	ALLOY STEEL	L D6AC	y K _{ta}								
	PRODUCT	oucr				3	SPECIMEN	7	CRACK			Kı				ī -
CONDITION	FORM	THICK (in.)	TERT TEMP (°F)	SPEC	YIELD STR (Kei)	WIDTH (in.)	THICK (in.)	DESIGN	LENGTH (in.) A	(K _{k,} /TYS)* (in.)	K. (Kei • (in.)	K. MEAN	BTAN	DATE	REFER	
		ŀ			197.9	2.000	1.006	CT	1.046	0.28	67.37			1979	MD001	
1616F 2.25HR A-BQ 325F AC 310-345F 3HR 1080F 6-6.5HR	Forging	ï	R.T.	8-31	198.0	2.000	1.001	CT	1.061	0.29	68.26	64.7	5.5	1979	MD001	
					199.8	1.997	1.001	CT	1.041	0.21	58.33			1980	MD001	
		1			198.1	2.001	1.005	cr	1.048	0.33	72.62			1979	MD001	
		i			198.1	2.000	1.005	CT	1.072	0.55	93.00			1979	MD001	
1615F 2.25HR A-BQ 325F AC		ı	5		198.5	2.000	1.005	CT	1.069	0.55	93.67			1979	MD001	
310-346F 3HR 1080F 6-6.5HR	Forging	1	H H	<u></u>	198.5	2.000	1.001	CT	1.060	0.49	87.89	78.4	16.1	1979	MD001	
		ı			207.5	1.998	1.002	cr	1.024	0.20	59.04			1980	MD001	
		:			207.5	1.997	1.000	CT	1.035	0.23	64.27			1980	MD001	
		:			186.7	2.000	1.005	CT	1.045	0.55	88.32			1978	MD001	
		1			186.7	2.000	1.005	CT	1.030	0.36	71.78			1978	MD001	
		ï			186.7	1.999	1.005	CT	1.042	0.71	99.54			1978	MD001	
		i			187.2	1.990	1.002	СT	1.021	0.76	103.25			1978	MD001	
		;		,	187.2	1.989	0.996	CT	1.003	0.81	106.64			1978	MD001	
1616F 2.25HR A-BQ 325F AC		:	Ē		187.2	1.987	0.996	CT	1.040	0.76	103.67			1979	MD001	
310-345F 3HR 1080F 6-6.5HR	Forging	:	K.T.		189.5	1.992	0.994	ст	1.016	0.63	95.25	83.9	14.8	1978	MD001	
		ï			189.6	1.997	0.993	CT	1.033	0.31	67.12			1978	MD001	
		:			189.6	1.996	1.003	CT	1.024	0.35	71.23			1978	MD001	
		ı			189.5	1.996	0.995	CŢ	1.034	0.61	93.78			1978	MD001	7
		:			189.5	1.994	0.994	CT	1.023	0.63	95.37			1978	MD001	
		•			189.5	1.993	0.994	CT	1.012	0.34	70,02			1978	MD001	

	PRODUCT	oucr				S	SPECIMEN	7	CRACK	i d		K _{lo}			
CONDITION	FORM	THICK (in.)	TEMP (°F)	SPEC	YTELD STR (Kei)	WIDTH (in.)	THICK (fn.) B	DESIGN	LENGTH (in.) A	(K.,TYS)* (in.)	K. (Kei * √in.)	K. MEAN	BTAN	DATE	REFER
		:			191.0	2.002	0.991	CT	1.027	0.46	82.63			1979	MD001
		"		1	191.0	1.995	0.992	CT	1.021	0.45	81.67			1979	MD001
		i			191.0	2.001	0.990	CT	1.028	0.37	73.64			1979	MD001
		ı			191.9	1.994	1.002	CT	1.035	0.50	86.37			1978	MD001
		ł			191.9	1.996	1.003	cr	1.043	0.54	89.64			1978	MD001
		i			191.9	1.988	1.003	cr	1.033	0.67	92.34			1978	MD001
		ŀ	•		192.8	2.004	0.991	CT	1.015	0.18	53.02			1979	MD001
		ŧ		L	192.8	2.000	0.991	cr	1.019	0.17	51.11			1979	MD001
		i			192.8	2.000	0.991	J.	1.037	0.16	48.96			1979	MD001
		ı			193.0	2.000	1.000	C.	1.044	0.34	71.92			1979	MD001
1616F 2.26HR A-BQ 326F AC	Forging	;	R.T.	18	193.0	1.999	0.965	£	1.023	0.54	89.71			1979	MD001
	Cont'd	!	Cont'd	Cont'd	193.8	1.998	1.000	CI	1.031	0.27	64.19	Cont'd	Contd	1978	MD001
		ı	-		193.8	2.000	1.001	CT	1.049	0.31	69.12			1977	MD001
					193.8	2.000	0.992	ţ	1.024	0.30	68.14			1977	MD001
		i			194.1	2.001	0.997	CT	1.036	0.61	96.00			1980	MD001
		:			194.1	1.999	0.999	CT	1.076	0.41	78.90			1980	MD001
		ı			194.1	1.999	966.0	CT	1.037	0.47	84.17			1980	MD001
		ı			194.4	1.998	1.000	СŢ	1.026	0.43	80.69			1978	MD001
		ı			194.5	2.000	1.004	CT	1.050	0.55	91.67			1977	MD001
		:			194.6	2.000	1.004	cr	1.062	0.55	91.59			1977	MD001
		·			195.5	1.999	1.002	CT	1.067	0.30	68.54			1979	MD001
		ı			195.5	2.000	1.004	CT	1.025	0.29	67.40			1979	MD001

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					AL	ALLOY STEEL	L D&AC	J. K.							
	PRO	PRODUCT				u 2	SPECIMEN	7	CRACK	•		K _{Io}			
CONDITION	FORM	THICK (In.)	TEMP (°F.)	SPEC	YTELD STR (Kel)	WIDTH (fn.) W	THICK (in.)	DEBIGN	LENGTH (in.) A	(KTYS)* (in.)	K. (Kei • √(n.)	K. MEAN	STAN	DATE	REFER
				1	196.3	1.999	1.003	CT	1.057	0.45	83.50			1979	MD001
		1			196.3	2.001	1.000	CT	1.058	0.60	96.67			1977	MD001
		ı	•	L	196.3	1.998	1.000	CT	1.045	0.36	75.10			1978	MD001
		:			196.3	2.000	1.005	cr	1.040	0.55	92.69			1979	MD001
		1		1	196.9	1.999	1.002	CT	1.011	0.65	101.04			1978	MD001
		:		1	196.9	1,999	1.002	CT	1.017	0.67	102.31			1979	MD001
		ŀ		!	196.9	1.999	1.002	cr	1.034	0.63	99.31			1978	MD001
		:			200.2	1.999	1.007	CT	1.014	0.38	78.63			1978	MD001
1615F 2.25HR A-BQ 325F AC	Forging	ı	R.T.	1 7-8	200.2	1.999	1.007	CT	1.025	0.35	75.67			1978	MD001
Cont'd	Cont'd	ı	Cont'd	Cont'd	200.2	1.999	1.007	CT	1.027	0.35	75.91	Cont'd	Cont'd	1978	MD001
		1			201.5	1.997	1.000	CT	1.036	0.65	103.09			8/61	MD001
		i		I	201.5	1.997	0.999	СТ	1.062	09:0	99.19			1978	MD001
		i			201.6	1.997	0.999	CT	1.037	0.67	104.62			1978	MD001
		1			202.3	2.003	1.000	cr	1.038	0.55	95.21			1977	MD001
			•	1	202.3	2.000	1.000	CT	1.042	0.56	95.80			1877	MD001
		:		I	202.3	2.001	0.999	СT	1.042	0.55	95.58			1977	MD001
		·			202.7	2.000	1.002	CT	1.037	0.32	73.46			1980	MD001
		:			202.7	1.995	1.00.1	CT	1.037	0.25	65.34			1980	MD001
		1.50			228.0	1.501	0.750	CT	0.790	0.05	31.20			1972	82543
1650F AUS-BAY QUENCH 975F SQ	Ē	0.80	ţ	i	228.0	1.502	0.757	CT	0.759	0.11	47.00			1972	82543
325F 1000F 2+2HR	riate	1.50	ę	<u> </u>	228.0	1.499	0.750	СŢ	0.760	0.06	35.80	37.0	6.9	1972	82643
		1.50			228.0	1.499	0.750	CT	0.854	0.05	34.10			1972	82543

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WIDTH WIDTH WIDTH THICK (In.) PB SIGN PB SIGN
THICK (In.) DESIGN (In.) (In.)
0.750 CT 0.771 0.06 8 0.750 CT 0.781 0.06 8 0.750 CT 0.777 0.07 8 0.757 CT 0.769 0.15 6 0.750 CT 0.784 0.16 7 0.750 CT 0.784 0.06 3 0.750 CT 0.784 0.08 3 0.750 CT 0.784 0.06 3 0.750 CT 0.784 0.06 3 0.750 CT 0.789 0.10 3 0.750 CT 0.789 0.10 3 0.750 CT 0.789 0.10 3 0.750 CT 0.787 0.08 3 0.750 CT 0.787 0.13 3 0.748 CT 0.789 0.11 3 0.750 CT 0.769 0.36 3 0.750 </td
0.760 CT 0.781 0.06 3 0.750 CT 0.777 0.07 5 0.757 CT 0.769 0.15 6 0.757 CT 0.765 0.16 6 0.750 CT 0.784 0.06 5 0.750 CT 0.784 0.06 5 0.750 CT 0.789 0.10 6 0.750 CT 0.789 0.10 6 0.750 CT 0.780 0.06 6 0.750 CT 0.789 0.10 6 0.750 CT 0.780 0.06 6 0.750 CT 0.787 0.13 6 0.740 CT 0.777 0.08 6 0.750 CT 0.769 0.36 6 0.760 CT 0.769 0.36 6 0.760 CT 0.769 0.36 6 0.760 </td
0.750 CT 0.777 0.07 0.757 CT 0.765 0.15 F 0.750 CT 0.765 0.15 F 0.750 CT 0.811 0.06 F 0.750 CT 0.784 0.06 F 0.750 CT 0.784 0.08 F 0.750 CT 0.789 0.10 F 0.750 CT 0.780 0.06 F 0.750 CT 0.777 0.08 F 0.760 CT 0.777 0.01 F 0.760 CT 0.769 0.36 F 0.760 CT 0.769 0.36 C 0.760 CT<
0.767 CT 0.769 0.16 0 0.779 CT 0.765 0.16 0 0.750 CT 0.811 0.06 3 0.750 CT 0.784 0.06 3 0.750 CT 0.789 0.10 3 0.750 CT 0.789 0.10 3 0.750 CT 0.780 0.06 3 0.750 CT 0.780 0.06 3 0.750 CT 0.787 0.08 3 0.750 CT 0.787 0.13 3 0.746 CT 0.787 0.13 3 0.746 CT 0.787 0.11 3 0.750 CT 0.769 0.36 3 0.750 CT 0.769 0.36 3 0.750 CT 0.769 0.36 3 0.750 CT 0.779 0.36 3 0.750 </td
0.767 CT 0.765 0.16 0.749 CT 0.811 0.06 0.750 CT 0.784 0.06 0.750 CT 0.784 0.08 0.750 CT 0.784 0.10 0.750 CT 0.789 0.10 0.750 CT 0.789 0.10 0.750 CT 0.789 0.08 0.751 CT 0.780 0.08 0.750 CT 0.777 0.08 0.748 CT 0.711 0.11 0.750 CT 0.769 0.36 0.750 CT 0.777 0.08 0.750 CT 0.769 0.36 0.750 CT 0.769 0.36 0.750 CT 0.777 0.11
0.749 CT 0.811 0.06 0.750 CT 0.786 0.06 0.750 CT 0.817 0.08 0.750 CT 0.784 0.08 0.750 CT 0.789 0.10 0.750 CT 0.780 0.06 0.750 CT 0.780 0.06 0.750 CT 0.787 0.13 0.740 CT 0.777 0.08 0.740 CT 0.717 0.08 0.750 CT 0.769 0.36 0.750 CT 0.769 0.36 0.750 CT 0.769 0.36 0.750 CT 0.769 0.36 0.750 CT 0.777 0.11
0.750 CT 0.786 0.06 0.750 CT 0.817 0.08 0.750 CT 0.784 0.08 0.750 CT 0.789 0.10 0.750 CT 0.789 0.10 0.750 CT 0.837 0.08 0.751 CT 0.780 0.06 0.750 CT 0.787 0.13 0.750 CT 0.777 0.08 0.750 CT 0.717 0.08 0.750 CT 0.719 0.36 0.750 CT 0.769 0.36 0.750 CT 0.777 0.11
0.750 CT 0.817 0.08 0.750 CT 0.784 0.08 0.750 CT 0.789 0.10 0.750 CT 0.789 0.10 0.750 CT 0.837 0.08 0.751 CT 0.787 0.08 0.750 CT 0.777 0.08 0.748 CT 0.717 0.08 0.750 CT 0.717 0.08 0.750 CT 0.769 0.35 0.750 CT 0.779 0.36
0.750 CT 0.784 0.08 0.750 CT 0.789 0.10 0.750 CT 0.789 0.10 0.750 CT 0.837 0.08 0.750 CT 0.780 0.06 0.751 CT 0.787 0.13 0.750 CT 0.777 0.08 0.750 CT 0.717 0.36 0.750 CT 0.769 0.36 0.756 CT 0.777 0.11
0.760 CT 0.789 0.10 0.750 CT 0.768 0.10 0.750 CT 0.837 0.08 0.751 CT 0.787 0.06 0.750 CT 0.777 0.08 0.748 CT 0.815 0.11 0.750 CT 0.769 0.36 0.756 CT 0.777 0.08 0.756 CT 0.777 0.36 0.756 CT 0.777 0.11
0.750 CT 0.768 0.10 0.750 CT 0.837 0.08 0.750 CT 0.780 0.06 0.751 CT 0.787 0.13 0.750 CT 0.777 0.08 0.760 CT 0.815 0.11 0.766 CT 0.769 0.36 0.766 CT 0.777 0.11
0.750 CT 0.837 0.08 0.750 CT 0.780 0.06 0.751 CT 0.787 0.13 0.750 CT 0.777 0.08 0.760 CT 0.815 0.11 0.760 CT 0.769 0.36 0.766 CT 0.777 0.11
0.750 CT 0.780 0.06 0.751 CT 0.787 0.13 0.750 CT 0.777 0.08 0.750 CT 0.815 0.11 0.750 CT 0.769 0.36 0.766 CT 0.777 0.11
0.751 CT 0.787 0.13 0.750 CT 0.777 0.08 0.748 CT 0.815 0.11 0.750 CT 0.769 0.36 0.756 CT 0.777 0.11
0.750 CT 0.777 0.08 0.748 CT 0.815 0.11 0.750 CT 0.769 0.36 0.766 CT 0.777 0.11
0.748 CT 0.815 0.11 0.750 CT 0.769 0.36 0.756 CT 0.777 0.11
0.750 CT 0.769 0.36 0.756 CT 0.777 0.11
0.756 CT 0.777 0.11
1.498 0.755 CT 0.790 0.13 48.70
1.504 0.767 CT 0.767 0.35 81.00
1.502 0.757 CT 0.750 0.34 80.10
1,602 0.765 CT 0.765 0.37 88.60
1,501 0.755 CT 0.815 0.12 46.50

		1			AL	ALLOY STEEL	SL D&AC	C IK,							
	PRODUCT	UCT					SPECIMEN	7.	CRACK			K _{Io}			
CONDITION	FORM	THICK (In.)	TEST TEMP (°F)	SPEC	YIELD STR (Kal)	WIDTH (fn.)	THICK (in.) B	DESIGN	LENGTH (in.) A	(K _w /TYS)* (in.)	K. (iii)	K. MRAN	BTAN	DATE	REFER
		1.50		l	211.0	1.498	0.750	CT	0.763	08'0	72.50			1972	82543
1650F AUS-BAY QUENCH 975F SQ 325F 1000F 2+2HR	Plate	1.50	175	5	211.0	1.502	0.750	CT	0.823	0.32	75.40	74.7	0.0	1972	82543
		1.50			211.0	1.499	0.750	CT	0.768	0.32	76.30		ì	1972	82543
	-	1.60		1	204.0	1.496	0.751	CT	0.763	0.61	100.80			1972	82543
1650F AUS-BAY QUENCH 975F SQ 325F 1000F 2+2HR	Plate	1.50	300	5	204.0	1.601	0.750	CT	0.798	0.67	105.40	104.2	3.0	1972	82543
		1.50			204.0	1.503	0.750	CT	0.772	99'0	106.40			1972	82543
1650F 1 HR PC 1650F 1HR OQ	1000	7.00	£	E	210.0	2.500	1.000	CT	1.400	0.32	75.10			1972	84277
1025F 2+2HR	Dillet	7.00	R. I.	3	210.0	2.500	1.000	CT	1.400	98'0	81.80	78.5	4.7	1972	84277
1650F 1 HR FC TO 960F OQ AT	100	7.00	E p	L	211.0	2.500	1.000	CT	1.400	0.37	80.90			1972	84277
150F AC 1000F 2+2HR	Dillet	7.00		5	211.0	2.500	1.000	ст	1.400	96'0	79.70	80.3	8.0	1972	84277
		1.50			219.0	1.000	0.500	CT	0.500	0.40	88.00			1972	84277
1650F 1 HR FC TO 960F OQ AT 180F AC 1025F 2+2HR	Forging	1.60	R.T.	:	219.0	1.000	0.500	cr	0.500	0.41	88.30	87.7	2.0	1972	84277
		1.50			219.0	1.000	0.500	CI	0.500	0.39	86.90			1972	84277
		1.50			217.0	1.202	0.608	cr	0.645	0.17	56.80			1972	82543
		1.50			217.0	1.199	0.599	cr	0.625	0.35	81.10			1972	82543
		1.50			217.0	1.199	0.608	CT	0.612	0.14	60.40			1972	82543
1660F AUS BAY QUENCH 975F SQ	5	1.50	Ē	E	217.0	1.201	0.602	CT	0.618	0.32	77.90			1972	82543
375F 1000F 2+2HR		1.50	; 4	<u> </u>	217.0	1.196	0.608	cr	0.642	0.09	40.20	62.2	14.0	1972	82543
		1.50			217.0	1.200	0.605	CT	0.619	0.12	47.40			1972	82543
		1.50			217.0	1.205	0.605	CT	0.641	0:30	75.10			1972	82543
		1.50			217.0	1.204	0.605	CT	0.648	0.21	62.60			1972	82543

					ALI	ALLOY STEEL	L D6AC	J. K.							
	PRODUCT	OUCT				S	SPECIMEN	,	CRACK			$\mathbf{K}_{\mathbf{I}^{\mathbf{c}}}$			
CONDITION	FORM	THICK (in.)	TEMP TEMP (°F)	SPEC OR	YIELD STR (Kel)	WIDTH (In.)	THICK (in.) B	DESIGN	LENGTH (ln.) A	(K.,TYS)*	K. (Roi •	K. MEAN	STAN DEV	DATE	REFER
		1.50			217.0	1.197	0.604	CT	0.644	0.28	72.20			1972	82543
		1.60			217.0	1.198	0.605	C.	0.636	0.18	67.80			1972	82543
		1.50	-		217.0	1.202	0.604	cr	0.641	0.31	76.50			1972	82543
		1.50			217.0	1.195	0.605	CT	0.621	0.26	69.40			1972	82543
		1.50			217.0	1.211	0.607	CT	0.632	0.14	50.40			1972	82643
1650F AUS-BAY QUENCH 975F SQ 375F 1000F 2+2HR	Plate Cont'd	1.50	R.T. Cont'd	L-T Cont'd	217.0	1.201	0.599	CT	0.618	0.12	48.00	Cont'd	Cont'd	1972	82543
Cont'd		1.60			217.0	1.203	0.608	CT	0.623	0.12	47.70			1972	82543
		1.50			217.0	1.204	0.607	CT	0.628	0.25	68.20			1972	82543
		1.50			217.0	1.193	0.604	cT	0.610	0.12	46.80			1972	82543
		1.50			217.0	1.200	0.605	cr	0.630	0.41	87.90			1972	82543
		1.50			217.0	1.201	0.600	cr	0.599	0.23	66.30			1972	82543
1650F AUS-BAY QUENCH 975F SQ		1.60	;		225.0	1.507	0.756	CT	0.773	90'0	31.80			1972	82543
375F 1000F 2+2HR	Forging	1.50	-65	7	225.0	1.507	0.756	cr	0.773	90:0	31.80	81.8	0.0	1972	82543
		1.50			222.0	1.506	0.755	CT	0.768	90:0	35.50			1972	82643
1650F AUS-BAY QUENCH 975F SQ 376F 1000F 2+2HR	Forging	1.50	-20	L.	222.0	1.504	0.753	CT	0.755	90.0	34.50	94.8	0.6	1972	82543
		1.50			222.0	1.506	0.755	CT	0.758	90:0	34.50			1972	82543
1650F AUS-BAY QUENCH 975F SQ 376F 1000F 2+2HR	Forging	1.50	0	LT	220.0	1.504	0.755	CT	0.791	90:0	34.60	i	1	1972	82543
		1.50			218.0	1.506	0.755	CT	0.782	0.08	39.00			1972	82543
1650F AUS-BAY QUENCH 976F SQ 376F 1000F 2+2HR	Forging	1.50	20	7.	218.0	1.506	0.756	CT	0.773	90:0	39.90	37.5	3.5	1972	82543
		1.50			218.0	1.503	0.751	ст	0.785	90:0	33.50			1972	82543

					AL	ALLOY STEEL	IL DBAC	C K,							
	PRODUCT	UCT					SPECIMEN	7.	CRACK			K _{Io}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (in.) W	THICK (in.) B	DESIGN	LENGTH (In.) A	(KTYS)* (in.)	K. (Kai •	K. MBAN	STAN	DATE	RBFER
		1.50			214.0	1.501	0.753	CT	0.771	0.13	48.40			1972	82543
		1.50			214.0	1.497	0.753	CT	0.762	0.16	54.40			1972	82543
		1.50		!	214.0	1.508	0.755	CT	0.766	0.11	45.10			1972	82543
1650F AUS-BAY QUENCH 976F SQ	, ,	1.50	E	! E	214.0	1.503	0.755	CT	0.794	0.11	44.70			1972	82543
375F 1000F 2+2HR	rorging	1.50	į	<u>.</u>	214.0	1.514	0.755	CT	0.764	0.12	46.10	46.0	4.2	1972	82543
		1.50			214.0	1.504	0.750	cr	0.783	0.10	42.40			1972	82543
		1.50		1	214.0	1.502	0.753	cr	0.767	60.0	40.30			1972	82543
		1.50			214.0	1.502	0.750	cr	0.768	0.12	46.80			1972	82543
		1.50		1	208.0	1.503	0.750	CT	0.775	0.33	75.60			1972	82543
1650F AUS-BAY QUENCH 975F SQ 375F 1000F 2+2HR	Forging	1.50	175	1	208.0	1.601	0.755	CT	0.780	0.19	57.30	64.1	10.0	1972	82543
		1.50			208.0	1.497	0.750	cr	0.773	0.20	69.40			1972	82543
1650F AUS-BAY QUENCH 975F SQ	ŗ	1.50	Ş	E	201.0	1.501	0.753	CT	0.762	0.51	90.50			1972	82543
376F 1000F 2+2HR	rorging	1.50	36	1.5	201.0	1.502	0.755	CT	0.779	0.54	93.40	92.0	2.1	1972	82543
		0.80			228.0	1.501	0.755	CI	0.743	0.04	30.40			1972	82543
		0.80			228.0	1.507	0.759	CT	0.758	0.07	37.30			1972	82543
1650F AUS-BAY QUENCH 975F SQ 400F 1000F 2+2HR	Plate	0.80	86	2	228.0	1.504	0.758	CT	0.763	90:0	31.80	33.2	2.8	1972	82543
		0.80			228.0	1.504	0.755	CT	0.763	90'0	31.90		:	1972	82543
		08.0			228.0	1.503	0.751	CT	0.748	90.0	34.70		,	1972	82543

FORDING TOWARD WATER LINES TASK (MAR)						AL	ALLOY STEEL	L D6AC	, K,							
Hailey Tight (19.1) Hailey Ti		PROI	oucr				42	PECIMEN	-	CRACK	•		$\mathbf{K}_{\mathbf{I}c}$			
Plate 0.00 Horizon 0.1450 0.176 0.776 0.00 0.07 0.00 0.07 0.00 0.07 0.00 0.07 0.00 0.07 0.00 0.07 0.00 0.07 0.00 0.07 0.00 0.07 0.00 0.07 0.00 0.07 0.00 0.07 0.00 0.07 0.00	CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (in.) W	THICK (in.) B	DESIGN	LENGTH (in.) A	(K _{a,} TY8)* (in.)	R. (Red · vin.)	K. MEAN	BTAN DRV	DATE	REFER
Harte Good Harte Land Land Gard Card			0.80			227.0	1.496	0.757	cT	0.760	0.07	38.50			1972	82543
Haife Good Good Good Good Good Good Good Goo			0.80			227.0	1.498	0.757	CT	0.758	0.07	37.60			1972	82543
Haie 0.80			0.80			227.0	1.502	0.693	C.	0.750	0.07	37.00			1972	82543
1972 1972	LBAY QUENCH 976F SQ 0F 1000F 2+2HR	Plate	08.0	-40	LT	227.0	1.499	0.758	cT	0.770	0.06	36.70	38.5	2.0	1972	82543
Hais been seed to so the source of the sourc			08.0			227.0	1.505	0.693	СТ	0.765	0.07	37.30			1972	82543
Plate 0.80 CR 0.00 G0.00 CT 0.00 4140 CR 1972 197			08.0			228.0	1.201	0.599	ст	0.624	90'0	41.20			1972	82543
Plate 0.80 -22 1,501 0.767 CT 0.746 0.08 99.10 40.3 1972 <			0.80			228.0	1.201	0.599	CT	909.0	90.0	41.40			2461	82543
Plate 0.80 -20 L-T 226.0 1.501 0.767 CT 0.764 0.09 42.30 40.30 42.30 40.80 42.30 40.80 <td></td> <td></td> <td>08.0</td> <td></td> <td></td> <td>226.0</td> <td>1.501</td> <td>0.757</td> <td>CT</td> <td>0.748</td> <td>90.0</td> <td>39.10</td> <td></td> <td></td> <td>1972</td> <td>82543</td>			08.0			226.0	1.501	0.757	CT	0.748	90.0	39.10			1972	82543
Hate 0.80			0.80			226.0	1.502	0.757	cr	0.754	0.09	42.30			1972	82543
0.80 4.080	1650F AUS-BAY QUENCH 976F SQ 400F 1000F 2+2HR	Plate	0.80	-50	L.T	226.0	1.501	0.757	CT	0.756	90:0	39.90	40.3	1.3	1972	82543
Hate 0.80			0.80			226.0	1.501	0.755	CT	0.756	0.08	40.80			1972	82543
Plate 0.80 0 LT 224.0 14.89 0.767 CT 0.776 0.06 44.50 42.4 42.4 22.4 1972 Plate 0.80 0 LT 224.0 14.86 0.767 CT 0.781 0.08 42.40 22.4 1872			080			226.0	1.498	0.757	ст	0.755	0.08	39.60			1972	82543
Plate 0.80 0 L-T 224.0 1.487 0.767 CT 0.746 0.08 40.20 42.40 9.20 40.20 40.46 9.02 40.20 1872 1872 Plate 0.80 2. 1.50 1.50 0.757 CT 0.764 0.02 47.70 47.70 1972 1972 Plate 0.80 2. LT 222.0 1.503 0.753 CT 0.769 47.60 45.4 3.9 1972 1972 Plate 0.80 4. 222.0 1.502 0.753 CT 0.769 0.12 47.60 45.4 3.9 1972 Plate 0.80 4. 222.0 1.501 0.753 CT 0.779 0.14 51.90 45.4 3.9 1972 0.80 4. 4.0 0.0 4.0 4.0 4.0 1972 1972			08:0			224.0	1.498	0.758	CT	0.772	0.10	44.50		-	1972	82543
Plate 0.80 22. 1.50 0.757 CT 0.784 0.09 42.40 42.40 1972 1972 Plate 0.80 20 LT 222.0 1.500 0.758 CT 0.778 0.08 45.4 45.4 3.9 1972 1972 Plate 0.80 20 LT 222.0 1.503 0.758 CT 0.779 47.50 45.4 3.9 1972 1972 Plate 0.80 40 LT 220.0 1.501 0.758 CT 0.779 0.14 51.30 45.4 3.9 1972 1972	S-BAY QUENCH 976F SQ 00F 1000F 2+2HR	Plate	0.80	0	LT	224.0	1.487	0.757	СT	0.746	90:0	40.20	42.4	2.2	1972	82543
Plate 0.80 20. LT 222.0 1.60% 0.767 CT 0.764 0.12 47.70 45.4 45.4 3.9 1972 1972 Plate 0.80 20. LT 222.0 1.503 0.758 CT 0.789 0.12 47.60 45.4 3.9 1972 1972 Plate 0.80 40 LT 220.0 1.501 0.758 CT 0.770 0.14 61.30 62.8 2.1 1972			0.80			224.0	1.496	0.757	СТ	0.781	0.09	42.40			1972	82543
Plate 0.80 20 LT 222.0 1.503 0.758 CT 0.778 0.08 40.90 46.4 3.9 1972 1972 0.80 4.0.80 222.0 1.502 0.758 CT 0.779 0.12 47.60 47.60 1972 1972 Plate 0.80 40 LT 220.0 1.501 0.758 CT 0.770 0.15 52.8 2.1 1972			0.80			222.0	1.500	0.757	CT	0.764	0.12	47.70			1972	82543
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1650F AUS-BAY QUENCH 976F SQ 400F 1000F 2+2HR	Plate	08.0	20	7.	222.0	1.503	0.758	CT	0.778	90.08	40.90	45.4	3.9	1972	82543
Plate 0.80 40 L-T 220.0 1.501 0.758 CT 0.773 0.14 51.30 1972 1972 1972			0.80			222.0	1.502	0.758	СŢ	0.769	0.12	47.60			1972	82543
Plate 0.80 40 L-T 220.0 1.502 0.758 CT 0.770 0.15 54.30 52.8 2.1 1972	S-BAY QUENCH 976F SQ		0.80	<u>-</u>	E	220.0	1.501	0.758	CT	0.773	0.14	61.30			1972	82543
	400F 1000F 2+2HR	Plate	08.0	40	1.4	220.0	1.502	0.758	cr	0.770	0.15	54.30	52.8	2.1	1972	82543

		REFER	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543
		DATE	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	2461	1972	1972	1972	1972	1972	1972	1972	1972	1972
		STAN DBV												12.1						·		·		
	K _{Io}	K. MEAN												64.4										
		K. (Kei • √(n.)	26.00	72.70	54.70	86.10	89.40	54.20	67.70	54.00	80.80	79.60	81.50	73.30	66.70	81.90	66.70	56.10	63.90	62.00	69.00	99.99	81.70	61.90
	* **	(K, TYS)" (in.)	0.16	0.28	0.16	0.39	0.42	0.16	0.18	0.16	0.35	0.34	0.35	0.28	0.16	0.36	0.24	0.28	0.15	0.14	0.18	0.24	98.0	0:30
	CRACK	LENGTH (in.) A	0.752	0.769	0.773	0.767	0.771	0.622	0.747	0.756	0.633	0.617	0.624	0.622	0.770	0.624	0.762	0.622	0.755	0.768	0.765	0.756	0.762	0.623
C K,	z	DEBIGN	cr	CT	cr	CT	CT	CT	CT	CT	CI	cr	CT	CT	СŢ	CT	CT	CT	CT.	CT	CT	CT	CT	CT
IL D&AC	SPECIMEN	THICK (in.) B	0.692	0.749	0.753	0.749	0.747	909'0	0.692	0.750	90910	0.608	0.607	0.607	0.694	0.607	0.755	0.606	0.691	0.750	0.692	0.757	0.754	909.0
ALLOY STEEL	<i>a</i> 2	WIDTH (in.)	1.504	1.504	1.494	1.504	1.502	1.197	1.505	1.501	1.202	1.199	1.200	1.200	1.505	1.199	1.500	1.197	1.505	1.603	1.505	1.498	1.500	1.198
AL		YIRLD STR (Kel)	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0
		SPEC	.										1											
		TEST TEMP (°F)											1	K.T.										
	oucr	THICK (in.)	0.80	0.80	0.80	0.80	0.80	0.80	0.80	08.0	0.80	08.0	0.80	08'0	0.80	0.80	0.80	0.80	0.80	0.80	0.80	080	0.80	0.80
	PRODUCT	FORM												Plate										
		CONDITION											1650F AUS-BAY QUENCH 975F 9Q	400F 1000F 2+2HR										

					ALI	ALLOY STEEL	L D6AC	C K,							
1	PRODUCT	UCT				æ	SPECIMEN	7	CRACK	9		Kı			
	FORM	THICK (In.)	TEST TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (in.)	THICK (in.)	DESIGN	LENGTH (in.) A	(K.,TYS)* (in.)	K. (iii)	K. MEAN	STAN	DATE	RBFER
	•	0.80			217.0	1.203	0.608	cr	0.625	0.29	73.40			1972	82543
	******	08.0			217.0	1.193	0.605	CT	0.613	0.17	67.50			1972	82543
	•	0.80			217.0	1.501	0.752	CT	0.765	0.11	46.40			1972	82543
		0.80			217.0	1.502	0.695	CT	0.762	0.10	44.50			2261	82543
		0.80		1	217.0	1.197	0.607	CT	0.625	0.42	88.80			1972	82543
		0.80			217.0	1.505	0.694	CT	0.755	0.19	59.40			1972	82543
		0.80			217.0	1.203	0.600	CT	0.635	0.18	58.90			1972	82543
		0.80			217.0	1.200	0.608	CT	0.616	0.18	58.60			1972	82543
		0.80		•	217.0	1.198	0.603	CJ.	0.636	0.17	56.00			1972	82543
		0.80		•	217.0	1.500	0.751	CT	0.729	0.32	77.10			1972	82543
1650F AUS BAY QUENCH 975F 9Q	Plate	0.80	R.T.	T.1	217.0	1.201	0.600	CT	0.622	0.19	69.50			1972	82543
	Cont'd	0.80	Cont'd	Cont'd	217.0	1.199	0.605	CT	0.621	0.44	91.00	Cont'd	Cont'd	1972	82543
		0.80			217.0	1.198	909:0	СŢ	0.619	0.18	28:00			1972	82543
		0.80			217.0	1.501	0.759	CT	0.756	0.18	48.50			1972	82543
		08.0			217.0	1.198	0.608	CT	0.622	0.14	52.10			1972	82543
		08'0			217.0	1.494	0.756	CT	0.755	0.18	68.60			1972	82543
		08.0			217.0	1.200	0.607	CT	0.620	0.31	76.80			1972	82543
		080			217.0	1.197	909'0	CT	0.617	0.31	76.60			1972	82543
		08.0			217.0	1.605	0.694	СŢ	0.758	0.21	62.90			1972	82543
		0.80			217.0	1.502	0.754	СŢ	0.766	0.37	83.60			1972	82543
		0.80			217.0	1.505	0.692	CT	0.759	0.16	55.40			1972	82543
		0.80			217.0	1.496	0.748	CT	0.744	0.20	60.80			1972	82543

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					AL	ALLOY STEEL	SL D6AC	C K.							
	PRO	PRODUCT				4	SPECIMEN	z	CRACK			K _{Io}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIRLD STR (Kel)	WIDTH (In.) W	THICK (In.)	DESIGN	LENGTH (ib.) A	(K, TYS)* (In.)	K. (Kad • √(m.)	K. MEAN	BTAN	DATE	REFER
		0.80			217.0	1.504	0.693	CT	97.0	0.17	57.20			1972	82543
		0.80			217.0	1.505	0.691	СT	0.747	0.18	69.00			1972	82543
		0.80			217.0	1.199	0.606	CT	0.613	0.33	79.30			1972	82543
		0.80			217.0	1.605	0.692	CT	0.762	0.19	60.20			1972	82543
		0.80			217.0	1.498	0.757	CI	0.771	0.29	73.60			1972	82543
		0.80		1	217.0	1.202	0.607	CT	0.621	0.21	63.40			1972	82543
		0.80			217.0	1.505	0.694	CT	0.753	0.20	61.80			1972	82543
		0.80			217.0	1.496	0.756	CT	0.747	0.45	92.30			1972	82543
		0.80		1	217.0	1.502	0.692	CT	0.779	0.20	61.90			1972	82543
		0.80			217.0	1.501	0.692	r U	0.755	0.10	43.90			1972	82543
10EAD ATTO DAY OTTENDED ON		0.80			217.0	1.203	0.606	CL	0.621	0.24	62.80			1972	82543
400F 1000F 2+2HR	Plate Cont'd	0.80	R.T. Cont'd	Cont'd	217.0	1.505	0.694	CT	0.753	0.20	60.90	Cont'd	Cont'd	1972	82543
0000		0.80		4	217.0	1.504	0.692	ÇŢ	0.741	0.16	64.50			1972	82543
		0.80			217.0	1.202	0.605	G.	0.630	0.32	78.00			1972	82543
		0.80		t	217.0	1.498	0.749	ÇŢ	0.766	0.27	71.40			1972	82543
		0.80			217.0	1.502	0.755	CT	0.751	0.18	64.00			1972	82543
		0.80			217.0	1.497	0.757	CT	0.749	0.18	67.90			1972	82543
		0.80			217.0	1.198	0.605	CT	0.630	0.31	76.20			1972	82543
		0.80			217.0	1.199	909.0	CT	0.617	0.14	60.60			1972	82543
		0.80			217.0	1.500	0.758	CT	0.777	0.32	77.70			1972	82543
		0.80			217.0	1.504	0.692	CT	0.774	0.16	55.20			1972	82543
		0.80			217.0	1.504	0.692	CT	0.764	0.17	67.00			1972	82543
		0.80			217.0	1.196	909.0	CI	0.620	0.22	64.20			1972	82543

		Ħ.			<u>_</u>	8	8	8	စ	8	8	63	83	<u> </u>	63	13	£3	£3	£3	£	2	£	43	£3
		RRFER	82543	82543	82543	82543	82543	82543	82543	82543	82543	82643	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543
		DATE	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972
		BTAN DEV												Cont'd										
	$\mathbf{K}_{\mathbf{lo}}$	K. MEAN												Contd										
		K. (Kel • √in.)	66.00	75.40	62.80	58.00	61.80	48.60	86.90	65.40	66.70	53.30	54.60	60.30	83.50	63.50	69.00	76.40	52.40	60.09	76.60	47.70	70.50	59.20
	***	(K/IYB)* (in.)	0.23	0.30	0.15	0.18	0.20	0.12	0.40	0.23	0.24	0.15	0.16	0.19	0.37	0.15	0.18	0.31	0.15	0.19	0.31	0.12	0.26	0.19
	CRACK	LENGTH (In.)	0.838	0.625	0.764	0.641	0.624	0.766	0.612	0.768	0.640	0.765	0.787	0.619	0.768	0.762	0.625	0.618	0.629	0.774	0.638	0.638	0.784	0.770
C K,	7	DESIGN	CT	CT	cr	CT	CT	CĪ.	CT	cT	CT	СT	CT	CT	cr	cr	CT	Ç	៦	СŢ	CT	CT	СT	Ę
L D6AC	SPECIMEN	THICK (in.) B	0.749	0.607	0.750	0.604	90.00	0.750	0.604	0.754	909.0	0.693	0.757	0.602	0.749	0.692	0.603	0.607	0.603	0.750	0.600	909.0	0.758	0.759
ALLOY STEEL	S2	WIDTH (In.)	1.498	1.200	1.500	1.201	1.198	1.501	1.199	1.498	1.201	1.504	1.500	1.199	1.500	1.504	1.199	1.200	1.199	1.497	1.199	1.199	1.500	1.505
ALI		YIRLD STR (Kal)	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0
		SPEC											7	Cont'd										
		TEST TEMP (°F)											R.T.	Cont'd										
	UCT	THICK (in.)	08.0	0.80	08.0	08.0	08:0	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	08.0	0.80	0.80	08.0	0.80	0.80	0.80	0.80	0.80
	PRODUCT	FORM											Plate	Cont'd										
	:	CONDITION											1650F AUS-BAY QUENCH 975F SQ	400F 1000F 2+2HR Cont'd									-	

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		REFER	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543
		DATE	1972	1972	1972	1972	1972	1972	1972	2261	1972	1972	1972	1972	2261	1972	1972	1972	1972	1972	1972	1972	1972	1972
		STAN								Cont'd								3.0		2.1			3.2	
	K _I °	K. MEAN								Cont'd								88.0		89.5			86.6	
		K. (Kal • √in.)	89.00	60.00	65.60	71.60	62.30	60.80	61.60	50.30	02'09	78.40	69.50	88.90	67.80	60.60	85.90	90.10	88.10	91.90	88.60	88.10	82.90	88.80
	* 30	(K _{s.} ,TYS)* (in.)	0.42	0.13	0.16	0.27	0.21	0.20	0.20	0.13	0.19	0.33	0.19	0.42	0.18	0.14	0.42	0.46	0.44	0.47	0.44	0.47	0.41	0.47
	CRACK	LENGTH (in.)	0.625	0.781	0.746	0.621	0.621	0.630	9696	0.773	0.615	0.630	0.779	0.619	0.630	0.765	0.761	0.770	0.779	0.775	0.784	0.782	0.770	0.771
C K.	7	DESIGN	CT	cr	cr	CT	CT	ст	CT	CT	ст	ст	CT	CT	CT	CT	CT	CT	CT	CT	CT	CT	CT	CT
L D6AC	SPECIMEN	THICK (in.)	0.605	0.753	0.755	0.608	0.605	0.605	0.608	0.753	0.608	0.605	0.749	0.608	0.605	0.753	0.757	0.757	0.758	0.758	0.758	0.759	0.750	0.759
ALLOY STEEL	92	WIDTH (fn.)	1.198	1.498	1.501	1.203	1.200	1.199	1.199	1.501	1.201	1.199	1.508	1.203	1.199	1.505	1.499	1.500	1.506	1.505	1.602	1.501	1.501	1.505
ALI		YIELD STR (Kei)	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	217.0	211.0	211.0	211.0	211.0	211.0	204.0	204.0	204.0
		SPEC	1	1						Cont'd								3					5	
		TEST TEMP (°F)							R.T.	Cont'd								OZ.		176			8	
	oucr	THICK (in.)	0.80	08:0	0.80	0.80	0.80	08'0	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	08.0	0.80
	PRODUCT	FORM							Plate	Cont'd							Ē	FIRIG		Plate			Plate	
		CONDITION							1650F AUS-BAY QUENCH 976F 8Q	Cont'd							1650F AUS-BAY QUENCH 975F SQ	400F 1000F 2+2HR		1650F AUS-BAY QUENCH 975F SQ 400F 1000F 2+2HR			1650F AUS-BAY QUENCH 976F SQ 400F 1000F 2+2HR	

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		REFER	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543
		DATE	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972
		BTAN DEV			2.9			1.3		3.2				3.0						12.3			
	K _{Ie}	K. MEAN			33.1			40.7		41.2				43.4						66.2			
		K. (Kei • vin.)	34.00	29.00	33.60	35.70	41.60	39.80	44.40	41.10	38.10	36.50	40.00	44.60	45.60	81.00	63.10	55.10	66.10	78.60	55.80	73.10	96.30
	•	(K. TY8)* (in.)	90'0	0.04	0.06	0.06	60'0	0.08	0.10	0.08	0.07	0.07	0.11	0.10	0.11	0.36	0.22	0.16	0.24	0.34	0.17	0.29	0.51
	CRACK	LENGTH (in.) A	0.784	0.790	0.757	0.760	0.753	0.776	0.759	0.769	0.765	0.769	0.761	0.757	0.751	0.628	0.784	0.618	0.618	0.625	0.618	0.623	0.775
c K	z	DEBIGN	CT	cr	CT	СТ	cr	CT	ст	CT	CT	cr	CT	Ę.	СŢ	CT	СŢ	CT	CT	cr	СT	cr	CI
L D6AC	SPECIMEN	THICK (In.) B	0.756	0.756	0.750	0.749	0.694	0.693	0.750	0.749	0.749	0.750	0.750	0.750	0.750	0,608	0.749	0.602	0.607	0.607	0.602	0.607	0.692
ALLOY STEEL	<i>a</i> 2	WIDTH (ln.) W	1.502	1.502	1.500	1.500	1.495	1.497	1.498	1.497	1.494	1.502	1.499	1.499	1.490	1.198	1.502	1.202	1.200	1.200	1.199	1.199	1.503
ALI		YIBLD STR (Kel)	225.0	225.0	225.0	225.0	224.0	224.0	222.0	222.0	222.0	220.0	218.0	218.0	218.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0
		SPEC	1	1	<u>.</u>			1.				LT		7.					E	Š			
		TEST TEMP (°F)		ě	ę		•	94.		-30		0		8					£	į			
	UCT	THICK (In.)	1.50	1.50	0.80	0.80	08.0	0.80	0.80	0.80	0.80	1.50	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80
	PRODUCT	FORM		ß	Forging			rorging		Forging		Forging		Forging					G Stranger	8018104			
		CONDITION		1650F AUS-BAY QUENCH 975F SQ	400F 1000F 2+2HR		1650F AUS BAY QUENCH 975F SQ	400F 1000F 2+2HR		1650F AUS-BAY QUENCH 975F SQ 400F 1000F 2+2HR		1650F AUS BAY QUENCH 976F SQ 400F 1000F 2+2HR		1650F AUS-BAY QUENCH 975F SQ 400F 1000F 2+2HR					1660F AUS-BAY QUENCH 975F SQ	400F 1000F 2+2HR			

		REFER	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543
		DATE	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972
		STAN												Cont'd										
	K _{Io}	K. MEAN									·			Cont'd							•			
		. (π.) (π.)	60.30	72.30	79.50	62.00	73.60	76.50	67.40	94.40	64.20	78.40	69.80	73.20	60.60	79.70	67.90	84.10	68.70	82.30	63.10	61.00	66.50	61.20
		2.0 (K _{r.} /TYS) ³ (in.)	0.14	0.28	0.34	0.15	0.30	0.31	0.18	0.49	0.22	0.34	0.20	0.29	0.20	0.35	0.18	0.39	0.26	0.37	0.15	0.20	0.24	0.14
	CRACK	LENGTH (in.) A	0.628	0.619	0.634	0.620	0.621	0.766	0.747	0.634	0.627	0.618	0.755	0.623	0.754	0.620	0.762	0.645	0.631	0.624	0.615	0.627	092.0	0.620
C K,	z	DESIGN	CT	cr	CT	СŢ	cr	CT	CT	CT	CT	СT	cr	cr	CT									
L D8AC	SPECIMEN	THICK (in.) B	0.695	0.603	0.607	0.602	0.602	0.750	0.696	909.0	0.604	0,603	0.749	0.599	0.757	0.604	0.750	0.607	0.605	0.603	0.603	909.0	0.752	0.605
ALLOY STEEL	92	WIDTH (in.) W	1.198	1.201	1.200	1.202	1.199	1.500	1.498	1.195	1.203	1.199	1.499	1.201	1.498	1.200	1.499	1.198	1.202	1.202	1.201	1.200	1.499	1.200
AL		YIELD STR (Kst)	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0
		SPEC					1		I				7	Cont'd	1						!		L	
		TEST TEMP (°F)											R.T.	Cont'd									-	
	PRODUCT	THICK (in.)	0.80	08:0	0.80	08:0	0.80	08.0	0.80	08.0	0.80	0.80	0.80	08:0	08:0	08'0	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80
	PROI	FORM			-								Forging	Cont'd			-							
		CONDITION											1650F AUS BAY QUENCH 975F SQ	Cont'd										

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		REFER	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82543	82643	82543	82543	82543	82543
		DATE	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972
		STAN												Cont'd											
	K _{Io}	K. MEAN												Cont'd											
		K. (Kei • (in.)	55.50	61.00	93.60	65.70	67.60	60.10	61.20	77.60	64.40	52.90	76.30	61.30	65.60	64.60	64.50	65.20	60.40	63.60	70.00	39.30	78.40	60.80	56.20
		(K_TYS)* (in.)	0.17	0.20	0.48	0.24	0.25	0.20	0.20	0.33	0.23	0.15	0.32	0.14	0.24	0.16	0.16	0.23	0.20	0.16	0.27	0.08	0.34	0.20	0.17
	CRACK	LENGTH (In.) A	0.762	0.766	0.767	0.631	0.631	0.761	0.635	692.0	0.756	0.626	0.598	0.620	0.617	0.623	0.775	0.618	0.626	0.751	0.622	0.866	0.617	0.633	0.623
J K _{te}	-	DESIGN	CT	CT	cr	Cţ.	CT	CT	CT	CT	CT	CT	CT	CT	CT	cr	CT	r.	Ç	CI	ಕ	C.	ţ	CT	చ్
L D6AC	SPECIMEN	THICK (in.)	0.750	0.750	0.692	0.603	0.607	0.694	0.607	0.750	0.753	0.603	0.608	909.0	909.0	0.603	0.750	0.599	0,605	0.750	0.604	0.756	0.603	0.603	0.603
ALLOY STEEL	62	WIDTH (in.)	1.502	1.499	1.502	1.200	1.200	1.497	1.197	1.501	1.499	1.202	1.198	1.200	1.199	1.201	1.502	1.200	1.200	1.497	1.200	1.499	1.199	1.201	1.199
ALI		YIELD STR (Kal)	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0
		SPEC												L-T Cont'd											
		TEST TEMP (°F)												R.T. Cont'd						,					
	UCT	THICK (in.)	08:0	0.80	0.80	0.80	0.80	08'0	0.80	08'0	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	08'0	1.50	0.80	0.80	0.80
	PRODUCT	FORM												Forging Cont'd											
		CONDITION												1650F AUS-BAY QUENCH 976F SQ 400F 1000F 2+2HR	Cont'd										

					YE.	ALLOY STEEL	EL D6AC	C K.							
	PRODUCT	UCT					SPECIMEN	z	CRACK			K _I °			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIRLD STR (Kei)	WIDTH (in.)	THICK (in.) B	DESIGN	LENGTH (in.)	E.S. (K., TYS)* (In.)	K. (Kal	K. MEAN	STAN	DATE	REFER
	•	0.80			208.0	1.498	0.750	CT	0.757	0.32	74.30			1972	82543
1650F AUS-BAY QUENCH 975F SQ 400F 1000F 2+2HR	Forging	0.80	176	7	208.0	1.500	0.750	C.T.	0.762	0.37	80.30	77.2	3.0	1972	82543
		0.80			208.0	1.604	0.750	СŢ	0.771	0.34	77.10			1972	82543
		1.00			i	1.999	1.008	CT	1.105	0.42	78.30			1973	85883 (1)
1675F AC 1575F OQ 400F 2HR	5758	1.00	Ē		1	2.002	1.006	CT	1.069	0.40	76.50			1973	85883 (1)
1100F 2HR (RC 42.5)	2	1.00	 	!	i	1.997	1.007	CT	1.075	0.42	77.60	77.1	1.0	1973	85883 (1)
		1.00			ï	1.995	1.008	CT	1.076	0.40	76.20			1973	85883 (1)
		1.00		1		2.001	1.007	CŢ	1.031	0.06	34.00			1973	85883 (2)
1675F AC 1675F OQ 400F 2HR	5	1.00	9		i	1.999	1.007	CT	1.046	0.04	33.00			1973	85883 (2)
500F 2HR (RC 50)	Linke	1.00	į	:	i	1.996	1.007	СŢ	1.032	90.0	35.10	34.5	1.2	1973	85883 (2)
		1.00			i	1.996	1.007	CT	1.069	0.06	35.80			8261	85883 (2)
		1.00			•	1.995	1.006	CT	1.139	0.15	63.50			1973	85883 (3)
1675F AC 1575F OQ 400F 2HR	210	1.00	£		i	1.995	1.006	СT	1.116	0.16	65.90			1973	85883 (3)
800F 2HR (RC 46.5)	Liane	1.00		' !	ı	1.992	1.006	CT	1.097	0.14	52.20	63.7	1.6	1973	85883 (3)
		1.00			ı	1.996	1.006	сī	1.118	0.15	53.10			1973	85883 (3)
		7.00			215.0	2.500	1.000	CŢ	1.400	0.31	75.70			1972	84277
1700F 1 HR FC TO 960F OQ AT 150F AC 1000F 2+2HR	Billet	7.00	R.T.	រ	215.0	2.500	1.000	CT.	1.400	0.38	84.30	80.3	8,4	1972	84277
		7.00			215.0	2.500	1.000	CT	1.400	0.36	80.80			1972	84277

PRODUCT												
_			0 2	SPECIMEN	יער	CRACK			K _{Ie}			
TEST SPEC YI TEMP OR E	F " 0	YTELD STR (Kal)	WIDTH (in.) W	THICK (in.)	DESIGN	LENGTH (In.) A	(K.,TYS)* (in.)	K. (Kal	K. MEAN	STAN	DATE	REFER
~]		214.0	2.500	1.000	CT	1.400	0.33	78.40			1972	84277
		214.0	2.500	1.000	CT	1.400	0.36	81.10			1972	84277
		214.0	2.500	1.000	C.	1.400	0.33	78.10			1972	84277
R.T.		216.0	2.500	1.000	CI	1.400	0.30	75.30	77.3	2.6	1972	84277
		216.0	2.500	1.000	C.	1.400	0.32	77.10			1972	84277
2	7	216.0	2.500	1.000	CL	1.400	0.29	73.70			1972	84277
5	83	228.0	1.502	0.759	CT	0.774	0.13	51.40			1972	82543
	- 7	228.0	1.502	0.750	CT	0.759	0.10	46.40			1972	82543
		228.0	1.506	0.759	CT	0.774	0.15	56.40			1972	82543
63	87	228.0	1.499	0.749	cT	0.755	0.16	68.60			1972	82543
.66 L-T		228.0	1.502	0.749	CT	0.748	0.13	62.80	51.4	6.0	1972	82543
	- 67	228.0	1.502	0.755	cr	0.763	0.11	48.70			1972	82543
		228.0	1.502	0.750	ភ	0.769	0.10	46.40			1972	82543
		228.0	1.501	0.759	C.	0.780	0.17	69.80			1972	82543
		228.0	1.506	0.750	Ľ.	0.753	60:0	42.20			1972	82543
		227.0	1.503	0.749	L	0.768	0.10	44.60			1972	82643
-40 L-T		227.0	1.499	0.754	CT	0.772	0.11	47.90	46.4	2:2	1972	82543
		227.0	1.601	0.750	CT	0.768	0.09	43.70			1972	82543
		226.0	1.601	0.750	СŢ	0.763	0.12	50.40			1972	82543
		226.0	1.504	0.754	CT	0.773	0.27	74.00			1972	82543
.50 .7.		226.0	1.502	0.752	CT	0.779	0.14	64.00	62.4	12.0	1972	82543
		226.0	1.500	0.755	Ę.	0 759	90.0	75.90			-	07.00

					AL	ALLOY STEEL	EL DEAC	C K,							
	PRODUCT	oucr					SPECIMEN	7	CRACK			K _{Ie}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kei)	WIDTH (in.) W	THICK (in.) B	DESIGN	LENGTH (in.) A	(K _{L,} /TYS)* (In.)	Kei (n)	K. MEAN	STAN	DATE	REFER
		08'0			226.0	1.504	0.749	CT	0.756	0.24	69.30			1972	82543
1700F AUS-BAY QUENCH 975F OG		0.80			226.0	1.502	0.755	CT	0.760	0.23	67.90			1972	82543
140F 1000F 2+2 HR Cont'd	Plate Cont'd	1.50	-20 Cont'd	Cont'd	226.0	1.499	0.749	CT	0.754	0.10	45.90	Cont'd	Cont'd	1972	82543
		0.80		<u></u> 1	226.0	1.506	0.749	CT	0.756	0.27	74.40			1972	82543
		1.60			226.0	1.601	0.750	CT	0.763	0.12	50.40			1972	82543
		1.50			224.0	1.602	0.750	CT	0.768	0.14	63.60			1972	82543
1700F AUS-BAY QUENCH 976F OQ 140F 1000F 2+2 HR	Plate	1.50	0	5	224.0	1.499	0.756	CT	0.799	0.16	56.50	ž.	ī	1972	82543
		1.50			225.0	1.503	0.750	CT	0.767	0.15	54.80	3	?	1972	82543
		1.60			222.0	1.500	0.755	CT	0.788	0.17	69.10			1972	82543
		0.80		<u>.</u>	222.0	1.504	0.755	CT	0.770	0.35	83.70			1972	82543
		0.80	•	L	222.0	1.601	0.753	CT	0.753	0.37	85.70			1972	82543
1700F AUS-BAY QUENCH 976F OQ 140F 1000F 2+2 HR	Plate	1.50	80	7.	222.0	1.501	0.750	CT.	0.778	0.17	58.40	76.5	13.5	1972	82543
		0.80			222.0	1.502	0.754	CT	0.770	0.41	89.90			1972	82543
		1.50		l	222.0	1.500	0.748	CT	0.762	0.26	71.30			1972	82543
		0.80			222.0	1.504	0.754	CT	0.765	0.39	87.20			1972	82543
		1.50			220.0	1.601	0.750	CT	0.790	0.22	66.10			1972	82543
1700F AUS-BAY QUENCH 976F OQ 140F 1000F 2+2 HR	Plate	1.50	40	7	220.0	1.499	0.752	CT	0.779	0.21	64.50	70.4	80	1972	82543
		1.50			220.0	1.501	0.749	CT	0.767	0.33	80.50			1972	82543
		0.80			217.0	1.504	0.757	CI	0.790	0.50	97.00			1972	82543
1700F AUS BAY QUENCH 976F OQ	Plate	0.80	E- pr	<u>-</u>	217.0	1.502	0.757	CT	0.779	0.47	94.20			1972	82543
140F 1000F 2+2 HR		0.80		1	217.0	1.506	0.752	CT	0.759	0.44	90.60	92.0	8.2	1972	82543
		0.80			217.0	1.498	0.756	CT	0.773	0.50	97.20			1972	82543

82643 82543 82543 82543 REFER 82543 82543 82543 82543 82543 82543 82543 82543 82543 82543 82543 82543 82543 82543 82543 82543 82543 82543 1972 1972 1972 1972 1972 DATE 1972 1972 1972 1972 1972 1972 1972 1972 1972 1972 1972 1972 1972 1972 1972 1972 1972 Cont'd STAN DEV Cont'd K. MEAN $K_{
m Ic}$ 101.70 100.50 94.70 91.70 91.00 92.50 83.30 99.10 95.40 93.20 91.90 70.80 96.30 Ж. . . 95.10 92.80 77.40 93.90 96.50 91.40 96.10 92.60 96.30 2.6 • (K.,TYS)* (in.) 0.48 0.46 0.53 0.48 0.46 0.44 9.65 0.49 0.45 0.45 0.49 0.49 0.520.27 0.37 0.47 0.44 0.48 0.45 0.49 0.46 0.32 CRACK LENGTH (In.) 0.786 0.776 0.779 0.767 0.782 0.766 0.803 0.759 0.755 0.7690.755 0.624 0.781 0.747 0.817 0.759 0.759 0.773 0.754 0.791 0.761 0.621 DESIGN 5 บี Ę Ç Ç CI CJ ร Ç Ç ij ธ CI 티 Ð ij ij ÇŢ Ç Ç ij ರ Ŗ, D6AC SPECIMEN 0.749 THICK (in.) B 0.749 0.758 0.758 0.756 0.758 0.758 0.752 0.753 0.760 0.757 0.6920.749 0.756 0.7520.607 0.694 0.757 0.757 0.758 0.607 0.757 ALLOY STEEL 1.499 1.495 WIDTH (fn.) W 1.502 1.497 1.603 1.502 1.496 1.497 1.503 1.498 1.500 1.202 1.497 1.639 1.501 1.601 1.504 1.500 1,503 1.498 1.499 1.201 217.0 217.0 217.0 217.0 217.0 217.0 YIELD STR (Ksi) 217.0 217.0 217.0 217.0 217.0 217.0 217.0 217.0 217.0 217.0 217.0 217.0 217.0 217.0 217.0 217.0 L.T Cont'd SPEC R.T. Cont'd TEST TEMP (°F) 53. 0.80 0.80 THICK (In.) 0.80 0.80 1.50 0.80 0.80 0.80 0.80 0.80 0.80 0.80 0.80 0.80 1.50 0.80 8.0 1.50 9.80 0.80 0.80 PRODUCT Plate Cont'd PORM 1700F AUS-BAY QUENCH 976F OQ 140F 1000F 2+2 HR Cont'd CONDITION

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TABLE 3.30.2.1 (CONTINUED)

					ALI	ALLOY STEEL	L D&AC	; Kı,							
	PROI	PRODUCT					SPECIMEN	7	CRACK			Kı			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (fn.)	THICK (in.) B	DESIGN	LENGTH (in.) A	2.0 (K _{L,} /TYB)* (In.)	K. (Kei •	K. MEAN	STAN	DATE	REFER
		0.80			217.0	1.500	0.758	CT	0.792	0.44	91.20			1972	82543
1700F AUS-BAY QUENCH 975F OQ	Plate	08.0	R.T.		217.0	1.500	0.751	CT	0.756	0.51	98.20			1972	82543
Cont'd	Cont'd	1.50	Cont'd	Cont'd	217.0	1.504	0.750	CT	0.765	0.22	64.10	Cont'd	Cont'd	1972	82543
		08.0			217.0	1.495	0.757	CT	0.802	0.47	94.20			1972	82543
		1.50			211.0	1.501	0.752	CT	0.785	0.48	92.70			1972	82543
		1.50			211.0	1.501	0.750	CT	0.763	0.61	95.20			1972	82543
1700F AUS-BAY QUENCH 975F OQ	, T	1.50	į	E	211.0	1.500	0.749	CT	0.760	0.44	89.20			1972	82643
140F 1000F 2+2 HR	riare	08.0	<u> </u>	<u> </u>	211.0	1.499	0.752	CT	0.752	0.45	89.30	92.3	3.1	1972	82543
		0.80		1	211.0	1.506	0.753	ст	0.761	0.46	90.70			1972	82543
		08.0			211.0	1.501	0.754	cr	0.779	0.62	96.50			1972	82543
		1.50			204.0	1.499	0.754	CT	0.790	0.50	91.30			1972	82543
1700F AUS-BAY QUENCH 975F OQ 140F 1000F 2+2 HR	Plate	1.50	300		204.0	1.499	0.750	CT	0.779	0.45	86.40	988	20.00	1972	82543
		1.50			204.0	1.499	0.749	CT	0.758	0.47	88.00			1972	82543
		1.50			225.0	1.500	0.751	CT	0.789	0.11	47.50			1972	82543
		1.50			225.0	1.601	0.749	CT	0.762	0.14	62.80			1972	82543
1700F AUS-BAY QUENCH 975F OQ	Doenin	1.60		E	226.0	1.502	0.751	CT	0.783	0.11	47.30			1972	82543
140F 1000F 2+2 HR	91118	1.60	3		225.0	1.501	0.752	CT.	0.760	0.09	41.80	45.5	5.5	1972	82543
		1.50			225.0	1.501	0.752	CT	0.760	0.09	42.60			1972	82543
		1.50			225.0	1.500	0.753	CT	0.758	0.08	41.10			1972	82543
		1.50			222.0	1.501	0.750	CT	0.752	0.18	65.70			1972	82543
1700F AUS-BAY QUENCH 976F OQ 140F 1000F 2+2 HR	Forging	1.50	-30	5	222.0	1.498	0.751	CT	0.765	0.12	49.60	58.3	10.3	1972	82543
		1.50			222.0	1.601	0.750	CT	0.777	0.25	69.60			1972	82543

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TABLE 3.30.2.1 (CONTINUED)

OPTION CONDITION (MICHOLAGE) FINAL PLANE (MICHOLAGE) STATE (MICH						ALI	ALLOY STEEL	L D8AC	K,							
Portrol		PROI	DUCT	, , , , , , , , , , , , , , , , , , ,			SC .	PECIMEN	7	CRACK			K _{Ie}			
Prompting 11.50 CT 0.775 CT 0.771 0.715 CT 0.741 0.159 6.55 8.55 8.55 1872	TION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (in.)	THICK (in.) B	DESIGN	LENGTH (in.)	(K_TYS)*	K. (E)	K. MEAN	STAN	DATE	REFER
Propriet 1.50 0.160 0.77 0.70 0.70 0.80 66.5 8.6 1.77 0.77			1.50			218.0	1.500	0.750	CT	0.778	0.31	76.50			1972	82543
1.60 1.60 1.80 1.80 0.70 0.70 0.21 6.50 1.97 <th< td=""><td>UENCH 976F 0Q F 2+2 HR</td><td>Forging</td><td>1.50</td><td>20</td><td>r.</td><td>218.0</td><td>1.499</td><td>0.750</td><td>CI</td><td>0.741</td><td>0.19</td><td>60.00</td><td>66.5</td><td>8.8</td><td>1972</td><td>82543</td></th<>	UENCH 976F 0Q F 2+2 HR	Forging	1.50	20	r.	218.0	1.499	0.750	CI	0.741	0.19	60.00	66.5	8.8	1972	82543
0.00 R. 14.0 1.486 0.787 CT 0.789 0.480 1850 1872			1.50			218.0	1.503	0.752	CT	0.770	0.21	63.10			1972	82543
0.80 0.80 CT 0.759 0.771 0.240 S0.200 CT 0.778 0.771 0.240 S0.200 CT 0.778 0.771 0.240 0.771 0.779 0.771 0.771 0.240 0.771 0.772 0.772 0.772 0.772 0.772 0.772 0.772 0.772 0.772 0.772 0.772 0.772 0.772 0.772 0.772 0.772 0.772 0.772 </td <td></td> <td></td> <td>0.80</td> <td></td> <td></td> <td>214.0</td> <td>1.498</td> <td>0.757</td> <td>CT</td> <td>0.767</td> <td>0.53</td> <td>98.50</td> <td></td> <td></td> <td>1972</td> <td>82543</td>			0.80			214.0	1.498	0.757	CT	0.767	0.53	98.50			1972	82543
0.80 114.0 1.60 0.70 0.778 0.46 90.40 1972			0.80			214.0	1.501	0.750	CT	0.759	0.46	91.80			1972	82543
0.80 214.0 1.801 0.776 0.756 0.677 10240 1972 1972 0.80 214.0 1.484 0.777 CT 0.786 0.47 88.00 1972 1972 0.80 214.0 1.600 0.760 CT 0.771 0.67 1920 1972 1.50 214.0 1.600 0.760 CT 0.760 0.49 66.39 84.00 1972 1972 1.50 214.0 1.601 0.762 CT 0.762 0.49 66.39 84.00 1972			080			214.0	1.503	0.750	CT	0.778	0.45	90.40			1972	82543
0.890 A. March 1.694 0.767 CT 0.788 0.47 93.00 1972 1972 1872			0.80			214.0	1.501	0.748	cr	0.755	0.67	102.40			1972	82543
0.80 R.1. 114.0 0.767 CT 0.780 CT 0.780 </td <td></td> <td></td> <td>0.80</td> <td></td> <td></td> <td>214.0</td> <td>1.494</td> <td>0.757</td> <td>cr</td> <td>0.758</td> <td>0.47</td> <td>93.00</td> <td></td> <td></td> <td>1972</td> <td>82543</td>			0.80			214.0	1.494	0.757	cr	0.758	0.47	93.00			1972	82543
Forging 0.80 R.T. 1.499 0.767 CT 0.765 0.49 66.30 1972 1972 Forging 0.80 R.T. 1.40 1.601 0.765 CT 0.765 0.89 84.90 1972 1972 Forging 0.80 R.T. 1.4 1.498 0.766 CT 0.762 0.85 98.00 644 1972 1972 0.80 R.T. 1.4 1.498 0.766 CT 0.789 0.47 92.00 1972 1972 0.80 2.1 1.50 0.766 CT 0.789 0.47 92.00 1972 1972 0.80 2.1 1.60 0.761 CT 0.789 0.47 92.00 1972 1972 0.80 2.1 1.60 0.761 CT 0.769 0.46 92.00 1972 1972 0.80 2.1 1.50 0.761 CT 0.762 0.47 92.00 1972 </td <td></td> <td></td> <td>0.80</td> <td></td> <td></td> <td>214.0</td> <td>1.500</td> <td>0.750</td> <td>CT</td> <td>0.771</td> <td>0.67</td> <td>102.00</td> <td></td> <td></td> <td>1972</td> <td>82543</td>			0.80			214.0	1.500	0.750	CT	0.771	0.67	102.00			1972	82543
Forging 0.80 R.T. L.T. 214.0 1,500 CT 0.765 0.59 84.90 1972 1972 Forging 0.80 R.T. 214.0 1,498 0,748 CT 0,769 0,46 91.00 96.2 197.0 1972			0.80	•	-	214.0	1.499	0.757	CT	0.760	0.49	95.30			1972	82543
Forging 0.80 R.T. L.T 214.0 1.488 0.750 CT 0.769 0.65 98.50 46.4 1872 1872 0.80 R.T. 214.0 1.498 0.749 CT 0.789 0.66 91.00 96.5 6.4 1972 1972 0.80 0.80 214.0 1.501 0.760 CT 0.789 0.47 92.60 1972 1972 1.50 214.0 1.601 0.750 CT 0.789 0.47 93.00 1972 1972 0.80 214.0 1.501 0.750 CT 0.789 0.46 95.00 1972 1972 0.80 214.0 1.500 0.761 CT 0.769 0.47 95.80 1972 1972 0.80 214.0 1.501 0.760 CT 0.769 0.47 92.80 1972 1972 0.80 214.0 1.501 0.776 CT 0.769 0.47			1.50			214.0	1.601	0.752	CT	0.765	0.39	84.90			1972	82543
Porging 0.80 R.T. L-T 214.0 1.488 0.748 CT 0.759 0.46 91.00 96.2 6.4 1972 0.80 214.0 1.501 0.749 CT 0.789 0.47 92.60 1972 1972 0.80 214.0 1.501 0.750 CT 0.789 0.47 92.60 1972 1972 1.50 214.0 1.503 0.753 CT 0.769 0.47 92.00 1972 1972 0.80 214.0 1.503 0.753 CT 0.769 96.90 96.90 1972 1972 1.50 214.0 1.501 0.751 CT 0.769 96.90 96.90 1972 1972 0.80 214.0 1.501 0.751 CT 0.769 96.80 96.80 1972 1972 0.80 214.0 1.501 0.749 CT 0.779 0.44 99.70 1972 1972			1.50			214.0	1.498	0.750	CT	0.762	0.53	98.50			1972	82543
214.0 1.500 0.766 CT 0.789 0.68 103.10 1972 214.0 1.501 0.749 CT 0.789 0.47 92.60 1972 214.0 1.499 0.750 CT 0.769 0.47 93.00 1972 214.0 1.500 0.763 CT 0.769 92.00 1972 214.0 1.500 0.761 CT 0.814 0.50 95.80 1972 214.0 1.501 0.751 CT 0.767 93.80 1972 214.0 1.501 0.761 CT 0.767 93.80 1972 214.0 1.501 0.761 CT 0.767 94.6 91.60 1972 214.0 1.501 0.761 CT 0.774 94.6 91.60 1972	QUENCH 976F 0Q 0F 2+2 HR	Forging		R.T.	LT	214.0	1.498	0.749	CT	0.759	0.45	91.00	96.2	6.4	1972	82543
214.0 1.501 0.749 CT 0.789 0.47 92.60 1972 214.0 1.499 0.750 CT 0.762 0.47 93.00 1972 214.0 1.503 0.753 CT 0.769 0.46 92.00 1972 214.0 1.500 0.751 CT 0.769 0.47 92.80 1972 214.0 1.601 0.750 CT 0.763 0.47 92.80 1972 214.0 1.501 0.761 CT 0.769 94.6 93.60 1972 214.0 1.501 0.749 CT 0.769 0.46 91.60 1972 214.0 1.501 0.752 CT 0.774 0.44 89.70 1972			0.80			214.0	1.500	0.756	СT	0.782	0.58	103.10			1972	82543
214.0 1.499 0.750 CT 0.769 0.47 98.00 1972 214.0 1.503 0.753 CT 0.769 0.46 92.00 1972 214.0 1.500 0.761 CT 0.814 0.50 95.80 1972 214.0 1.501 0.751 CT 0.753 0.47 92.80 1972 214.0 1.501 0.761 CT 0.767 93.60 1972 214.0 1.501 0.762 CT 0.774 91.60 1972 214.0 1.501 0.762 CT 0.774 89.70 1972			0.80			214.0	1.501	0.749	CT	0.789	0.47	92.60			1972	82543
214.0 1.503 0.763 CT 0.769 0.46 92.00 1972 214.0 1.500 0.761 CT 0.814 0.50 95.80 1972 214.0 1.499 0.760 CT 0.763 0.47 92.80 1972 214.0 1.501 0.761 CT 0.767 93.60 1972 214.0 1.501 0.749 CT 0.779 91.60 1972 214.0 1.501 0.762 CT 0.774 94.4 99.70 1972			08.0			214.0	1.499	0.750	CI	0.762	0.47	93.00			1972	82543
214.0 1.500 0.751 CT 0.814 0.50 95.80 1972 214.0 1.499 0.750 CT 0.763 0.47 92.80 1972 214.0 1.501 0.761 CT 0.767 0.48 93.60 1972 214.0 1.501 0.749 CT 0.774 91.60 1972 214.0 1.501 0.752 CT 0.774 0.44 89.70 1972			1.50			214.0	1.503	0.753	CT	0.769	0.46	92.00			1972	82543
214.0 1.499 0.750 CT 0.763 0.47 92.80 1972 214.0 1.501 0.751 CT 0.767 0.48 93.60 1972 214.0 1.500 0.749 CT 0.769 0.46 91.60 1972 214.0 1.501 0.762 CT 0.774 0.44 89.70 1972			08.0			214.0	1.500	0.751	СŢ	0.814	0.50	95.80			1972	82543
214.0 1.501 0.761 CT 0.767 0.48 93.60 1972 214.0 1.501 0.749 CT 0.779 0.46 91.60 1972 214.0 1.501 0.752 CT 0.774 0.44 89.70 1972			08.0			214.0	1.499	0.750	CT	0.753	0.47	92.80			1972	82543
214.0 1.500 0.749 CT 0.769 0.46 91.60 1972 214.0 1.501 0.752 CT 0.774 0.44 89.70 1972			1.50			214.0	1.501	0.751	CT	0.757	0.48	93.60			1972	82543
214.0 1.501 0.752 CT 0.774 0.44 89.70 1972			08:0			214.0	1.500	0.749	cr	0.759	0.46	91.60			1972	82543
			1.50			214.0	1.501	0.752	cr	0.774	0.44	89.70			1972	82543

TABLE 3.30.2.1 (CONTINUED)

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		DATE REFER	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 82543	1972 84277	1972 84277	
		STAN					.			Confe			L						1.7			10.1	<u></u>
	K _{Ic}	K. MBAN								Contid									97.5		-	75.1	:
		K. (Kei•	92.80	91.50	94.30	84.80	102.90	97.60	96.50	98.60	101.70	100.90	84.90	109.40	102.20	105.30	81.70	99.50	96.70	96.30	63.70	78.80	
		(K _L ,TYB)* (in.)	0.47	0.46	0.49	0.39	0.58	0.52	0.51	0.63	99.0	99.0	0.39	99.0	0.57	0.60	0.36	0.67	0.54	0.54	0.21	0.32	
	CRACK	LENGTH (in.) A	0.753	0.763	0.762	0.768	0.743	0.779	992'0	0.755	0.769	0.757	0.770	0.774	0.781	0.758	0.771	0.778	0.762	0.774	1.400	1.400	
C Kr.	7	DESIGN	CT	CT	cT	CT	CT	cr	ст	ст	CT	CT	CT	cr	CT	CT	CT	ст	CI	CT	CT	CT	
EL D6AC	SPECIMEN	THICK (in.) B	0.750	0.752	0.756	0.750	0.748	0.749	0.750	0.750	0.752	0.748	0.751	0.748	0.751	0.748	0.751	0.756	0.755	0.756	1.000	1.000	
ALLOY STEEL		WIDTH (In.) W	1.499	1.500	1.497	1.500	1.504	1.501	1.501	1.497	1.500	1.500	1.504	1.497	1.500	1.493	1.503	1.501	1.500	1.501	2.500	2.500	
		YIELD STR (Kel)	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	214.0	208.0	208.0	208.0	221.0	221.0	
		SPEC	•							L-T Cont'd									Ľ.			L.T.	
		TEST TEMP (°F)								R.T. Cont'd									175			R.T.	
	ucr	THICK (in.)	0.80	1.60	0.80	0.80	0.80	08'0	0.80	0.80	0.80	08.0	1.60	0.80	0.80	0.80	1.60	1.60	1.50	1.50	7.00	7.00	
	PRODUCT	FORM								Forging Cont'd									Forging			Billet	
		CONDITION							CO Library Control of the Control of	1700F AUS-BAY QUENCH 970F UQ 140F 1000F 2+2 HR	Conta								1700F AUS BAY QUENCH 976F OQ 140F 1000F 2+2 HR			960F SQ 350F 0.5 HR AC	1025F 2+2 HR

TABLE 3.30.2.1 (CONCLUDED)

<u> </u>	=																		
		REFER	84277	84277	84277	84277	84277	84277	84277	84277	84277	84277	84277	84277	84277	84277	84277	84029	84029
		DATE	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1972	1971	1971
		STAN DEV		2.7					6.2						6.1				1.8
	K _{Io}	K. MEAN		77.2					74.4						101.2				82.8
		K. (Kai • √in.)	80.10	74.70	76.90	75.50	73.20	83.10	64.60	71.90	77.90	97.70	91.20	109.00	104.00	103.00	102.00	87.00	84.50
	•	(K. TYS)* (in.)	0.35	0.31	0.33	0.31	0:30	0.38	0.22	0.27	0.32	09:0	0.62	0.74	0.65	0.63	0.62	0.45	0.42
	CRACK	LENGTH (in.) A	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	1.400	0.717	0.711
3 K.	7	DESIGN	CT	CT	CT.	CT	CT	CT	CT	CT	CT	CT	CT	CT	CT	CT	Сľ	NB NB	88
L D6AC	SPECIMEN	THICK (in.) B	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	0.700	0.700
ALLOY STEEL	oz.	WIDTH (fn.) W	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	1.400	1.401
		YIELD STR (Kei)	213.0	213.0	213.0	213.0	213.0	213.0	217.0	217.0	217.0	200.0	200.0	200.0	205.0	205.0	205.0	206.0	206.0
		SPEC	1			1		I	<u> </u>			LT						T-L	
		TEST TEMP (°F)		R.T.				E	1					Ę	į				R.T.
	UCT	THICK (in.)	7.00	7.00	7.00	7.00	7.00	7.00	10.00	10.00	10.00	7.00	7.00	7.00	10.00	10.00	10.00		ı
	PRODUCT	FORM		Billet				7-11:0	TO TO THE PARTY OF					7760	aniq				Plate
		CONDITION	Co di i dooni co di i dagani	1000F 1 HR OQ 1000F 1 HR 1000F 1 HR OQ 1000F 1 HR	AUTOL TITAL			1725F 1 HR AC 1700F 1 HR OQ	1025F 2+2 HR					1725F 1 HR AC 1700F 1 HR 09	1100F 2+2 HR			HEAT TREATED TO	46 RC HARDNESS

24 of 24

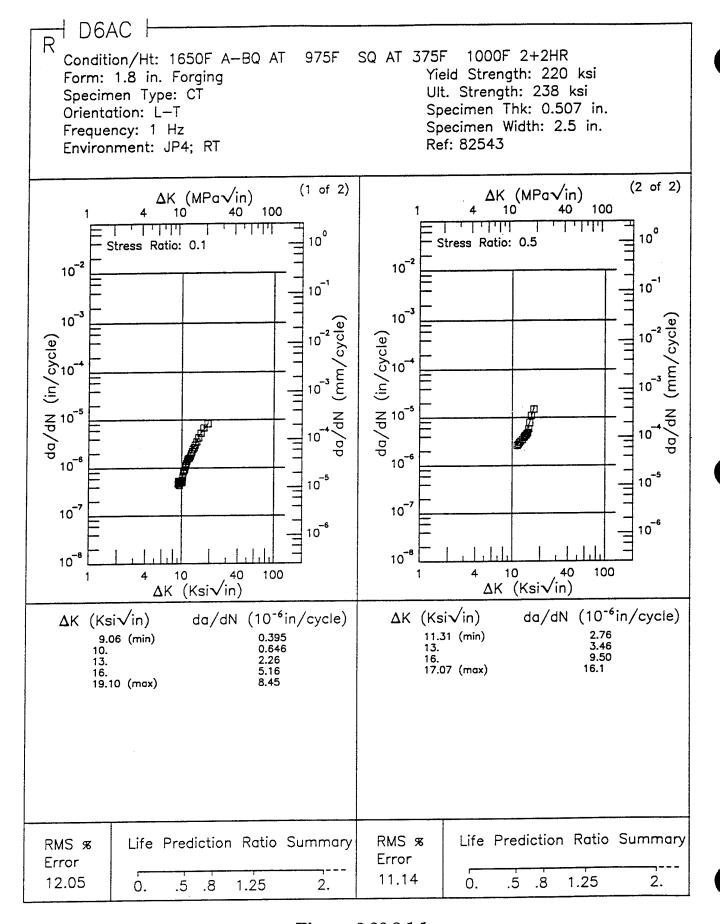


Figure 3.30.3.1.1

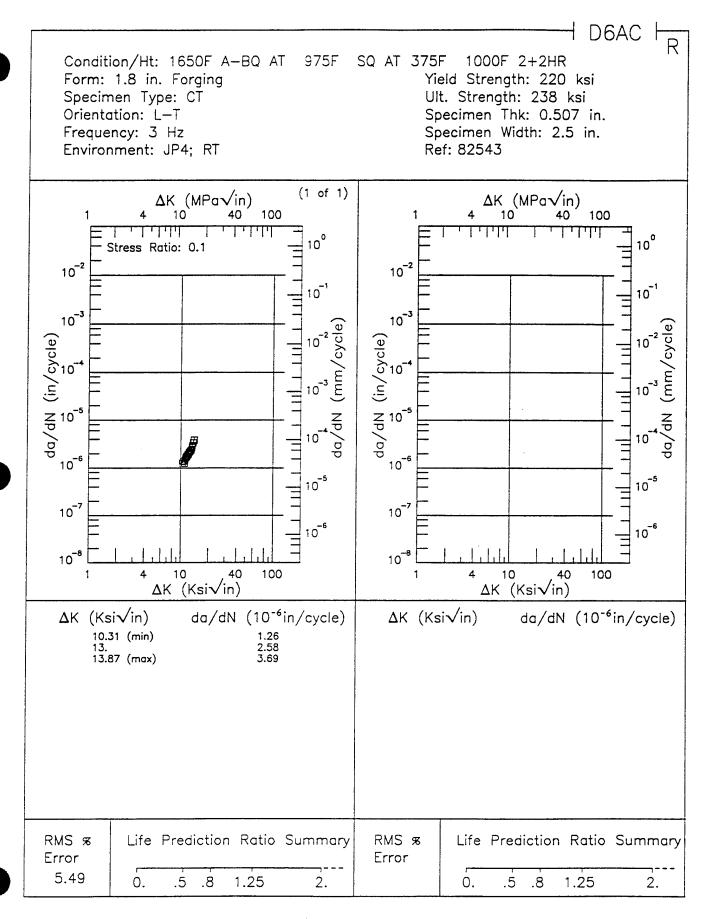


Figure 3.30.3.1.2

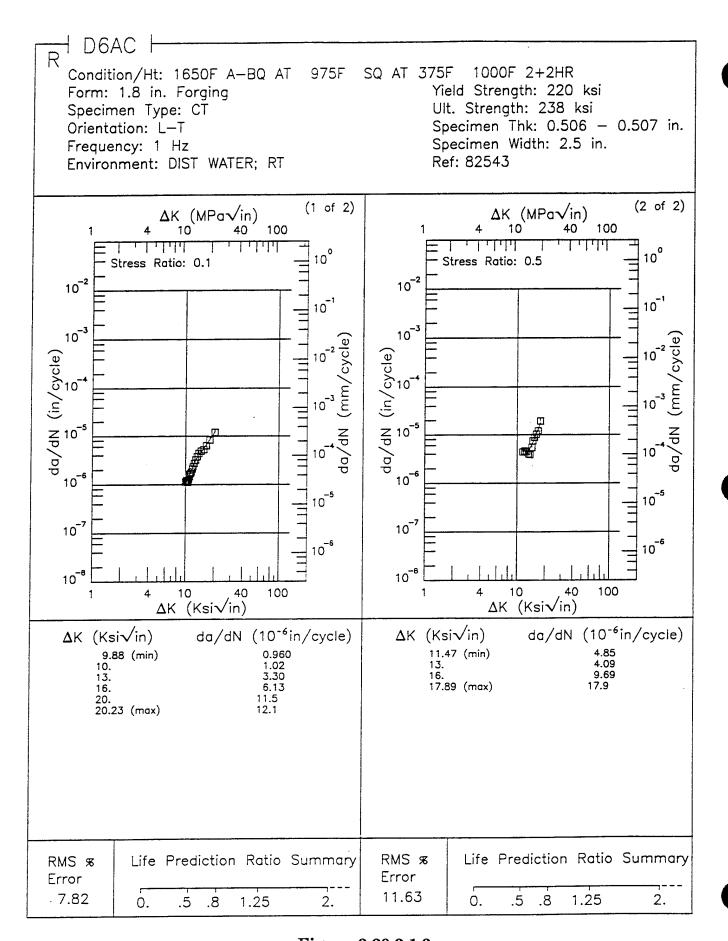


Figure 3.30.3.1.3

Yield Strength: 220 ksi Form: 0.8 in. Plate Ult. Strength: 238 ksi Specimen Type: CT Orientation: L-T Specimen Thk: 0.75 in. Stress Ratio: 0.08 Specimen Width: 5 in. Ref: 82543 Environment: DIST WATER; RT (1 of 2) (2 of 2) $\Delta K (MPa\sqrt{in})$ $\Delta K (MPa\sqrt{in})$ 10 40 100 10 100 11111 77111 11111 10° 10° Frequency: 0.1 Hz Frequency: 1 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10-6 10-6 10⁻⁵ 10⁻⁵ 10⁻⁷ 10-7 10-6 10 -8 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) ΔK (Ksi \sqrt{in}) $\Delta K (Ksi\sqrt{in})$ da/dN (10⁻⁶in/cycle) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS & Error Error Ó. .5 .5 8. 1.25 2. .8 1.25 2. 0.

SQ AT 400F

975F

Condition/Ht: 1650F A-BQ AT

1000F 2+2HR

D6AC F

Figure 3.30.3.1.4

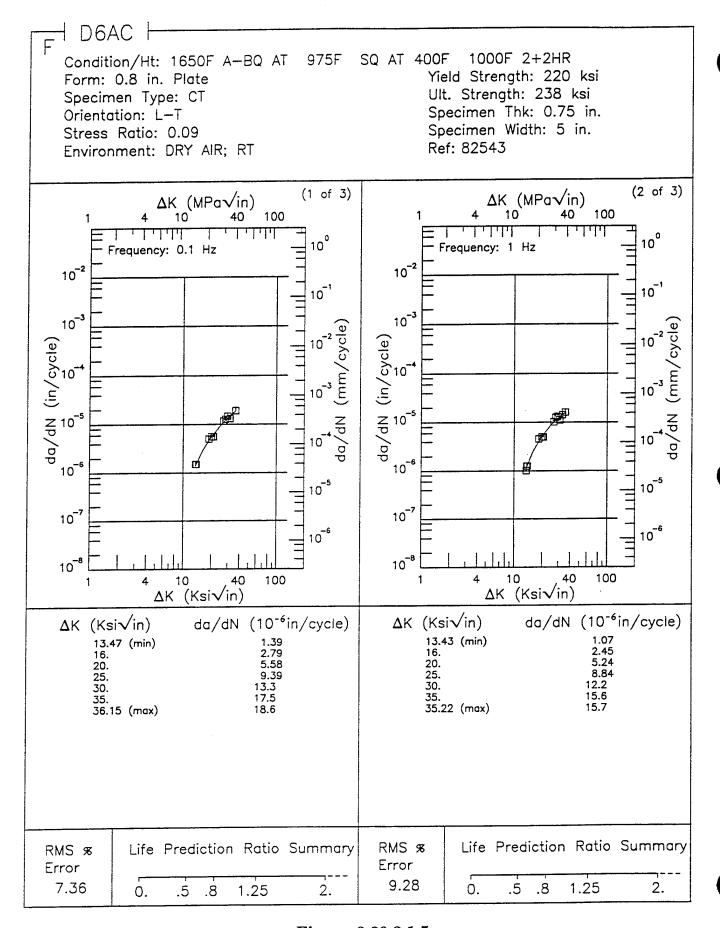


Figure 3.30.3.1.5

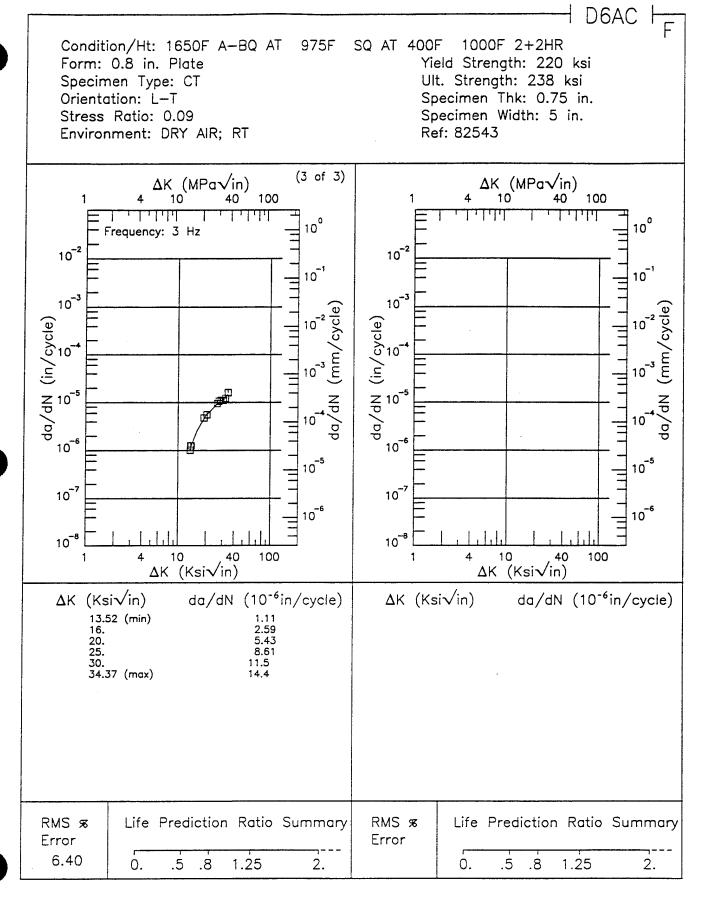


Figure 3.30.3.1.5 (Concluded)

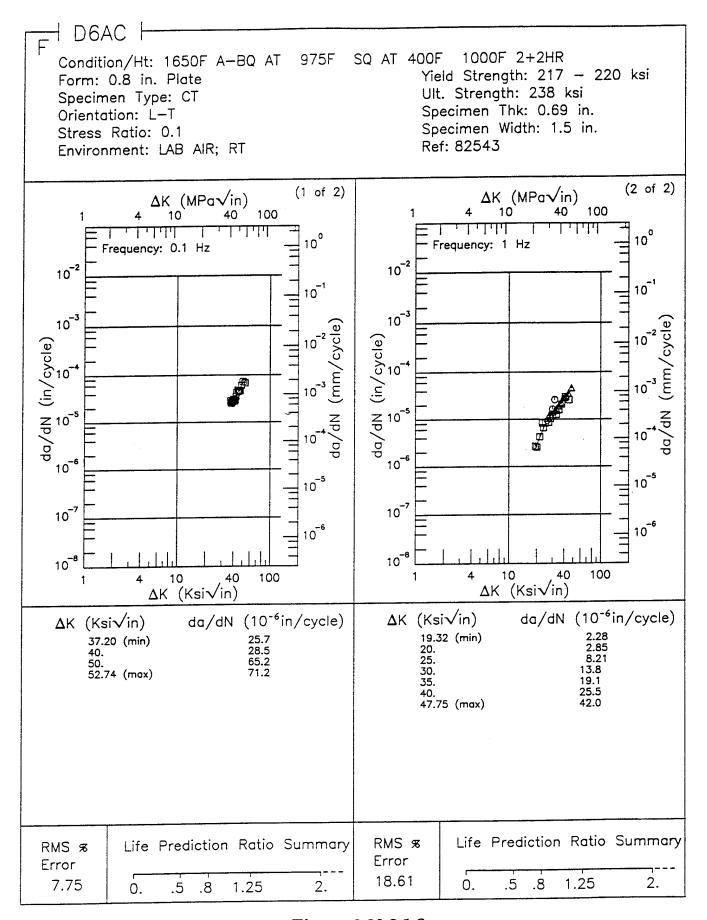


Figure 3.30.3.1.6

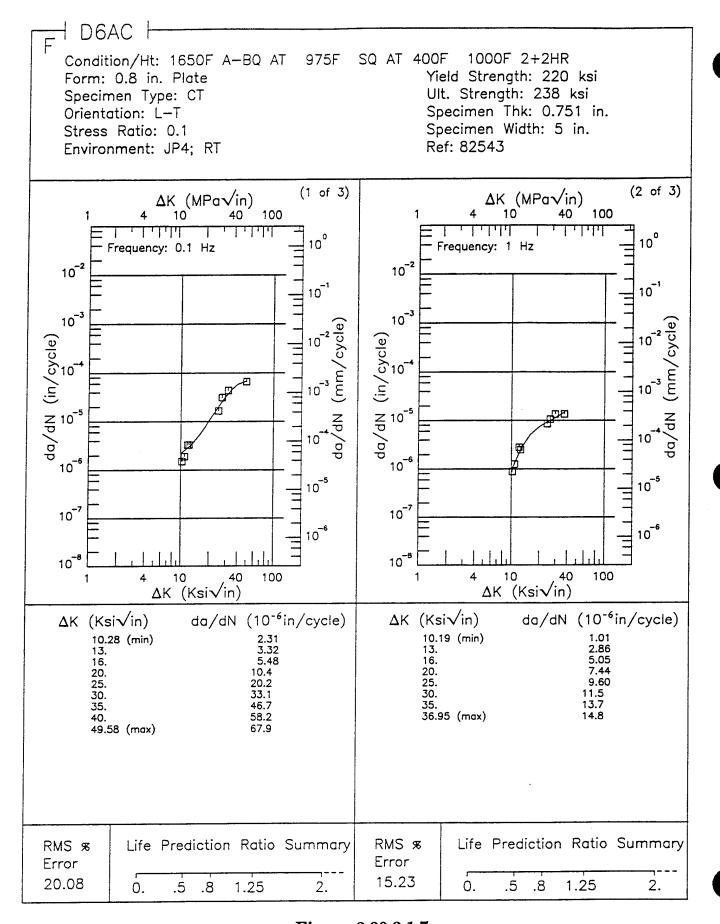


Figure 3.30.3.1.7

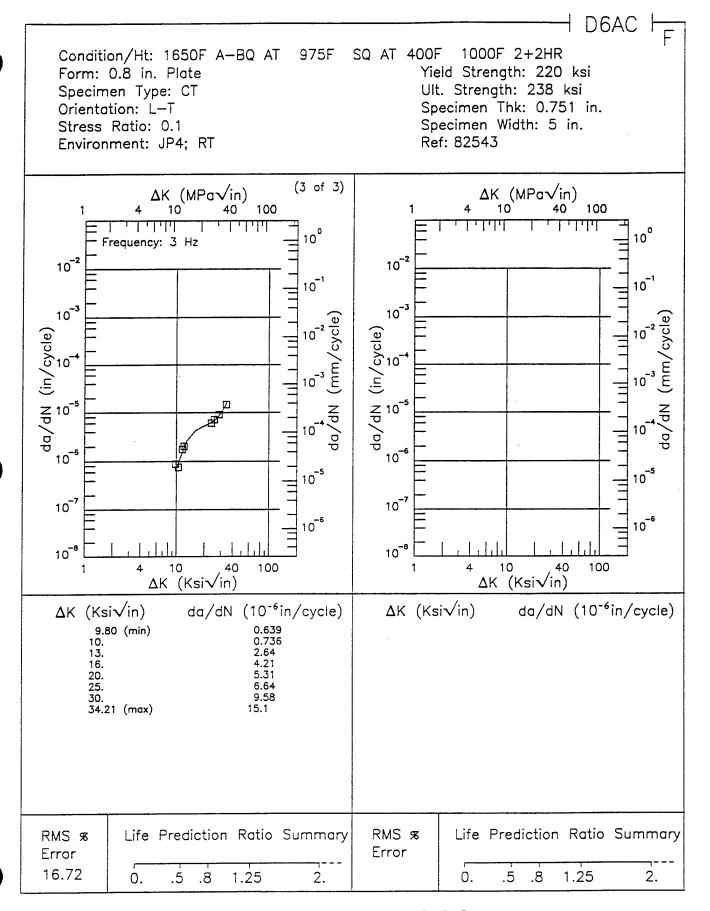


Figure 3.30.3.1.7 (Concluded)

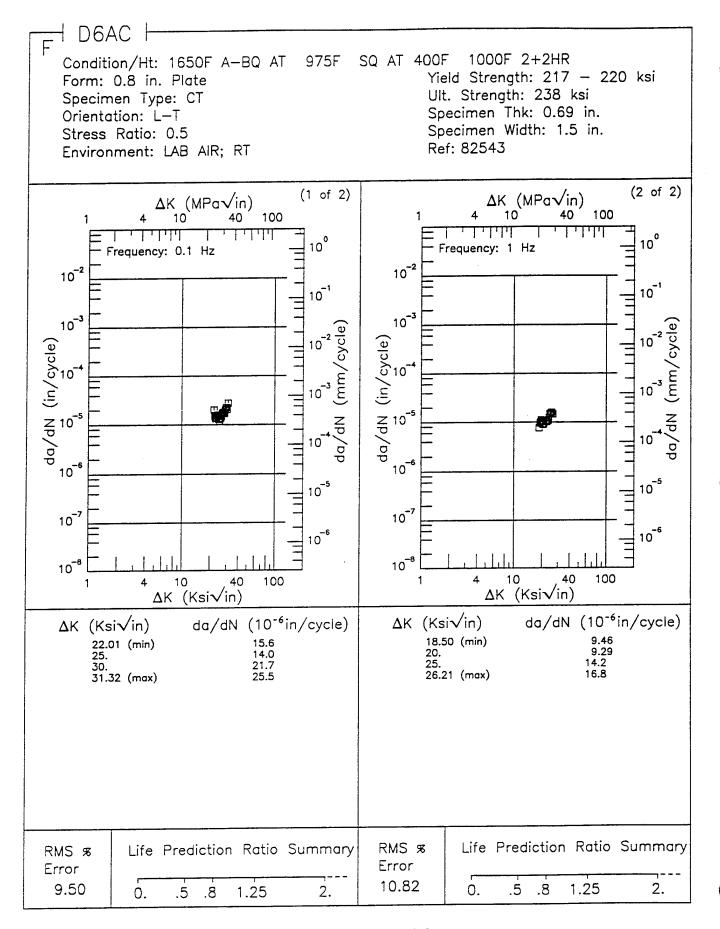


Figure 3.30.3.1.8

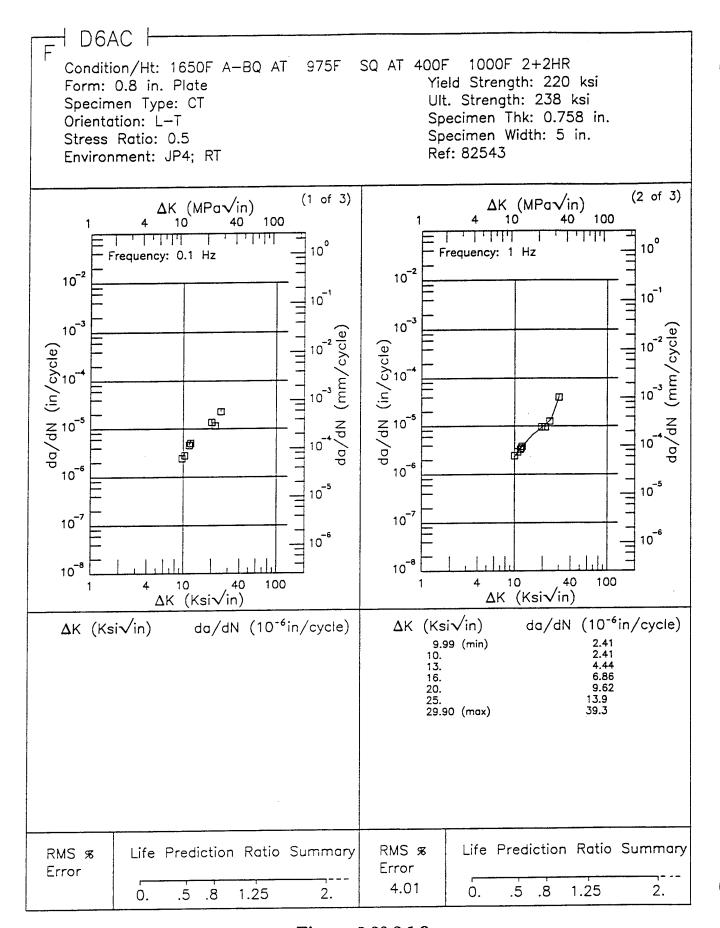


Figure 3.30.3.1.9

SQ AT 400F 1000F 2+2HR Condition/Ht: 1650F A-BQ AT 975F Yield Strength: 220 ksi Form: 0.8 in. Plate Specimen Type: CT Ult. Strength: 238 ksi Specimen Thk: 0.758 in. Orientation: L-T Specimen Width: 5 in. Stress Ratio: 0.5 Ref: 82543 Environment: JP4; RT (3 of 3)ΔK (MPa√in) Δ K (MPa \sqrt{in}) 100 10 100 10 40 المليلية لبليليا 10° 10° Frequency: 3 Hz 10-2 10-2 10 1 10 -1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10-3 10 10⁻⁶ 10-6 10⁻⁵ 10⁻⁵ 10⁻⁷ 10⁻⁷ 10 -6 10⁻⁶ 10-8 10⁻⁸ 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) ΔK (Ksi√in) 9.80 (min) 10. 0.980 13. 16. 4.38 6.45 20. 27.00 (max) RMS % Life Prediction Ratio Summary RMS & Life Prediction Ratio Summary Error Error 11.77 Ò. Ó. .5 .8 1.25 2. .5 .8 1.25 2.

1 D6AC F

Figure 3.30.3.1.9 (Concluded)

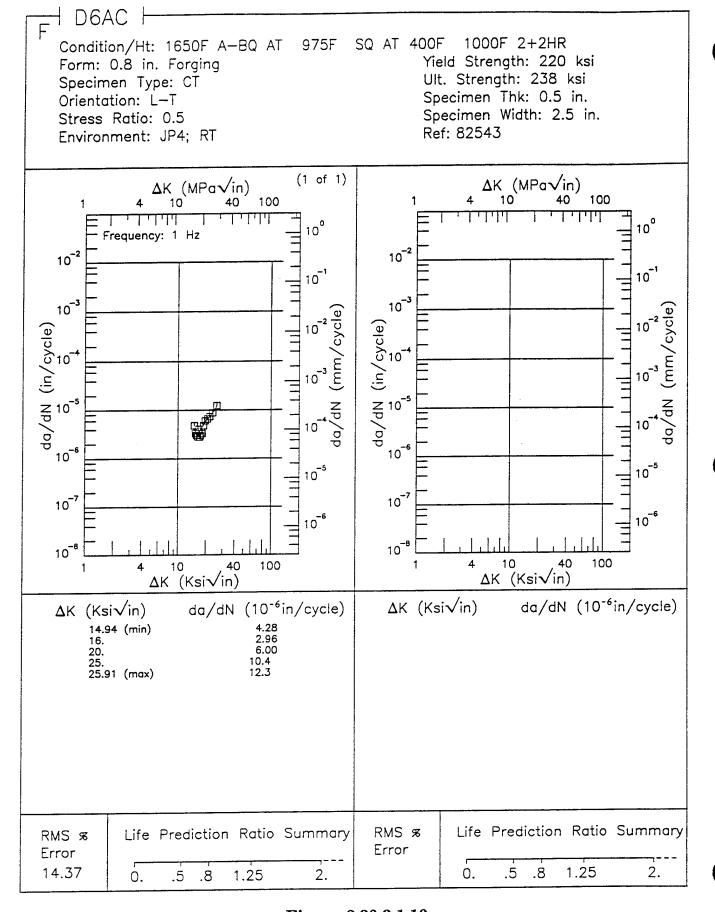


Figure 3.30.3.1.10

H D6AC F Condition/Ht: 1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS Form: 0.8 in. Plate Yield Strength: 220 ksi Specimen Type: CT Ult. Strength: 238 ksi Orientation: L-T Specimen Thk: 0.754 in. Stress Ratio: 0.08 Specimen Width: 5 in. Environment: DIST WATER; RT Ref: 82543 (1 of 2)(2 of 2) $\Delta K (MPa\sqrt{in})$ $\Delta K (MPa\sqrt{in})$ 40 100 10 10 100 <u>, 1, 1, 1, 1, 1, 1</u> 7 11111 11111 10° 10° Frequency: 0.1 Hz Frequency: 1 Hz 10-2 10-2 10-1 10 10⁻³ 10 da/dN (in/cycle) da/dN (in/cycle) 10-6 10-6 10 -5 10⁻⁵ 10⁻⁷ 10⁻⁷ 10-6 10 6 10 8 10⁻⁸ 100 10 40 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) Δ K (Ksi \sqrt{in}) da/dN ($10^{-6}in/cycle$) ΔK (Ksi \sqrt{in}) Life Prediction Ratio Summary RMS & RMS % Life Prediction Ratio Summary Error Error Ó. .5 .8 1.25 0. .5 .8 2. 1.25 2.

Figure 3.30.3.1.11

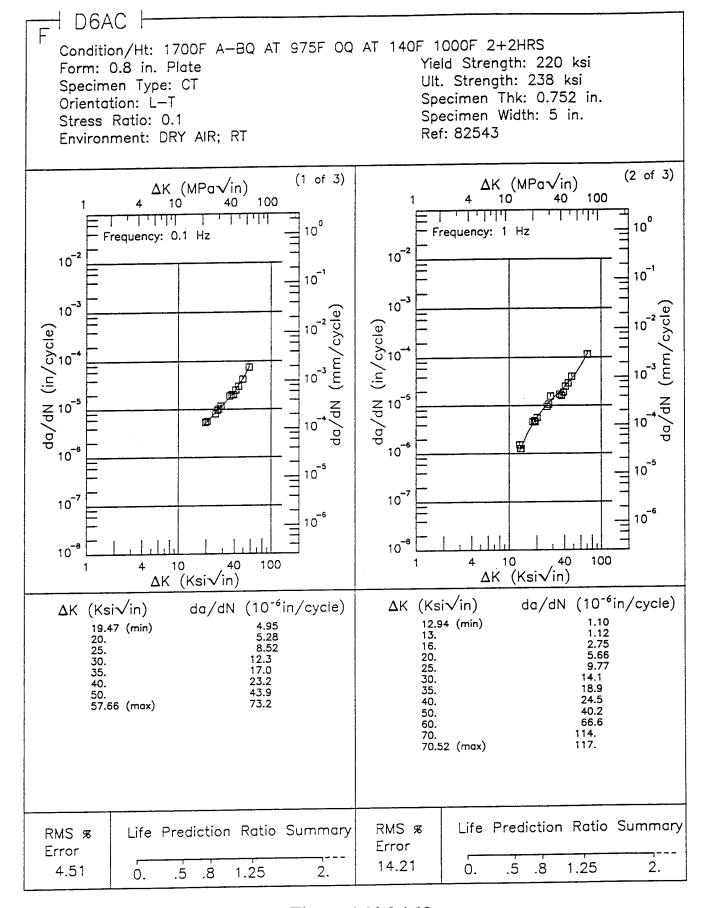


Figure 3.30.3.1.12

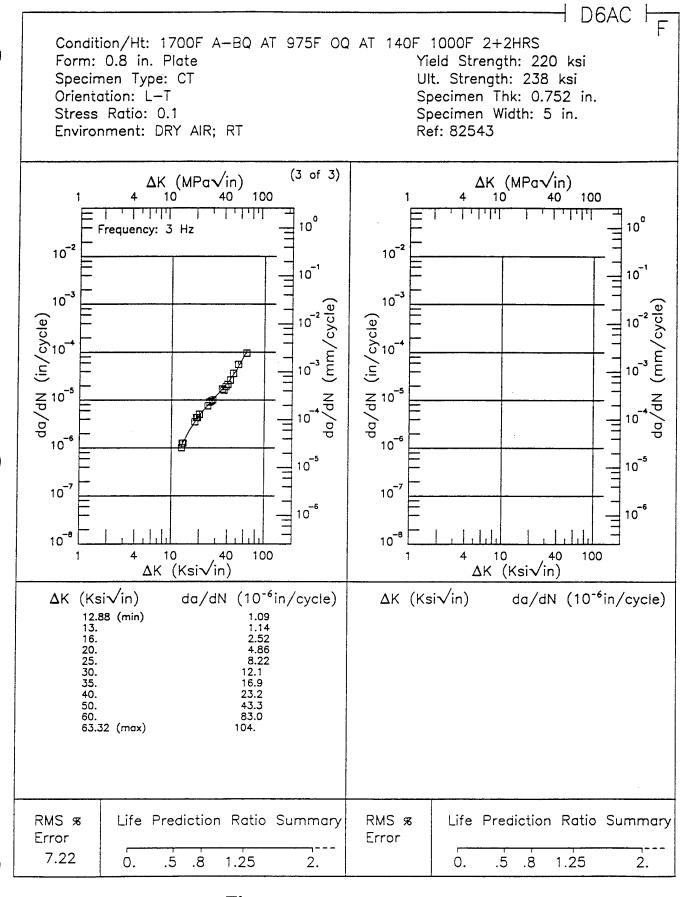


Figure 3.30.3.1.12 (Concluded)

D6AC H Condition/Ht: 1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS Yield Strength: 220 ksi Form: 0.8 in. Plate Ult. Strength: 238 ksi Specimen Type: CT Specimen Thk: 0.69 in. Orientation: L-T Specimen Width: 1.5 in. Stress Ratio: 0.1 Ref: 82543 Environment: LAB AIR; RT (1 of 1) $\Delta K (MPa\sqrt{in})$ $\Delta K (MPa\sqrt{in})$ 10 40 100 10 100 40 10° Frequency: 1 Hz 10 -2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10-6 10⁻⁶ 10 5 10-5 10⁻⁷ 10⁻⁷ 10⁻⁶ 10 -6 10-8 10 -8 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) Δ K (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) Δ K (Ksi \sqrt{in}) 19.72 (min) 20. 25. 30. 35. 40. 50. 105. 66.91 (max) RMS % Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % Error Error .5 1.25 2. 25.80 .8 0. 0. .5 .8 1.25 2.

Figure 3.30.3.1.13

D6AC Condition/Ht: 1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS Yield Strength: 220 ksi Form: 0.8 in. Plate Ult. Strength: 238 ksi Specimen Type: CT Specimen Thk: 0.741 in. Orientation: L-T Specimen Width: 5 in. Stress Ratio: 0.1 Ref: 82543 Environment: JP4/H20; RT (2 of 3)(1 of 3) ΔK (MPa√in) $\Delta K (MPa\sqrt{in})$ 100 10 100 10 40 1 1 1 1 1 1 1 1 11111 10° Frequency: 0.1 Hz Frequency: 1 Hz 10-2 10-2 10 1 10 10⁻³ 10-3 da/dN (in/cycle) da/dN (in/cycle) 10-6 10-6 10 5 10⁻⁵ 10⁻⁷ 10⁻⁷ 10⁻⁶ 10 6 10-8 10 40 100 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) ΔK (Ksi√in) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS & Error Error .5 1.25 2. 0. .8 .5 .8 1.25 2. 0.

Figure 3.30.3.1.14

Form: 0.8 in. Plate Yield Strength: 220 ksi Ult. Strength: 238 ksi Specimen Type: CT Orientation: L-T Specimen Thk: 0.741 in. Stress Ratio: 0.1 Specimen Width: 5 in. Environment: JP4/H20; RT Ref: 82543 (3 of 3)ΔK (MPa√in) 10 40 Δ K (MPa \sqrt{in}) 100 100 100 10° Frequency: 3 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10-6 10-6 10⁻⁵ 10⁻⁵ 10⁻⁷ 10-7 10⁻⁶ 10-8 10-8 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) ΔK (Ksi \sqrt{in}) da/dN ($10^{-6}in/cycle$) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS & RMS % Error Error .5 . 5 .8 Ò. 0. 1.25 2. .8 1.25 2.

Condition/Ht: 1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS

H D6AC F

Figure 3.30.3.1.14 (Concluded)

D6AC Condition/Ht: 1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS Yield Strength: 220 ksi Form: 0.8 in. Plate Ult. Strength: 238 ksi Specimen Type: CT Specimen Thk: 0.741 in. Orientation: L-T Specimen Width: 5 in. Stress Ratio: 0.11 Ref: 82543 Environment: DIST WATER; RT (2 of 3) (1 of 3) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 40 100 10 100 10 40 1 11111 11111 10° 10° Frequency: 1 Hz Frequency: 0.1 Hz 10-2 10-2 10 1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10-6 10-6 10 -5 10⁻⁷ 10⁻⁷ 10⁻⁶ 10-6 10 -8 10-8 10 40 100 4 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) Δ K (Ksi \sqrt{in}) 2.35 3.25 6.39 10.7 12.01 (min) 7.97 9.15 12.13 (min) 13. 16. 13. 16. 14.6 20. 25. 30. 25.4 20. 25. 44.9 69.9 30. 26.1 35. 39.73 (max) 127. 158. 46.20 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error 15.65 1.25 2. .5 8. 0. 2. 20.48 1.25 .5 .8 0.

Figure 3.30.3.1.15

Condition/Ht: 1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS Form: 0.8 in. Plate Yield Strength: 220 ksi Specimen Type: CT Ult. Strength: 238 ksi Specimen Thk: 0.741 in. Orientation: L-T Stress Ratio: 0.11 Specimen Width: 5 in. Environment: DIST WATER; RT Ref: 82543 (3 of 3) $\Delta K (MPa\sqrt{in})$ $\Delta K (MPa\sqrt{in})$ 10 40 100 10 40 100 11111 11111 10° Frequency: 3 Hz 10-2 10-2 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10⁻⁶ 10 -5 10⁻⁵ 10⁻⁷ 10⁻⁷ 10 -6 10⁻⁶ 10 8 10⁻⁸ 10 40 10 40 100 4 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) 12.24 (min) 13. 16. 20. 25. 5.88 7.59 30. 30.48 (max) RMS % Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary Error Error 35.22 Ò. .5 0. .5 .8 1.25 2. .8 1.25 2.

H D6AC F

Figure 3.30.3.1.15 (Concluded)

D6AC Condition/Ht: 1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS Yield Strength: 220 ksi Form: 0.8 in. Plate Ult. Strength: 238 ksi Specimen Type: CT Specimen Thk: 0.751 in. Orientation: L-T Specimen Width: 5 in. Stress Ratio: 0.5 Ref: 82543 Environment: DRY AIR; RT (2 of 3) (1 of 3) Δ K (MPa \sqrt{in}) $\Delta K (MPa\sqrt{in})$ 10 100 100 10 11111 11111 10° 10° Frequency: 1 Hz Frequency: 0.1 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10-6 10 -5 10 -5 10⁻⁷ 10-7 10⁻⁶ 10 6 10-8 10 8 100 10 40 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error .5 1.25 2. .8 0. 1.25 0. .5 8. 2.

Figure 3.30.3.1.16

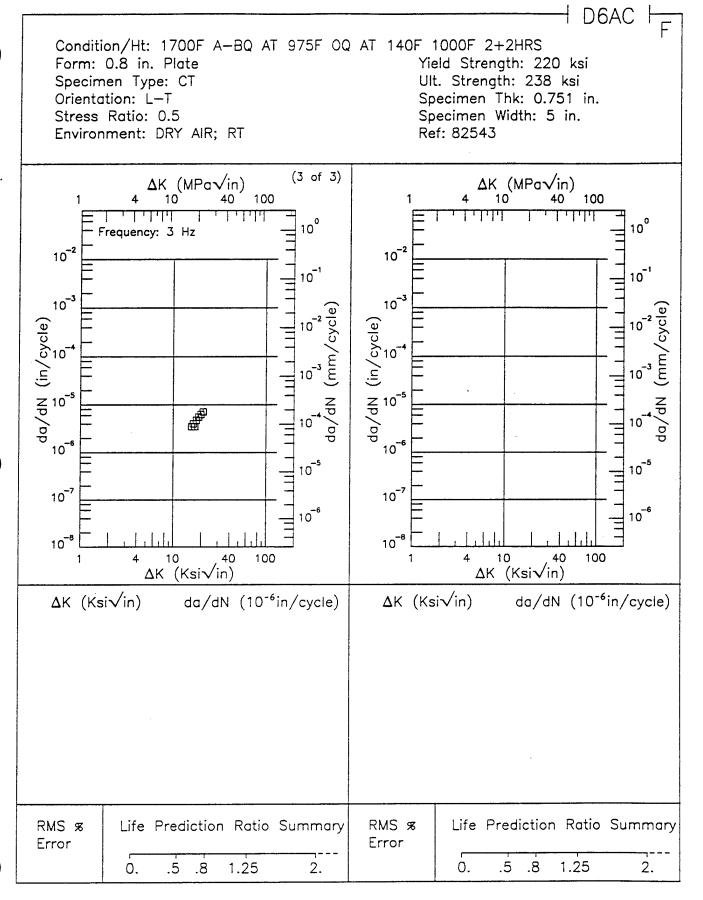


Figure 3.30.3.1.16 (Concluded)

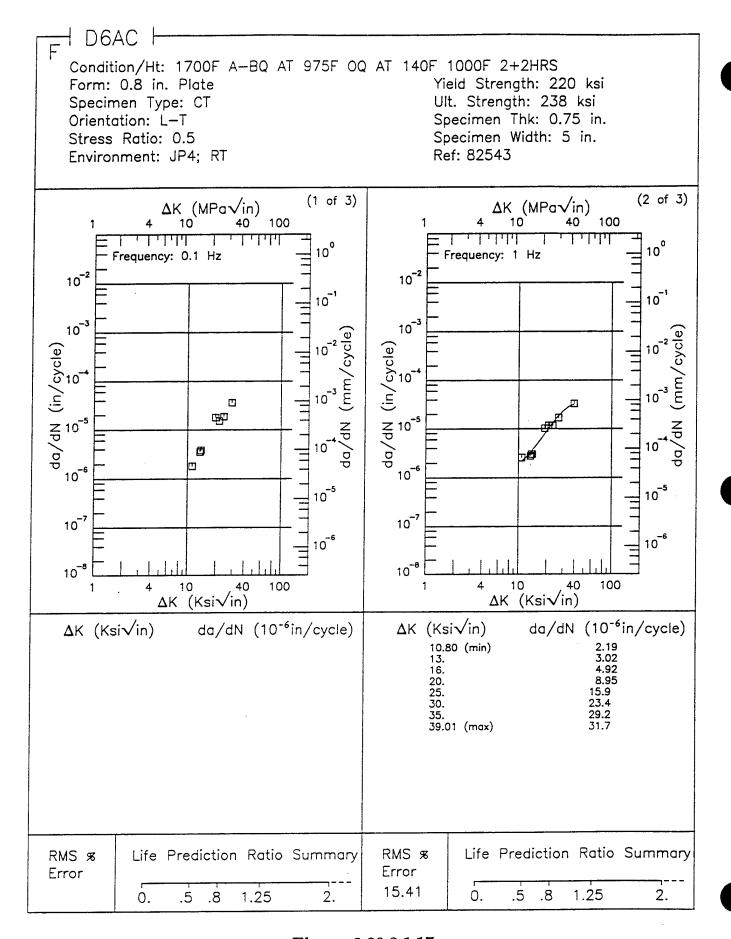


Figure 3.30.3.1.17

Condition/Ht: 1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS Yield Strength: 220 ksi Form: 0.8 in. Plate Ult. Strength: 238 ksi Specimen Type: CT Specimen Thk: 0.75 in. Orientation: L-T Specimen Width: 5 in. Stress Ratio: 0.5 Ref: 82543 Environment: JP4; RT (3 of 3)ΔK (MPa√in) Δ K (MPa \sqrt{in}) 10 100 10 100 40 40 711 1.1.1.1.1 10° 10° Frequency: 3 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10-2 10 10-6 10⁻⁶ 10 -5 10-5 10⁻⁷ 10⁻⁷ 10 -6 10⁻⁶ 10⁻⁸ 10-8 40 10 40 100 10 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 10.58 (min) 13. 16. 20. 25. 21.0 31.9 30. 33.66 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error 13.57 .5 1.25 2. 0. .5 .8 1.25 2. 0. .8

HD6AC F

Figure 3.30.3.1.17 (Concluded)

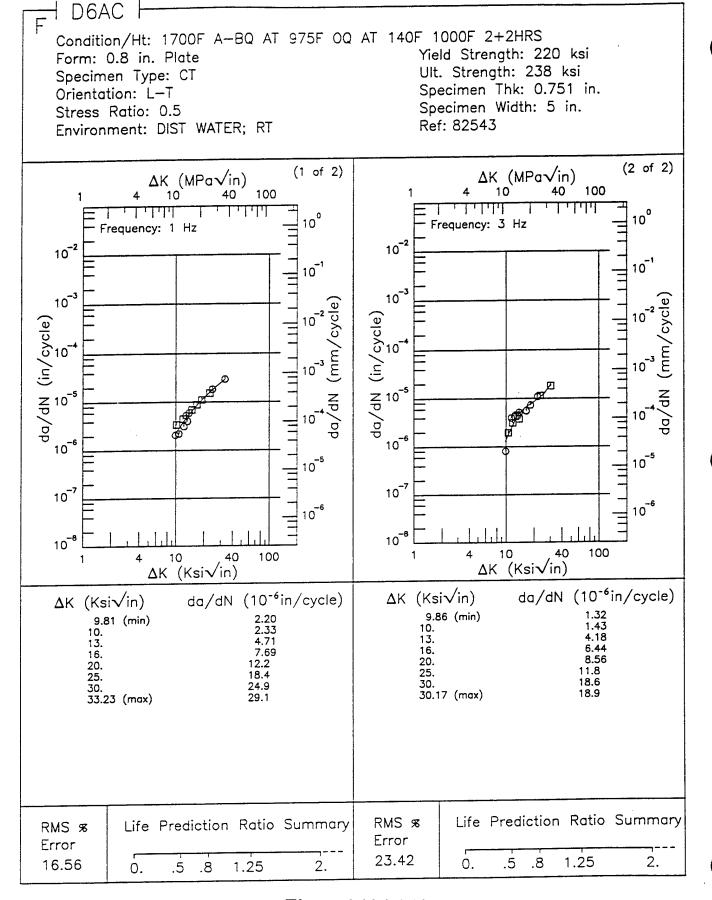


Figure 3.30.3.1.18

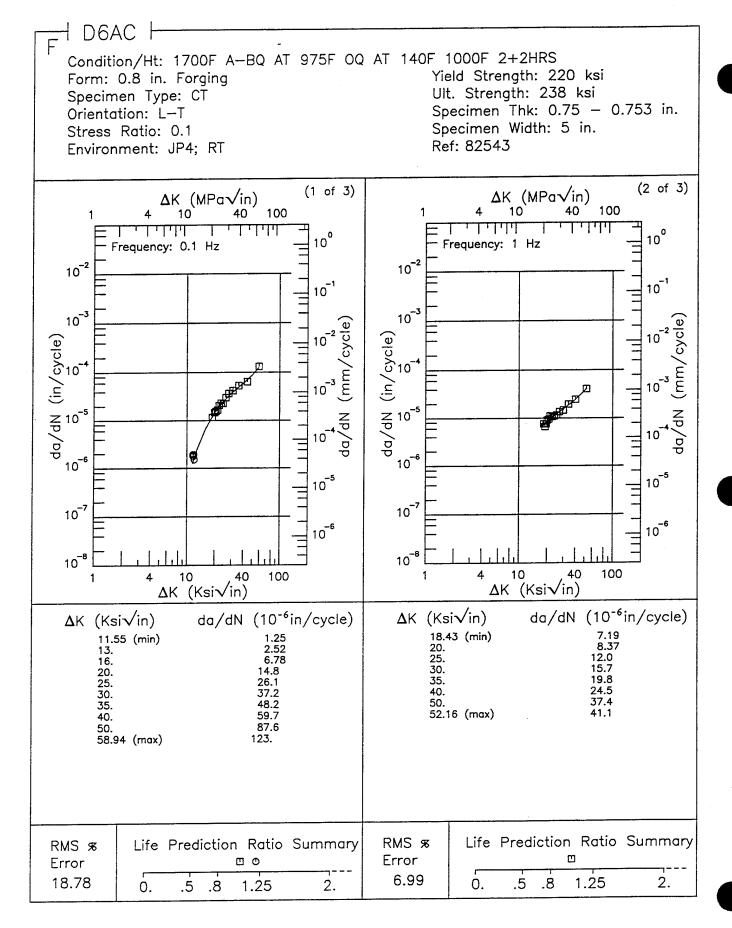


Figure 3.30.3.1.19

1 D6AC F Condition/Ht: 1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS Yield Strength: 220 ksi Form: 0.8 in. Forging Specimen Type: CT Ult. Strength: 238 ksi Orientation: L-T Specimen Thk: 0.75 - 0.753 in. Stress Ratio: 0.1 Specimen Width: 5 in. Ref: 82543 Environment: JP4; RT (3 of 3) $\Delta K (MPa\sqrt{in})$ $\Delta K (MPa\sqrt{in})$ 100 10 40 10 40 100 10° 10° Frequency: 3 Hz 10-2 10 -2 10-1 10-1 10⁻³ 10 da/dN (in/cycle) da/dN (in/cycle) 10⁻³ 10⁻⁶ 10-6 10 -5 10⁻⁵ 10⁻⁷ 10 -7 10 6 10 6 10 8 10⁻⁸ 4 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi \sqrt{in}) da/dN ($10^{-6}in/cycle$) da/dN (10⁻⁶in/cycle) 18.87 (min) 20. 25. 30. 50. 60. 70. 72.93 (max) 66.4 Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error 16.35 .5 .5 2. 0. .8 1.25 0. .8 1.25 2.

Figure 3.30.3.1.19 (Concluded)

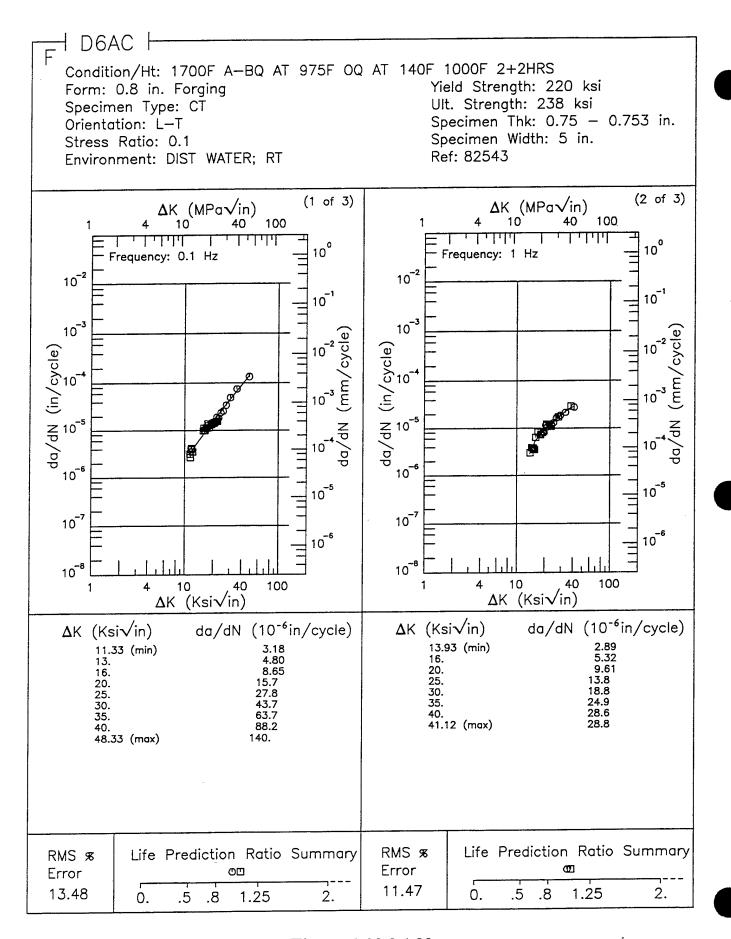


Figure 3.30.3.1.20

D6AC F Condition/Ht: 1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS Yield Strength: 220 ksi Form: 0.8 in. Forging Ult. Strength: 238 ksi Specimen Type: CT Orientation: L-T Specimen Thk: 0.75 - 0.753 in. Stress Ratio: 0.1 Specimen Width: 5 in. Environment: DIST WATER; RT Ref: 82543 (3 of 3) $\Delta K (MPa\sqrt{in})$ $\Delta K (MPa\sqrt{in})$ 100 100 40 10 40 11111 10° 10° Frequency: 3 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10-6 10⁻⁵ 10⁻⁵ 10⁻⁷ 10-7 10-6 10 -6 10-8 10⁻⁸ 10 40 10 40 100 100 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) Δ K (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) 5.90 6.68 18.38 (min) 20. 25. 30. 38.83 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error 15.42 0. .5 .8 1.25 2. .5 .8 1.25 2.

Figure 3.30.3.1.20 (Concluded)

H D6AC H Condition/Ht: 1700F A-BQ AT 975F OQ AT 140F 1000F 2+2HRS Yield Strength: 220 ksi Form: 0.8 in. Forging Ult. Strength: 238 ksi Specimen Type: CT Specimen Thk: 0.75 in. Orientation: L-T Specimen Width: 5 in. Stress Ratio: 0.48 Ref: 82543 Environment: DIST WATER; RT (1 of 1) $\Delta K (MPa\sqrt{in})$ $\Delta K (MPa\sqrt{in})$ 10 100 40 40 100 10° 10° Frequency: 1 Hz 10-2 10-2 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10⁻⁵ 10 -5 10⁻⁷ 10-7 10⁻⁶ 10 6 10-8 10 8 10 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 10.29 (min) 13. 16. 20. 25. 30. 35. 37.89 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error 1.25 2. .5 .8 19.65 1.25 0. .5 .8 2. 0.

Figure 3.30.3.1.21

TABLE 3.30.3.3

K_{Isce} SUMMARY FOR ALLOY STEEL D6AC

Condition	Dang	Test	9	Yield		S	Specimen	·		,	;	;	Test		
Heat Treat	Form	Temp (°F)	Or. (Ksi)	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)	Thk (in)	Crack (in)	Crack Ko K _{low} (in) (Ksivin) (Ksivin)	K _{low} (Ksi√in)	Time (min)	Test Date	Reference
1550° B 95min OO.					3N NaCl	CNT	2	0.05	0.08		ı	33*	1	1968	72283
850°F 1+1 hr	α	R.T.	R.T. L-T 224.7	224.7	Dist. Water	CNT	7	0.05	90.0	i	ŀ	33+	ļ	1968	72283
1550°F AQ; 650°F 4hr	S	R.T.	R.T. L-T 241.5	241.5	Dist. Water	CANT	0.75	0.165	0.16	1.0	61.7	4	i	1965	63061
1550°F AQ; 950°F 4hr	အ	R.T.	R.T. L.T 217.3	217.3	Dist. Water	CANT.	0.75	0.165	0.16	0.1	95.7	45.2	10000	1965	63061

* specimen thickness does not meet minimum requirements of 2.5 $(\frac{K_{loo}}{\sigma_{rr}})^2$

asterisk in specimen design column indicates that specimens are side-grooved

TABLE 3.31.1.2

FOR AK

FATIGUE CRACK GROW	GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOM HILL AT ROOM TEMPERATURE	OM TEM	EVELS O IPERAT	F STR	ESS IN	TENSI	TY FA	CI
ORIENTATION: L-T	: L-T		E	ENVIRONMENT: Lab Air	NMEN	T: Lab	Air	
			-		FICK	FCGR (10.8 in/cycle)	in/cyul	(0
CONDITION/ HEAT TREATMENT	PRODUCT FORM	Ħ	FREQ (Hz)		ΔI	AK Level (Kah/in)	(Ksivir	0
				2.5	5.0	10.0	20.0	8
		0.1	10				3.53	
		0.1	30			0.34	2.95	
AUSTENIZED & TEMPERED (TYS=220KSI)	ROUND BAR	0.5	10				4.94	
		0.5	30		0.09	0.72	4.93	

100.0

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Condition/Ht: AUSTENIZED & TEMPERED (TYS=220KSI) Yield Strength: 215.4 ksi Form: 3.18 in. Round Bar Ult. Strength: 258.1 ksi Specimen Type: CT Specimen Thk: 0.256 - 0.257 in. Orientation: L-T Specimen Width: 2.002 in. Frequency: 30 Hz Ref: DA001 Environment: LAB AIR; RT (2 of 2) (1 of 2) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 100 10 100 10 40 TTITI 10⁰ 11111 ليلتليا 10° Stress Ratio: 0.5 Stress Ratio: 0.1 10⁻² 10-2 10⁻¹ 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10⁻⁶ 10⁻⁵ 10⁻⁵ 10⁻⁷ 10⁻⁷ 10 -6 10 6 10 8 10⁻⁸ 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 3.07 3.5 0.0758 (min) 6.34 (min) 0.105 7. 8. 4. 5. 0.163 9. 10. 6. 7. 13. 9. 25. 30. 10. 13. 16. 35. 23.97 (max) 44.01 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error 14.13 2. 1.25 3.81 0. .5 .8 1.25 2. 0. .5 8.

H11

Figure 3.31.3.1.1

¹ H11 Condition/Ht: AUSTENIZED & TEMPERED (TYS=220KSI) Yield Strength: 215.4 ksi Form: 3.18 in. Round Bar Ult. Strength: 258.1 ksi Specimen Type: CT Specimen Thk: 0.257 - 0.488 in. Orientation: L-T Frequency: 7 Hz Specimen Width: 2 in. Environment: LAB AIR;650°F Ref: DA001 (1 of 2)(2 of 2) Δ K (MPa \sqrt{in}) $\Delta K (MPa\sqrt{in})$ 10 100 10 100 40 THI 11111 10° 10° Stress Ratio: 0.5 Stress Ratio: 0.1 10-2 10⁻² 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) 10-2 da/dN (in/cycle) 10 10-6 10-6 10⁻⁵ 10 -5 10⁻⁷ 10⁻⁷ 10-6 10⁻⁶ 10⁻⁸ 10⁻⁸ 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) $da/dN (10^{-6}in/cycle)$ ΔK (Ksi√in) ΔK (Ksi√in) 27.33 (min) 30. 35. 7.01 (min) 8. 7.00 8.83 1.03 1.17 1.36 13.1 9. 40. 10. 60. 70. 14.30 (max) 3.96 87.90 (max) RMS % Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary Error Error 6.97 11.25 1.25 0. .5 .8 1.25 2. 0. .5 .8 2.

Figure 3.31.3.1.2

Condition/Ht: AUSTENIZED & TEMPERED (TYS=220KSI) Yield Strength: 215.4 ksi Form: 3.18 in. Round Bar Ult. Strength: 258.1 ksi Specimen Type: CT Specimen Thk: 0.488 in. Orientation: L-T Specimen Width: 2.005 - 2.01 in. Frequency: 10 Hz Ref: DA001 Environment: LAB AIR; RT (2 of 2)(1 of 2) $\Delta K (MPa\sqrt{in})$ Δ K (MPa \sqrt{in}) 100 - 10 40 100 10 11111 10⁰ 11111 10° Stress Ratio: 0.5 Stress Ratio: 0.1 10-2 10-2 10-1 10 10⁻³ 10 da/dN (in/cycle) da/dN (in/cycle) با ق ا 10-6 10 -5 10 -5 10⁻⁷ 10-7 10⁻⁶ 10 -6 10-8 10⁻⁸ 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) ΔK (Ksi \sqrt{in}) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) 0.691 10.54 (min) 12.92 (min) 13. 0.949 1.41 2.66 0.970 13. 16. 16. 1.90 20. 20. 25. 30. 22.18 (max) 20.9 42.50 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % \Box Error Error 1.62 .5 .8 1.25 2. .5 0. 1.25 1.25 2. 0. .8

Figure 3.31.3.1.3

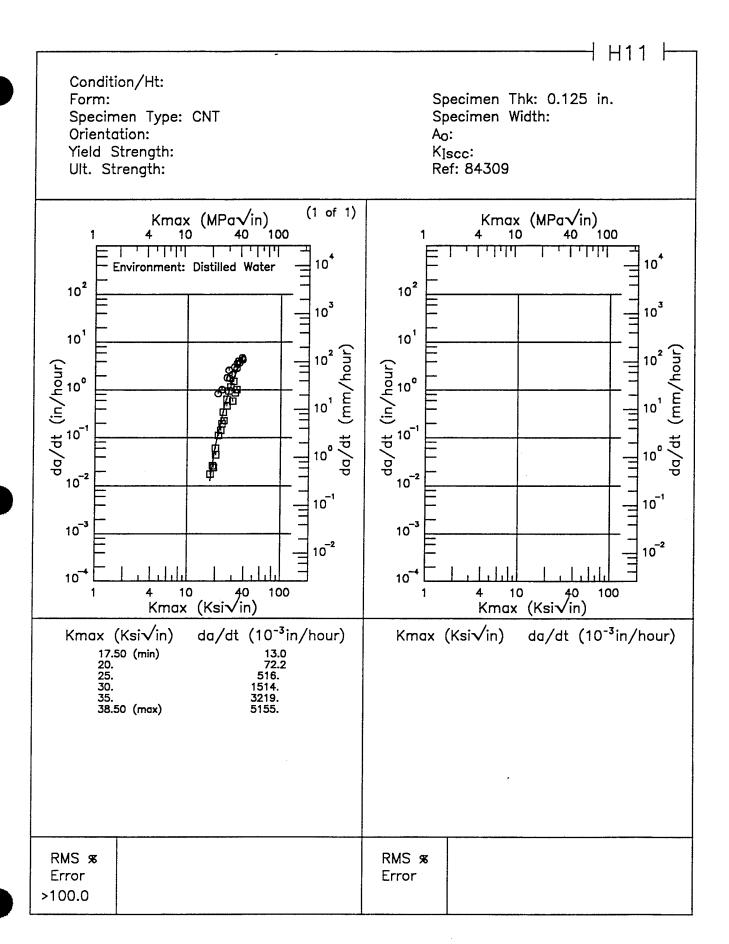


Figure 3.31.3.2.1

H11 Condition/Ht: Specimen Thk: 0.08 in. Form: Specimen Width: Specimen Type: CNT Ao: Orientation: Yield Strength: 230 ksi Kiscc: Ref: 75111 Ult. Strength: (2 of 2) (1 of 2)Kmax (MPa√in) Kmax (MPa√in) 100 10 10 40 1 1 1 1 1 1 1 1 ابليليك 1.1111110⁴ **Environment: Distilled Water** Environment: Argon 100% R.H. 10² 10² 103 103 101 10¹ 102 10² (mm/hour) da/dt (in/hour) da/dt (in/hour) 10 10° 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ 10-2 10-2 10 10 4 10 40 Kmax (Ksi√in) 10 100 100 Kmax (Ksi√in) $da/dt (10^{-3}in/hour)$ Kmax (Ksi√in) Kmax (Ksi√in) $da/dt (10^{-3}in/hour)$ 18.10 (min) 20. 25. 27.40 (max) 35.8 67.9 22.50 (min) 25. 30. 1191. 2363. 708. 1175. 3685. 37.00 (max) 4333. RMS % RMS % Error Error 18.61 20.66

Figure 3.31.3.2.2

TABLE 3.31.3.3

Klsce SUMMARY FOR ALLOY STEEL H11

,	r - G	Test	2	Yield		SZ.	Specimen		Prod	,	ŀ	;	Test	1	
Heat Treat	Form	Temp Or. Str (°F) Or. (Ksi)	opec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)	ľhk (in)	Crack (in)	Crack Ko K _{loo} (in) (Ksivin) (Ksivin)	K _{leo} (Ksi√in)	Time (min)	Test Date	Reference
1325°F;	٥	ΕĐ		טטב כ	Dist Water	CNT	2	0.08	80.0	i	***	35*	4000	1968	72283
1060°F 2+2hr	מ	P. T.	l	2007	3N NaCl	CNT	83	0.05	0.08	ł	:	28	20000	1968	72283
Quenched + Tempered at 1100°F	Ъ	R.T.	:	188	3.5% NaCi		1.5	0.48	0.48	i	54	30	i	1971	84351

* specimen thickness does not meet minimum requirements of 2.5 $(\frac{K_{loo}}{\sigma_{ys}})^2$

TABLE 3.32.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL HP 9-4-.20 AT ROOM TEMPERATURE

					K_{Ic}	$K_{Ic}~(ksi\!\sqrt{in})$	<u>(c</u>			
Product Form	Condition/Heat Treatment			S	pecime	Specimen Orientation	itation			
			L-T			T-L			S-L	
		Mean K _{le}	Std Dev	п	Mean K _{le}	Std Dev	п	Mean K _{te}	Std Dev	а
Ī	1650F 1-2HR AC 1-2HR 1-2HR AC -100F 1.5HR 1025F 4HR 1060F 4HR	123.5	12.	2	:		i	·	i	ı
Plate	1650F 1-2HR AC 1625F 1-2HR OQ -100F 2HR 1025F 4-6HR	121.6	29.	2				i	:	:
	1525F OQ -100F 1HR 1065F 4+4HR	i	:	:	111.7	2.	2	:		:
	1650F 1-2HR AC 1626F 1-2HR OQ -100F 1-2HR 1026F 4HR	134.8	12.3	5	109.7	4.7	3			
	1650F 1-2HR AC 1525F 1-2HR OQ -100F 2HR 1025F 4-6HR	135.2	11.6	15	125.3	1.8	6	:	••	i
Forging	1650F 1-2HR AC 1525F 1-2HR OQ -100F 2HR 1050F 4-6HR	133.2	3.9	מי	i	i	i	:	:	:
	1650F 1.2HR ACX	125.5	3.5	2	i	i	ŀ	I	:	
	1650F 2HR AC 1525F 2HR OQ 1000F 2+2HR AC	94.4	4.4	83	ŀ	:	:	1	:	:
	1650F 4.5HR AC TO 900F HELD 0.5HR AC -100F 1.5HR 1025F 8HR A-BQ	128.5	0.7	. 63	:	I	ŀ	ŀ	ŀ	

TABLE 3.32.1.1 (CONCLUDED)

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL HP 9-4-.20 AT ROOM TEMPERATURE

	-				K_{Ic}	$K_{lc}~(ksi\!\sqrt{in})$	<u>a</u>		·	
Product Form	Condition/Heat Treatment			62	pecime	Specimen Orientation	ntation			
			L-T			T-L			S-L	
		Mean K _{Ie}	Std Dev	q	Mean K _{io}	Std Dev	Ħ	Mean K _{te}	Std Dev	u
	1700F 4.5HR AC 1700F 1.5HR AC -100F 1.5HR 1025F 4HR	140.5	0.7	2	•	i		!	i	l
Forging	ANNEALED	120.6	7.3	12	117.7	1.9	3	i	;	:
(Cont.d)	HEAT TREATED	140.7	4.5	10	132.3	9.9	7	:	:	:
	Unspecified	150.6	4.5	2	136.3	16.8	2	1	;	:

TABLE 3.32.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4.20 AT ROOM TEMPERATURE

ORIENTATION	ON: L-T	ପ	ENVIRONMENT: 100% Relative Humidity	MENT	: 100%	Relati	ve Hun	nidity
CONDITION	PRODUCT		FREG		FC	<i>CZR</i> (10	FCGR (10 ^d in/cycle)	le)
HEAT TREATMENT	FORM	Ħ	(HZ)		ΔJ	T Lovel	AK Lovel (Kek/in)	1)
				2.3	5.0	10.0	20.0	50.0
	PLATE	0.08	1			0.93	6.26	
		0.08	0.1				6.63	38.47
1525F 2HRS AC -100F 2HRS 1025F 4HRS		0.08	1			0.65	6.45	42.25
	BILLET	0.3	1			0.98	8.45	
		0.5	1			1.51	8.02	

100.0

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK

		100.0	
		1)	39.67
	NaCl	FCGR (10 ⁶ in/cycle) AK Level (Kst/in) 10.0 20.0 1	
	3.5%	GR (10 ⁻	
	ENVIRONMENT: 3.5% NaCl	PCG AK	
ATURE	WIRO	2.5	
EMPER.	E	FREQ. (Hz)	-
T MOO		R	0.02
HP9-420 AT ROOM TEMPERATURE	: L-T	PRODUCT	BAR
	ORIENTATION: L-T	CONDITION/ HEAT TREATMENT	UNSPECIFIED

TABLE 3.32.1.2.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4.20 AT ROOM TEMPERATURE

80.0 **6**4 PCGR (10⁻⁸ in/cycle) **ENVIRONMENT: Distilled Water** ΔK Level (Ksiy/in) 98 8.73 10.0 9. 8) 10 FREQ (Hz) 0.1 0.08 Ľ PRODUCT FORM PLATE ORIENTATION: L-T 1525F 2HRS AC -100F 2HRS 1025F 4HRS HEAT TREATMENT CONDITION

100.0 253.71

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.20 AT ROOM TEMPERATURE

ENVIRONMENT: L.H.A.

Tre Craff Chieve	my and white		S. C. C. C. C. C. C. C. C. C. C. C. C. C.		MC	FCGR (10 ⁴ in/cycle)	8 in/cyc	(9)	
HEAT TREATMENT	FORM	R	(HZ)		A.	ΔK Level (Ksi\/in)	(Keivin	3	
				2.5	5.0	10.0	20.0	60.0	100.0
	PLATE	80.0	9			0.87	4.85	29.81	
		0.05	1				6.9	32.1	
		0.08	0.1				4.54	33.59	
1525F 2HRS AC -100F 2HRS 1025F 4HRS	RA T IIG	90:0	8				4.31	37.22	250.39
	BLALET	90:0	6		0.13	0.78	68.9		
		0.6	9			0.82			
		7.0	9			1.27	8.13		
		90'0	1				0.43	21.26	
WELDED	WELDMENT	0.3	9				1.01	29.54	
		0.5	8				5.24	50.6	

TABLE 3.32.1.2.5

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.20 AT ROOM TEMPERATURE

ENVIRONMENT: S.C.S.

			7	
		0.001	125.87	
		× 3	12	
		20.0 50.0		
		9	18.9	33.15
_		2	18	33.
9				
FCGR (10 ⁻⁸ in/cycle)	AK Lovel (Ksk/in)			
	2			_
S	.9		1.61	3.58
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NDTITION/	TREATMENT			UNSPECIFIED
20NDITION/	AT TREATMENT			UNSPECIFIED
CONDITION	SAT TREATMENT			UNSPECIFIED
CONDITION	IEAT TREATMENT			UNSPECIFIED
CONDITION/	HEAT TREATMENT			UNSPECIFIED
CONDITION	HEAT TREATMENT			UNSPECIFIED

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.20 AT ROOM TEMPERATURE

ENVIRONMENT: S.C.S.

		ŀ
	₩.₹	
	100.0	
1 1	-	
1	****	
	50.0	
	₩₹	

9 4	******	
8 >	20.0	
2 5	₩.₩	5.71
	₩-8	10

FCGR (10 ⁻⁸ in/cycle) AK Level (Ksi/in)		
0 6	10.0	
- 4	₩₩	
)	₩ ₩	9.0
2	₩=#	0

0 9	*****	

7		
	2.5 5.0	

FREQ (Hz)		
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RODUC		BILLET
PRODUC		BILLET
PRODUCT		BILLET
PRODUC		
CONDITION/ PRODUC HEAT TREATMENT FORM		
		1525F 2HRS AC -100F 2HRS 1025F 4HRS BILLET

TABLE 3.32.1.2.7

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.20 AT ROOM TEMPERATURE

	100.0	202.47
	80.0	30.66
Α.	d in/cycle I (Ksi/in	
ENVIRONMENT: S.S.W.		
MENI	FCGF AK	
IRON	_	
ENA	878	
	FREQ (Hz)	0.1-15
	R	0.02
	RODUCT	FORGING
÷	PRODU	FOR
ORIENTATION: L-T		
TLATI	N/ HENT	
ORIEL	CONDITION/ HEAT TREATMENT	UNSPECIFIED
	CONI	UNS
	HE	

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK

100.0 60.0 PCGR (10⁻⁸ in/cycle) AK Level (Ksivin) 20.0 6.94 5.26 ENVIRONMENT: S.T.W. 10.0 0.74 8 HP9-4-.20 AT ROOM TEMPERATURE 9 9 FREQ (Hz) 90.0 0.08 × PRODUCT FORM BILLET PLATE ORIENTATION: L-T 1525F 2HRS AC -100F 2HRS 1025F 4HRS HEAT TREATMENT CONDITION

TABLE 3.32.1.2.9

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.20 AT ROOM TEMPERATURE

CONDITION/ CONDITION/ HEAT TREATMENT	PRODUCT FORM	R	FREQ.	INVIRO	ENVIRONMENT: L.H.A. FCGR (10 d in AK Lovel (K) 10.0 20	AENT: L.H.A. PCCR (10 ⁶ in/cycle) AK Level (Ksi/in) 100 200 6	9 8 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0.0	100.0
1525F 2HRS AC -100F 2HRS 1025F 4HRS		0.05	1					29.83	
	BILLET	0.08	9				4.85		

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4.20 AT ROOM TEMPERATURE

PCGR (10 ⁶ in/cycle) ΔK Level (Kek/in) 20.0 2.99 **ENVIRONMENT: Lab Air** 10.0 0.24 6.0 27 84 FREQ (Hz) 0.1-200.02 × PRODUCT FORM FORGING ORIENTATION: T-L HEAT TREATMENT CONDITION UNSPECIFIED

100.0

30.69

TABLE 3.32.1.2.11

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.20 AT ROOM TEMPERATURE

	0.001	319.63
	(6)	31.39 31
	(cycle)	
S.W.	0-6 in/cycl rel (Ksk/in	2.41
S.L.S	FCGR (10 ⁻⁸ in/cycle) ΔK Level (Ksi/in)	
ONIME	FR A	
ENVIRONMENT: S.S.W.	9	
_	FREQ (Hz)	0.1-15
	Ħ	0.02
	CT	
	PRODUCT	FORGING
√: T-Γ	PJ	
ORIENTATION: T-L	NI	
LIENT	CONDITION/ HEAT TREATMENT	FIED
OF	ONDE	UNSPECIFIED
	C. HEAT	

TABLE 3.32.2.1

				7	ALLOY STEEL	STEEL	НР 9-4-20		$\mathbf{K_{Io}}$	·					
	PROI	PRODUCT				a.	SPECIMEN	7	CRACK			K _{Io}			
CONDITION	FORM	THICK (In.)	TEST TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (in.) W	THICK (in.) B	DESIGN	LENGTH (ln.) A	(K _{e,} TYS)* (in.)	K. (Kei • √in.)	K. MEAN	STAN	DATE	RRFER
	ŗ	1.25	E		196.5	3.995	2.000	CT	2.065	1.63	153.80			1977	MA005
:	Forging	1.25	i.	1	196.5	4.002	2.000	cr	2.118	1.40	147.39	150.6	4.5	1977	MA005
	ŗ	1.25	E		198.0	4.000	1.998	CT	2.068	1.39	148.10			1977	MA005
	Forging	1.26	K.T.	T-I	198.0	3.997	2.000	cr	2.070	0.98	124.40	136.3	16.8	1977	MA005
1525F OQ ·100F 1HR		4.00	į		179.0	3.996	1.497	CT	2.003	0.96	110,30			1974	90012
1065F 4+4HR	Forging	4.00	KT.	J.	179.0	3.995	1.498	CT	2.030	1.00	113.10	111.7	2.0	1974	90012
		3.25			184.0	6.248	1.506	CT	2.543	1.42	139.00			1973	86428
		3.00		I	186.0	4.495	1.505	CT	2.277	1.26	132.00			1973	86428
1650F 1·2 HR AC 1625F 1·2 HR OQ ·100F 2 HR 1050F 4·6 HR	Forging	3.25	R.T.	5	189.0	4.499	1.602	CT	2.275	1.17	129.00	133.2	3.9	1973	86428
		3.25			189.0	6.246	1.611	CT	2.563	2.50	131.00			1973	86428
		3.25			190.0	4.500	1.601	CT	2.287	1.26	135.00			1973	86428
1650F 1-2HR AC 1626F 1-2 HR AC -100F 1-2 HR 1026F 4 HR	Forging	3.70	26	7.7	190.0	6.000	2.000	СŢ		1.84	163.00	ı		1974	90011
1650F 1-2HR AC 1526F 1-2 HR AC -100F 1-2 HR 1026F 4 HR	Forging	3.70	36	T·L	190.0	6.000	2.000	СŢ	:	1.21	132.00	I		1974	90011
		7.00			190.0	6.63	1.995	cr	2.987	1.50	147.00			1973	85836
		4.00		1	190.0	5.997	1.752	CT	3.044	1.02	121.00			1973	85836
1650F 1-2HR AC 1625F 1-2 HR AC -100F 1-2 HR 1025F 4 HR	Forging	4.00	R.T.	7	190.0	6.999	1.756	CT	3.064	1.04	122.00	134.8	12.3	1973	85836
		7.00		1	190.0	900.9	1.997	СŢ	2.981	1.37	141.00			1973	85836
		7.00			190.0	6.002	1.991	CT	2.979	1.42	143.00			1973	85836
		4.00			190.0	900.9	1.757	CT	3.077	08.0	108.00			1973	85836
1650F 1-2HR AC 1625F 1-2 HR AC -100F 1-2 HR 1025F 4 HR	Forging	4.00	R.T.	T.L	190.0	6:68	1.765	CT	3.071	0.78	106.00	109.7	4.7	1973	85836
		7.00			190.0	6.005	1.992	CI	3.006	0.92	115.00			1973	85836

TABLE 3.32.2.1 (CONTINUED)

		DATE REFER	1974 90011	1974 90011	1974 90011	1973 85836	1973 85836	1974 80011	1974 90011	1974 90011	1974 90011	1974 90011	1974 90011	1974 90011	1974 90011	1974 90011	1974 90011	1972 84306	1974 90011	1973 85836
		STAN		12.0	i		3.5	i			9.2				6.1			29.0	•	ı
	K _{Ic}	K. MEAN		123.5	ı		125.5	i			100.4				97.3			121.6	1	1
		K. (Kal *	132.00	115.00	128.00	123.00	128.00	139.00	91.00	107.00	90'06	105.00	109.00	104.00	92.00	96.00	101.00	142.00	116.00	127.00
		2.0 (K., TYS)* (in.)	1.22	0.92	1.16	1.10	1.19	1.34	19:0	0.75	0.53	0.72	0.78	0.71	0.56	09:0	0.71	1.63	0.97	1.12
$\mathbf{K}_{\mathbf{I}\sigma}$	CRACK	LENGTH (in.) A			:	2.987	2.996	:	**	:	:	į	:	:		-	:	2.905	I	2.991
l	7	DESIGN	cr	CT	CT	cr	CT	CT	CT	CT	CT	CT	CT	CT	CT	CT	CT	CT	CT	CT
HP 9-4-20	SPECIMEN	THICK (in.) B	2.000	2.000	2.000	1.685	1.546	2.000	2.000	2.000	2.000	2.000	2.000	2.000	2.000	2.000	2.000	2.002	2.000	1.507
STEEL	W 2	WIDTH (In.)	6.000	6.000	6.000	900.9	6.007	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.997
ALLOY STEEL		YIELD STR (Kal)	189.0	189.0	189.0	185.0	185.0	190.0	195.0	195.0	195.0	195.0	195.0	195.0	195.0	195.0	189.0	190.0	186.0	190.0
,		SPEC	E	1.51	T.L	9	1.5	LT			፤				T-L		Ē	\$	T.L	LT
		TEST TEMP (°F)	E	R.I.	R.T.	Ę	R. I.	R.T.			28				99-		Ē	i.i.	R.T.	99-
	UCT	THICK (in.)	2.50	2.50	2.50	4.00	4.00	3.00	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.60	3.70
	PRODUCT	FORM	170	riate	Plate	1	Forging	Forging			Plate				Plate		Ē		Plate	Forging
		CONDITION	1650F 1-2HR AC 1-2 HR AC	1060F 6 HR	1650F 1-2HR AC 1-2 HR AC -100F 1.5 HR 1026F 4 HR 1060F 6 HR	1650F 1.2HR AC 1.5 HR OQ	1025F 12 HR	1650F 1-2HR AC 1626F 1-2 HR OQ -100F 2 HR 1000F 4-6 HR			1650F 1-2HR AC 1526F 1-2 HR OQ -100F 2 HR 1026F 4-6 HR				1650F 1-2HR AC 1626F 1-2 HR OQ -100F 2 HR 1026F 4-6 HR		1650F 1-2HR AC 1525F 1-2 HR 0Q	-100F 2 HR 1025F 4·6 HR	1650F 1.2HR AC 1625F 1.2 HR OQ -100F 2 HR 1025F 4.6 HR	1650F 1-2HR AC 1626F 1-2 HR OQ -100F 2 HR 1025F 4-6 HR

TABLE 3.32.2.1 (CONTINUED)

					ALLOY STEEL	STEEL	HP 9-420		K _{Io}						
	PR0	PRODUCT					SPECIMEN	7	CRACK			K _{Ic}			
CONDITION	FORM	THICK (tn.)	TEST TEMP (°F)	SPEC	YIELD STR (Kal)	WIDTH (in.) W	THICK (in.) B	DESIGN	LENGTH (in.) A	(K _e ,/TY8)* (in.)	K. (Kel • (m.)	K. MBAN	STAN	DATE	REFER
		4.00			186.0	6.000	2.010	CT	2.986	1.27	136.00			1973	85836
		4.00			186.0	6.998	2.010	CT	2.975	1.42	143.00			1973	85836
		4.00		_	186.0	6.002	2.010	CT	2.985	1.28	136.00			1973	85836
		4.00			186.0	6.000	2.005	CT	2.964	1.36	140.00			1973	85836
		4.00			186.0	6.003	2.010	CT	2.963	1.32	138.00			1973	85836
		4.00			186.0	6.005	2.010	CT	2.984	1.32	138.00			1973	85836
		4.00			188.0	6.000	2.000	CT		1.90	164.00			1974	11006
1650F 1-2HR AC 1525F 1-2 HR OQ -100F 2 HR 1025F 4-6 HR	Forging	4.00	R.T.	LT	194.0	4.014	1.506	CT	1.967	1.33	141.00	135.2	11.6	1972	84306
		4.00			194.0	4.000	1.635	CT	1.970	1.39	142.00			1972	84306
		4.00			194.0	3.994	1.598	ст	2.366	1.26	135.00			1972	84306
		4.00			198.0	5.000	2.000	CT	1	0.84	115.00			1974	11006
		4.00			198.0	6.000	2.000	cr		0.83	121.00			1974	11006
		4.00			198.0	6.000	2.000	cr	I	96.0	123.00			1974	11006
		4.00			198.0	6.000	2.000	СT	:	1.01	126.00		,	1974	11006
		4.00			198.0	6.000	2.000	CT.	:	1.08	130.00			1974	11006
		4.00			190.0	6.000	2.011	СT	2.977	1.11	126.00			1973	85836
		4.00			190.0	900.9	2.006	C.	2.970	1.10	126.00			1973	85836
1650F 1-2HR AC 1525F 1-2 HR OQ	· •	4.00	Ę	Ē	190.0	6.002	2.004	cr	2.963	1.11	127.00			1973	85836
-100F 2 HR 1026F 4-6 HR	80 18 10 4 10 18 10 4	4.00	į	1	190.0	6.002	2.010	CT	2.961	1.03	122.00	125.3	1.8	1973	85836
		4.00			190.0	6.005	2.010	ст	2.969	1.11	126.00			1973	85836
		4.00			194.0	4.013	1.506	СТ	1.991	1.07	125.00			1972	84306

					ALLOY 8	STEEL	HP 9-420		K _{lo}						
	PROI	PRODUCT				8	SPECIMEN		CRACK			K			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIRLD STR (Kai)	WIDTH (fn.)	THICK (in.) B	DESIGN	LENGTH (in.) A	2.0 (K _{e.} /TYS)* (in.)	K. (Kel • √In.)	K. MEAN	STAN	DATE	RRFER
1650F 1-2HR AC 1525F 1-2 HR OQ	į	4.00	E	E	190.0	3.003	1.632	CT	1.496	0.89	114.00			1973	85836
-100F 2 HR 1025F 4-6 HR	rorgnig	. 4.00	K.T.	J.	190.0	3.005	1.630	CT	1.484	0.93	116.00	115.0	1.4	1973	85836
1650F 1-2HR AC 1625F 1-2 HR OQ	£	4.00	8		190.0	9.000	1.740	CT	2.983	1.01	121.00			1973	85836
·100F 2 HR 1025F 4·6 HR	Forging	4.00	28	1.1	190.0	6.000	1.743	CT	2.971	1.19	131.00	126.0	7.1	1973	85836
1650F 1-2HR AC 1626F 1-2 HR OQ -100F 2 HR 1026F 4-6 HR	Forging	4.00	82	T.T	185.0	6.001	1.752	CT	3.000	96.0	114.00	;	ı	1973	85836
1650F 1-2HR AC 1525F 1-2 HR OQ -100F 2 HR 1050F 4-6 HR	Forging	1.70	R.T.	T-L	190.0	6.260	1.501	СТ	2.628	1.43	143.00	ŀ	i	1973	86428
		4.00		•	186.0	2.510	1.247	CT	1.146	09:0	91.10			1974	88136
1650F 2HR AC 1525F 2 HR OQ 1000F 2+2 HR AC	Forging	4.00	R.T.	LT	186.0	2.523	1.244	CT	1.136	0.72	99.40	94.4	4.4	1974	88136
		4.00			186.0	2.516	1.240	CT	1.171	0.63	92.80			1974	88136
1650F 4.5HR AC TO 900F HELD	j j	4.00	E	E	185.0	6.004	1.609	CT	3.020	1.19	128.00			1973	85836
1025F 8HR A-BQ	rorging	4.00	R.I.	15	185.0	6.000	1.590	CT	3.031	1.22	129.00	128.5	0.7	1973	85836
1700F 4.5HR AC 1700F 1.5HR AC	į.	4.00	E	E	185.0	6.003	1.596	CT	3.006	1.45	141.00			1973	85836
-100F 1.5 HR 1025F 4 HRS	rorging	4.00	I. I.	5	185.0	6.005	1.605	CT	3.031	1.43	140.00	140.5	0.7	1973	85836
		3.00			189.0	2.003	0.997	cr	1.041	0.80	107.30			1977	NC001
		3.00			189.0	3.000	0.998	CT	1.522	0.94	116.10			1977	NC001
		3.00			189.0	4.005	2.001	cr	2.049	1.00	120.00			1977	NC001
GAIVEN	2	3.00	Đ	£	189.0	4.009	1.504	CT	2.038	1.15	128.39			1977	NC001
	8 m8 m8	3.00	į	\$	189.0	2.000	0.998	CT	1.037	0.94	116.00	120.6	7.3	1977	NC001
		3.00			189.0	3.001	1.503	CT	1.631	0.97	118.30			1977	NC001
		3.00			189.0	4.005	2.001	CT	2.068	96.0	117.69			1977	NC001
		3.00			189.0	4.000	1.505	CI	2.033	0.99	119.19			1977	NC001

TABLE 3.32.2.1 (CONCLUDED)

					ALLOY STEEL	STEEL	HP 9-420	1	K _{io}						
	PROI	PRODUCT					SPECIMEN	z	CRACK			K _{Io}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Ket)	WIDTH (in.)	THICK (in.)	DESIGN	LENGTH (in.)	(K _n /TY8) ² (in.)	K. (Kei • (In.)	K. MEAN	STAN	DATE	REFER
		3.00			189.0	3.000	1.504	CT	1.629	0.93	115.40			1977	NC001
ANNEALED	Forging	3.00	R.T.	7	192.0	3.995	2.000	CT	2.033	1.19	132.50	;	;	1976	NC001
Cont'd	Cont'd	3.00	Cont'd	Cont'd	192.0	3.996	1.999	CT	2.013	1.13	129.30	Cont'd	Cont'd	1976	100DN
		3.00			192.0	3.992	2.000	CT	2.069	1.09	127.30			1976	100DN
		3.00			190.0	3.998	2.000	CT	2.012	96'0	118.30			1976	100DN
ANNEALED	Forging	3.00	R.T.	1.	190.0	3.998	2.000	CT	2.028	0.92	115.60	117.7	1.9	1976	NC001
		3.00			190.0	3.995	2.000	CT	2.080	0.98	119.30			1976	1000N
		3.40			185.0	4.003	1.601	CT	1.954	1.33	135.00			1973	85879
		4.00			189.0	4.000	1.503	CT	2.037	1.48	145.00			1973	85633
		4.00			190.0	3.980	1.505	CT	2.039	1.35	139.00			1973	85633
		4.00			190.0	3.999	1.504	CT	2.030	1.45	145.00			1973	85633
CITED A COUNTY OF A COUNTY		4.00	į		190.0	3.971	1.506	CT	2.049	1.35	139.00			1973	85633
HEAT TREATED	Forging	4.00	H.T.	<u>.</u>	190.0	3.995	1.504	cr	2.036	1.34	139.00	140.7	3.	1973	86633
		4.00			191.0	4.000	1.504	CT	2.026	1.30	138.00			1973	86633
		4.00			192.0	4.004	1.503	CT	2.031	1.30	138.00			1973	85633
		4.00			192.0	4.002	1.504	CT	2.034	1.33	139.00			1973	85633
		7.00			198.0	3.990	1.511	CT	2.063	1.46	150.00			1973	85857
		6.60			186.0	3.984	1.499	CT	2.026	1.46	142.00			1973	86867
		3.40			187.0	4.004	1.502	CT	2.011	1.22	131.00			1973	85879
		3.40		•	187.0	4.000	1.501	CT	1.985	1.22	131.00			1973	85879
HEAT TREATED	Forging	3.40	R.T.	15	190.0	4.005	1.499	cr	2.021	1.36	140.00	132.3	9.9	1973	85879
		3.40			196.0	4.002	1.484	CT	2.054	1.12	131.00			1973	85857
		7.00		•	198.0	3.986	1.607	CT	2.038	1.07	128.00			1973	85857
		7.00			198.0	3.989	1.464	CT	2.033	0.97	123.00			1973	85857

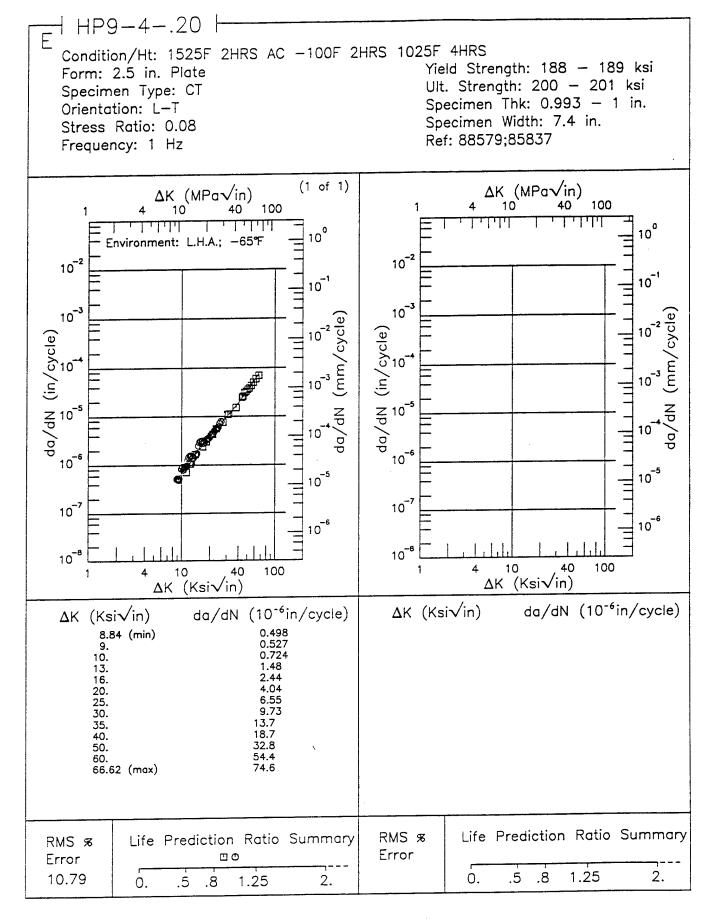


Figure 3.32.3.1.1

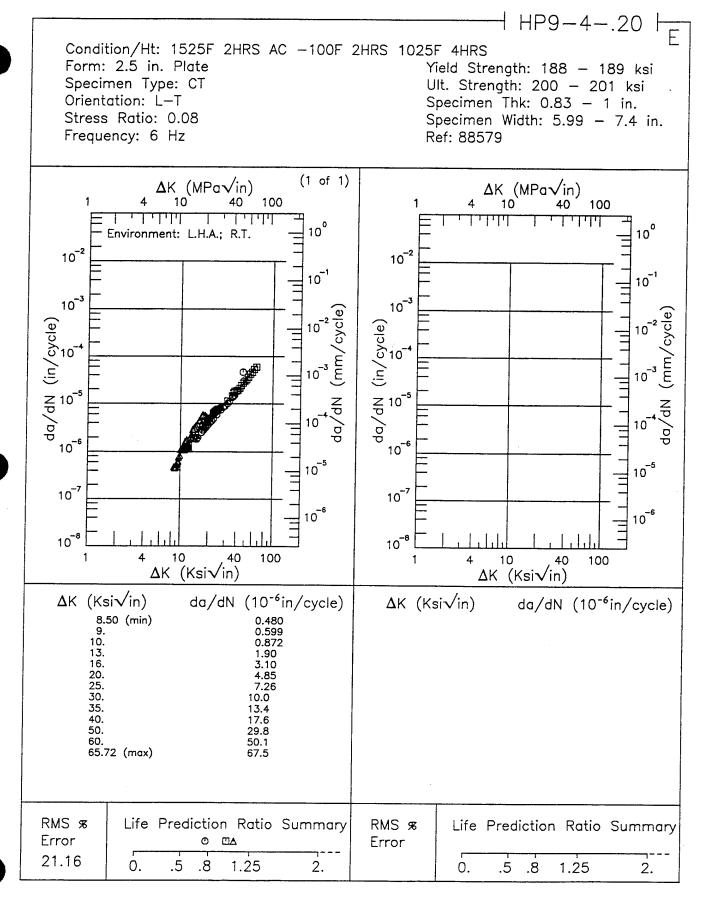


Figure 3.32.3.1.2

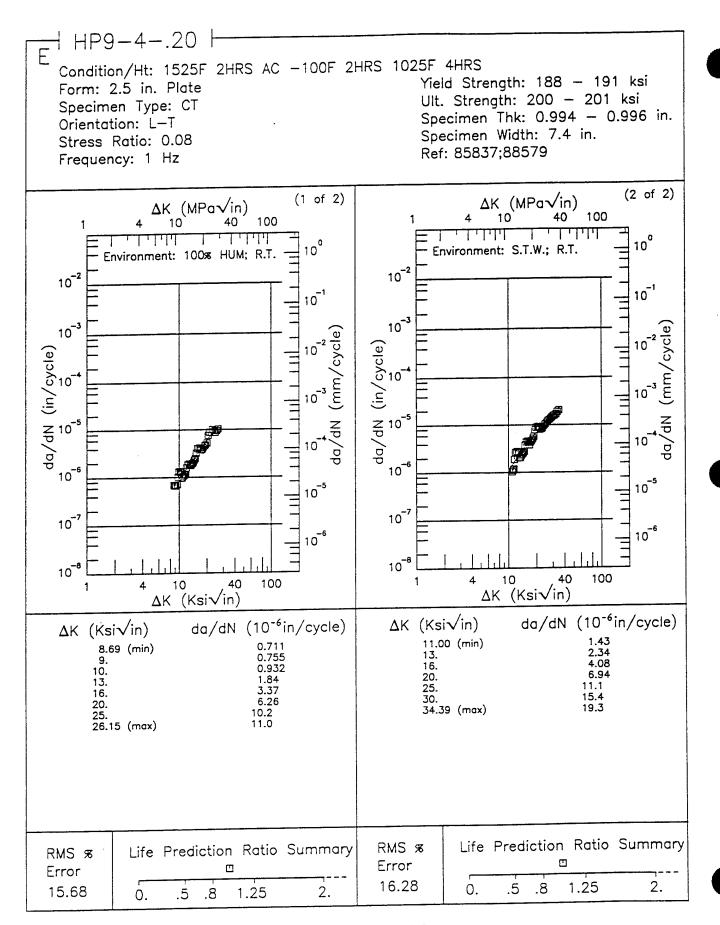


Figure 3.32.3.1.3

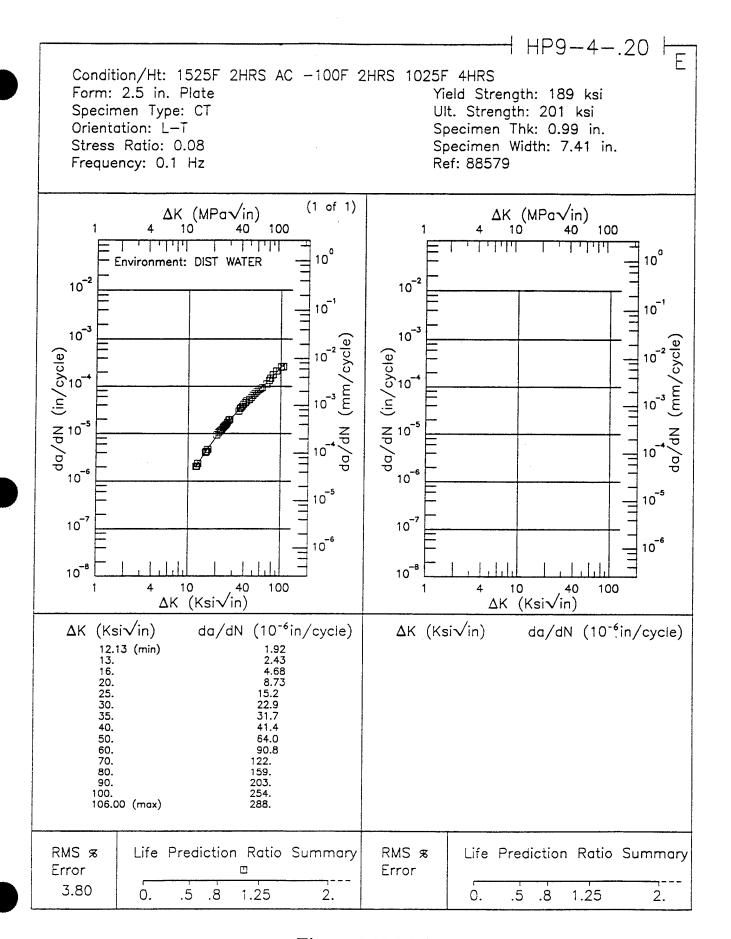


Figure 3.32.3.1.4

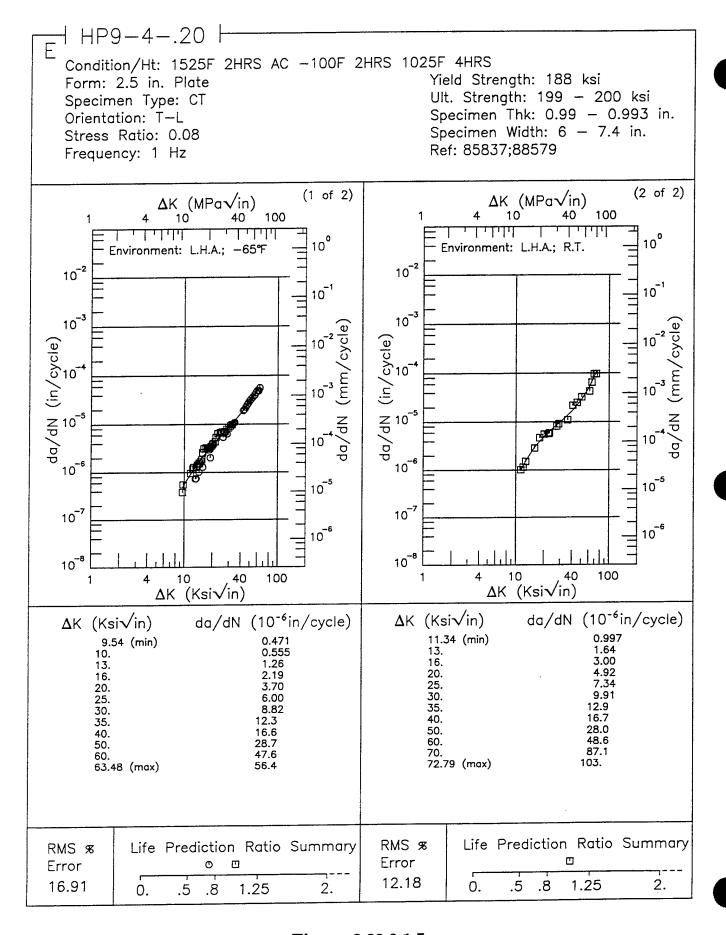


Figure 3.32.3.1.5

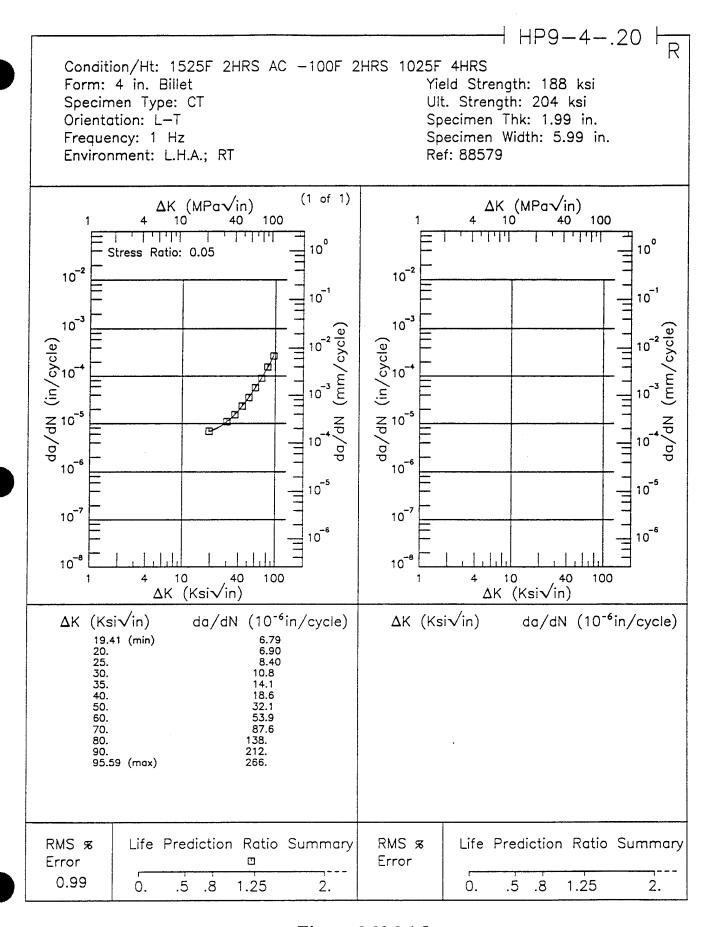


Figure 3.32.3.1.6

HP9-4-.20 Condition/Ht: 1525F 2HRS AC -100F 2HRS 1025F 4HRS Yield Strength: 189 ksi Form: 4 in. Billet Ult. Strength: 203 ksi Specimen Type: CT Specimen Thk: 0.986 - 0.987 in. Orientation: L-T Specimen Width: 7.4 in. Frequency: 1 Hz Ref: 85837 Environment: 100% HUM; RT (2 of 2)(1 of 2)ΔK (MPa√in) Δ K (MPa \sqrt{in}) 100 10 100 11111 10° 10° Stress Ratio: 0.5 Stress Ratio: 0.3 10-2 10 -2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10-6 10 -5 10 -5 10 -7 10⁻⁷ 10-6 10 6 10 8 10 40 100 10 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) $da/dN (10^{-6}in/cycle)$ ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) 6.77 (min) 7. 8. 0.631 0.674 0.893 7.60 (min) 0.331 8. 0.408 9. 0.980 9. 10. 10. 13. 16. 16. 20. 25. 27.39 (max) 20. 23.21 (max) 10.7 14.2 Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error

Figure 3.32.3.1.7

2.

19.90

.5 .8

0.

1.25

18.07

0.

.5 .8

1.25

2.

H HP9-4-.20 H Condition/Ht: 1525F 2HRS AC -100F 2HRS 1025F 4HRS Yield Strength: 186 - 189 ksi Form: 4 in. Billet Ult. Strength: 203 - 211 ksi Specimen Type: CT Specimen Thk: 0.991 - 0.997 in. Orientation: L-T Specimen Width: 6 - 6.01 in. Frequency: 6 Hz Environment: L.H.A.; RT Ref: 85837 (2 of 2) (1 of 2) $\Delta K (MPa\sqrt{in})$ $\Delta K (MPa\sqrt{in})$ 10 100 10 40 100 11111 111111 1,1,1,1 11111 10° 10° Stress Ratio: 0.7 Stress Ratio: 0.5 10-2 10-2 10-1 10-1 10-3 10⁻³ da/dN (mm/cycle) da/dN (in/cycle) da/dN (in/cycle) 10-2 10-3 10 10-6 10-6 10-5 10 -5 10⁻⁷ 10⁻⁷ 10-6 10⁻⁶ 10-8 10⁻⁸ 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) Δ K (Ksi \sqrt{in}) da/dN ($10^{-6}in/cycle$) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 9.59 (min) 10. 13. 0.150 0.674 5.66 (min) 0.819 6. 2.07 7. 8. 3.43 16. 9. 10. 19.92 (max) 5.62 13. 16. 20. 25. 20.7 26.7 30. 33.41 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error 19.29 3.52 Ò. .5 .8 1.25 2. 1.25 0. .5 8. 2.

Figure 3.32.3.1.8

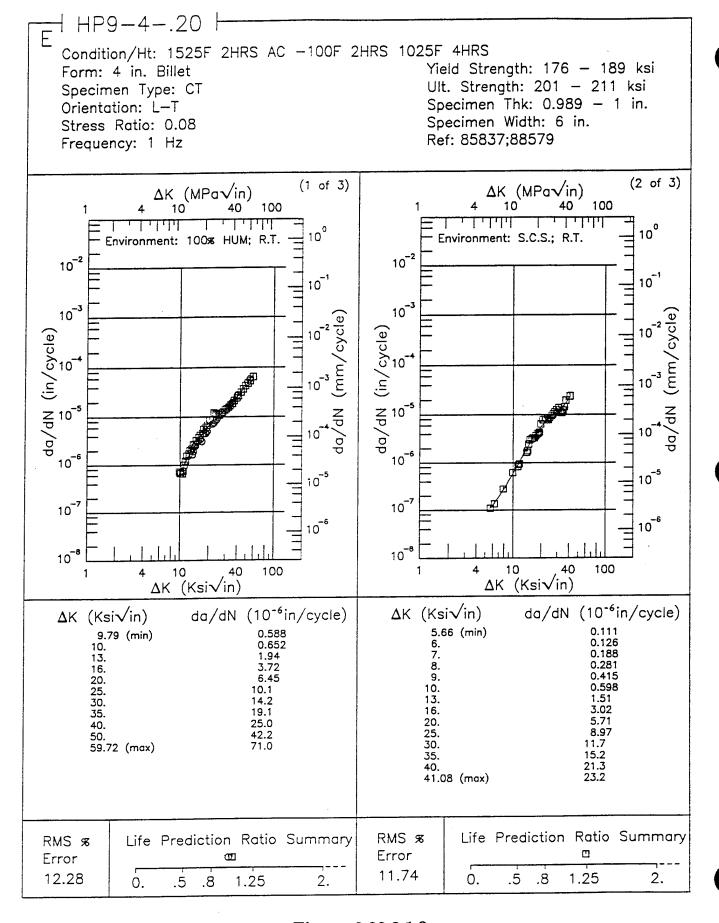


Figure 3.32.3.1.9

H HP9-4-.20 H Condition/Ht: 1525F 2HRS AC -100F 2HRS 1025F 4HRS Form: 4 in. Billet Yield Strength: 176 - 189 ksi Specimen Type: CT Ult. Strength: 201 - 211 ksi Orientation: L-T Specimen Thk: 0.989 - 1 in. Stress Ratio: 0.08 Specimen Width: 6 in. Ref: 85837;88579 Frequency: 1 Hz (3 of 3) Δ K (MPa \sqrt{in}) ΔK (MPa√in) 10 10 100 100 1 1 1 1 1 1 1 ויוידיד 10° 10° Environment: S.T.W.; R.T. 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10-6 10⁻⁵ 10 -5 10⁻⁷ 10-7 10-6 10⁻⁶ 10 8 10 -8 10 40 10 40 100 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) ΔK (Ksi \sqrt{in}) 0.144 0.172 0.265 5.62 (min) 6. 7. 8. 0.388 9. 13. 16. 20. 25. 30. 43.29 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error 6.45 Ò. .5 0. .5 .8 1.25 .8 1.25 2. 2.

Figure 3.32.3.1.9 (Concluded)

HP9-4-.20Condition/Ht: 1525F 2HRS AC -100F 2HRS 1025F 4HRS Yield Strength: 176 - 189 ksi Form: 4 in. Billet Ult. Strength: 201 - 211 ksi Specimen Type: CT Specimen Thk: 0.989 - 1 in. Orientation: L-T Specimen Width: 6 - 6.01 in. Stress Ratio: 0.08 Ref: 88579;85837 Environment: L.H.A.; -65°F - RT (2 of 4) (1 of 4)ΔK (MPa√in) Δ K (MPa \sqrt{in}) 40 100 100 40 10° 1 1 1 1 1 1 1 100 Frequency: 1 Hz Frequency: 0.1 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ 10 -2 da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10 -6 10 -5 10 -5 10⁻⁷ 10-7 10-6 10-6 10-8 40 100 100 10 40 10 ∆K (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 0.810 1.55 2.71 12.61 (min) 13. 10.61 (min) 13. 16. 16. 20. 25. 20. 25. 30. 35. 35. 40. 40. 50. 50. 55.93 (max) 58.49 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS %

Figure 3.32.3.1.10

2.

Error

3.27

.5 .8

0.

1.25

Error

20.74

.5

Ο.

.8

1.25

2.

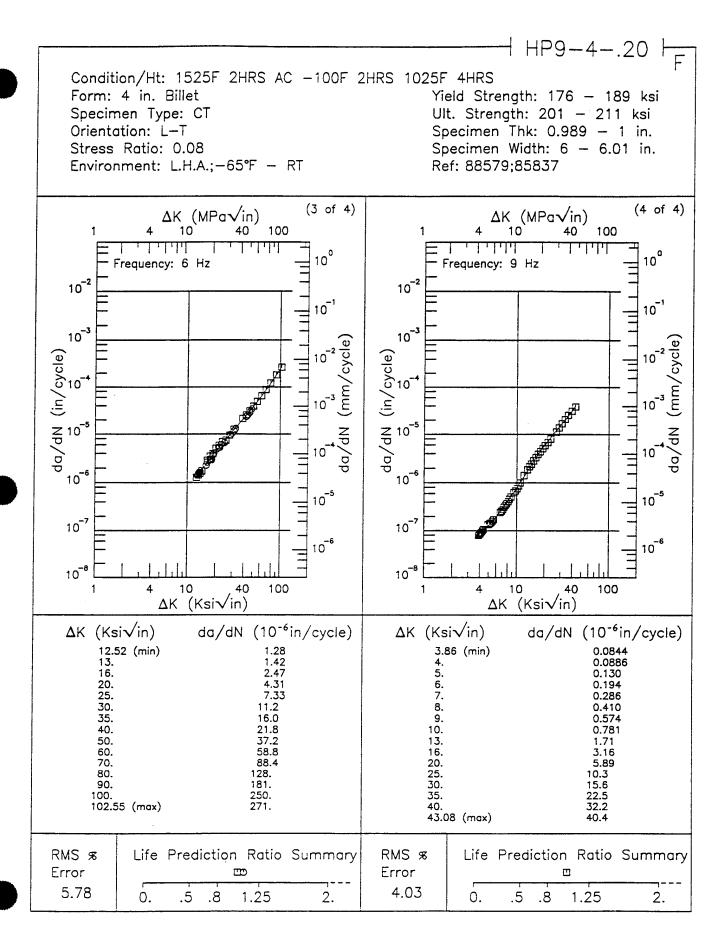


Figure 3.32.3.1.10 (Concluded)

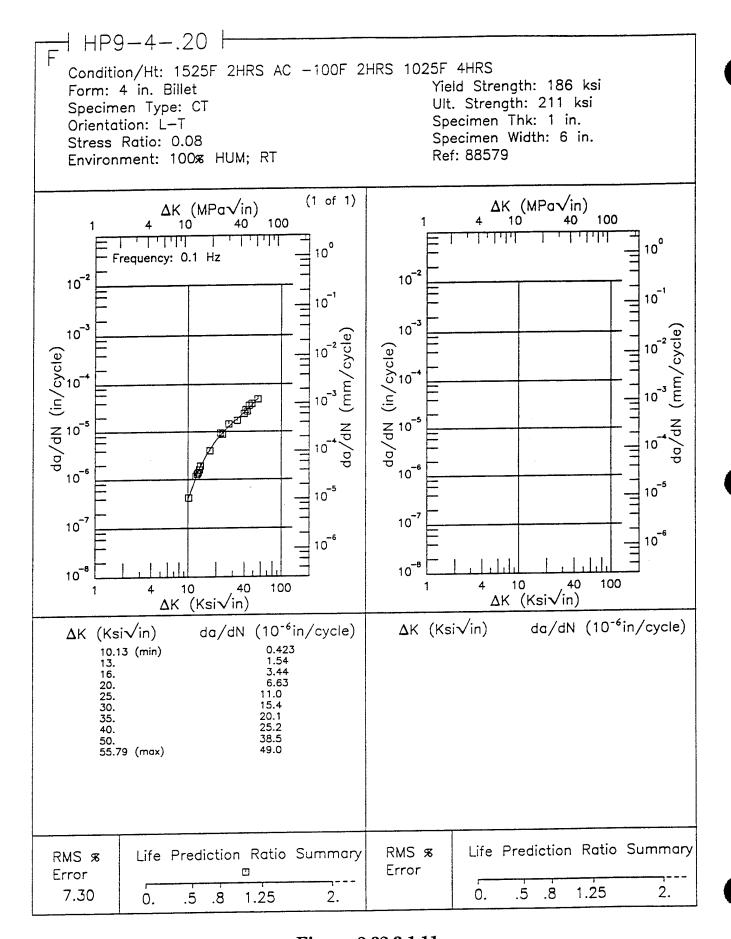


Figure 3.32.3.1.11

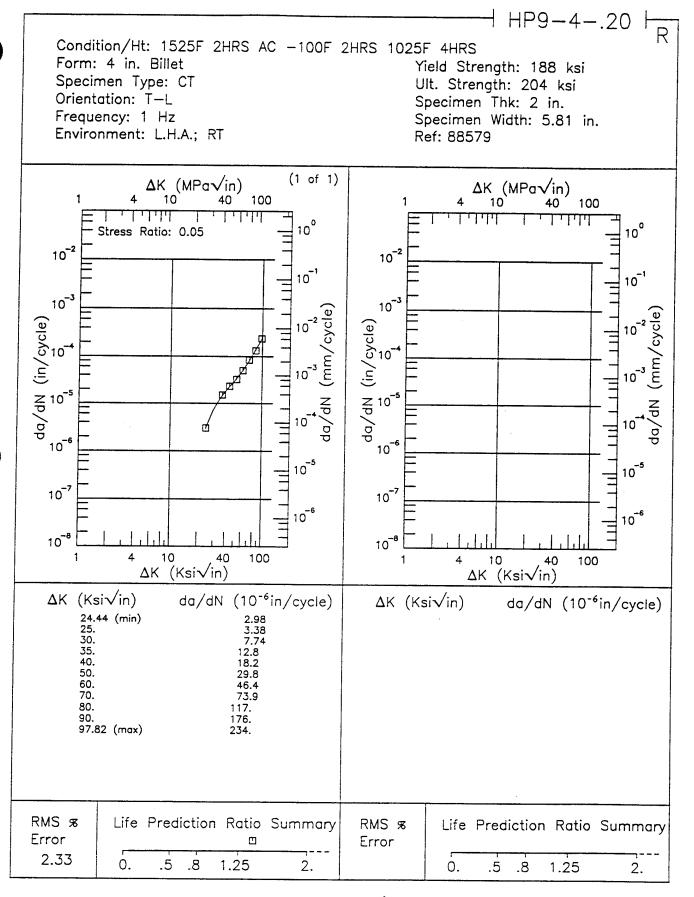


Figure 3.32.3.1.12

HP9-4-.20 F Condition/Ht: 1525F 2HRS AC -100F 2HRS 1025F 4HRS Yield Strength: 178 - 188 ksi Form: 4 in. Billet Ult. Strength: 204 - 209 ksi Specimen Type: CT Specimen Thk: 0.99 - 1 in. Orientation: T-L Specimen Width: 6 in. Stress Ratio: 0.08 Ref: 88579 (2 of 2)(1 of 2) $\Delta K_{10} (MPa\sqrt{in})$ ΔK (MPa√in) 100 40 10 100 ليلينا 10° 1 1 1 1 1 1 1 10° Environment: L.H.A.; R.T.; Frequency: 6 Hz Environment: L.H.A.; -65°F; Frequency: 1 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) 10-2 da/dN (in/cycle) 10⁻⁶ 10⁻⁶ 10 -5 10-5 10⁻⁷ 10⁻⁷ 10 6 10 -6 10 -8 10 -8 40 100 10 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) ΔK (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 1.15 1.52 2.77 11.94 (min) 17.18 (min) 13. 16. 20. 25. 30. 35. 40. 20. 25. 30. 35. 40. 50. 4.85 8.01 11.8 47.0 49.98 (max) 36.8 70. 110. 80. 86.98 (max) 140. Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % O Error Error 3.76 .5 .8 1.25 2. 4.50 2. 1.25 0. .5 .8

Figure 3.32.3.1.13

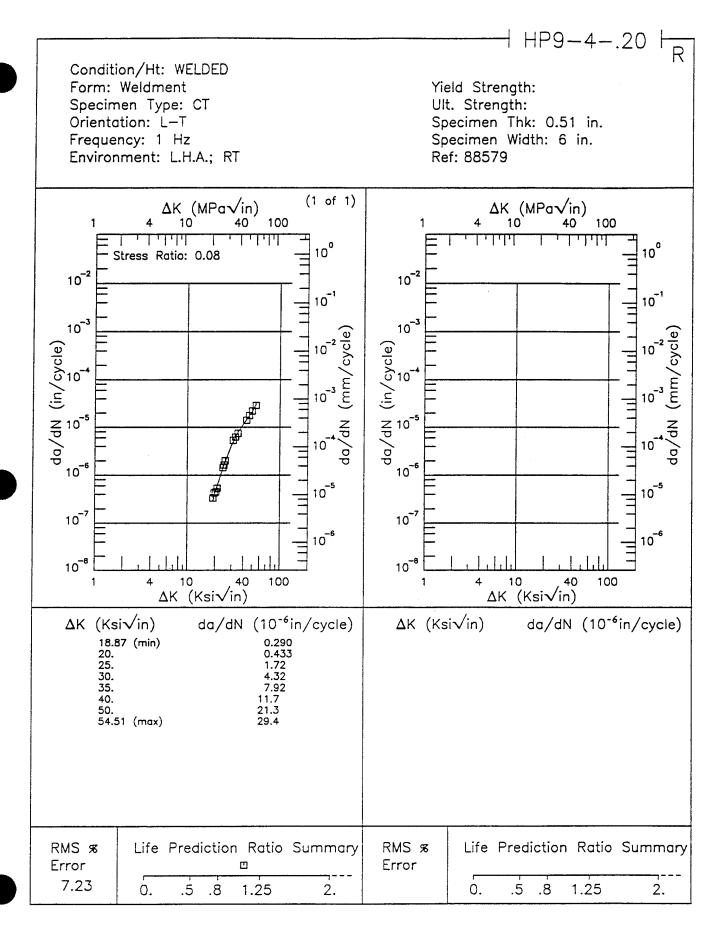


Figure 3.32.3.1.14

H HP9-4-.20 H Condition/Ht: WELDED Yield Strength: Form: Weldment Ult. Strength: Specimen Type: CT Specimen Thk: 0.49 - 0.5 in. Orientation: L-T Specimen Width: 6.01 in. Frequency: 6 Hz Ref: 88579 Environment: L.H.A.; RT (2 of 2) (1 of 2) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 100 10 10 40 100 11111 111111 11111 10° 10° Stress Ratio: 0.5 Hz Stress Ratio: 0.3 Hz 10-2 10-2 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10 -6 10-6 10 -5 10 -5 10⁻⁷ 10⁻⁷ 10-6 10 -6 10⁻⁸ 10 8 10 40 100 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 11.48 (min) 0.476 15.75 (min) 0.997 13. 16. 16. 20. 25. 20. 25. 30. 35. 40. 2.81 30. 35. 5.88 50. 60. 51.28 (max) 62.95 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error ╝ Error 6.45 0. .5 8. 1.25 2. 7.25 1.25 2. .5 8. 0.

Figure 3.32.3.1.15

HP9-4-.20 F Condition/Ht: Yield Strength: 196.5 ksi Form: 1.25 in. Forging Ult. Strength: 209.5 ksi Specimen Type: WOL Specimen Thk: 1.25 in. Orientation: L-T Stress Ratio: 0.02 Specimen Width: 5 in. Ref: MA005 Frequency: 0.1 - 20 Hz (2 of 2) (1 of 2) $\Delta K (MPa\sqrt{in})$ Δ K (MPa \sqrt{in}) 10 100 100 40 11111 100 10° Environment: LAB AIR; R.T. Environment: S.S.W.; R.T. 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ (mm/cycle) 10-2 da/dN (in/cycle) da/dN (in/cycle) 10 10⁻⁶ 10⁻⁶ 10⁻⁵ 10 -5 10⁻⁷ 10⁻⁷ 10⁻⁶ 10 -6 10 8 10-8 10 40 100 10 40 100 (Ksi√in) $\Delta \mathsf{K}$ ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 0.0939 8.36 (min) 21.08 (min) 25. 30. 4.80 9. 10. 35. 13. 40. 16. 50. 60. 70. 80. 100. 392. 130. 627. 160. 1876. 192.73 (max) 160. (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error 14.08 13.71 .8 1.25 0. .5 .8 1.25 2. 0. .5 2.

Figure 3.32.3.1.16

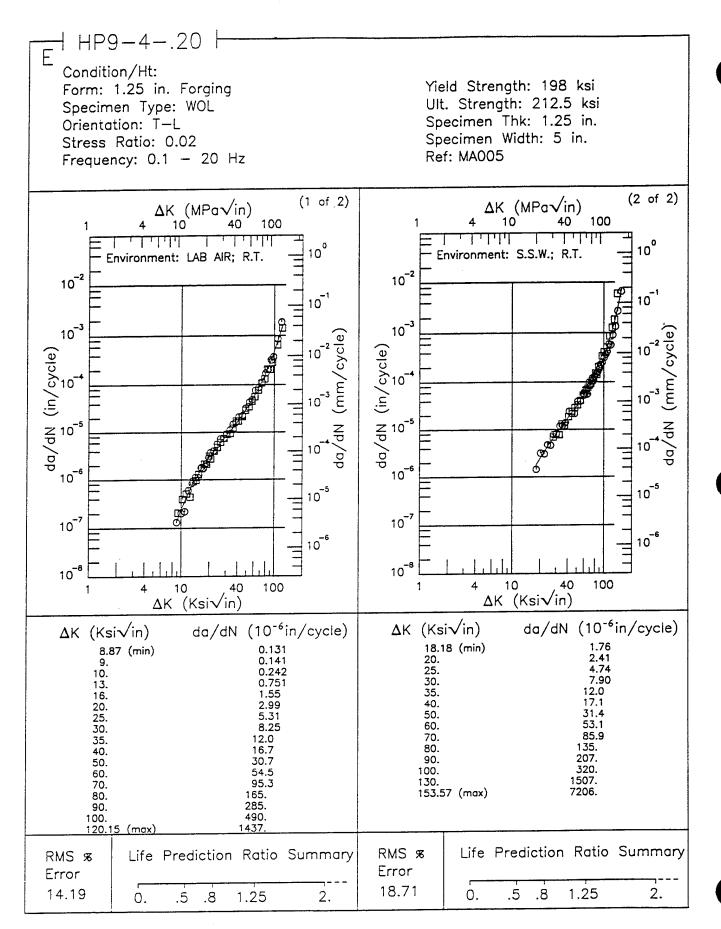


Figure 3.32.3.1.17

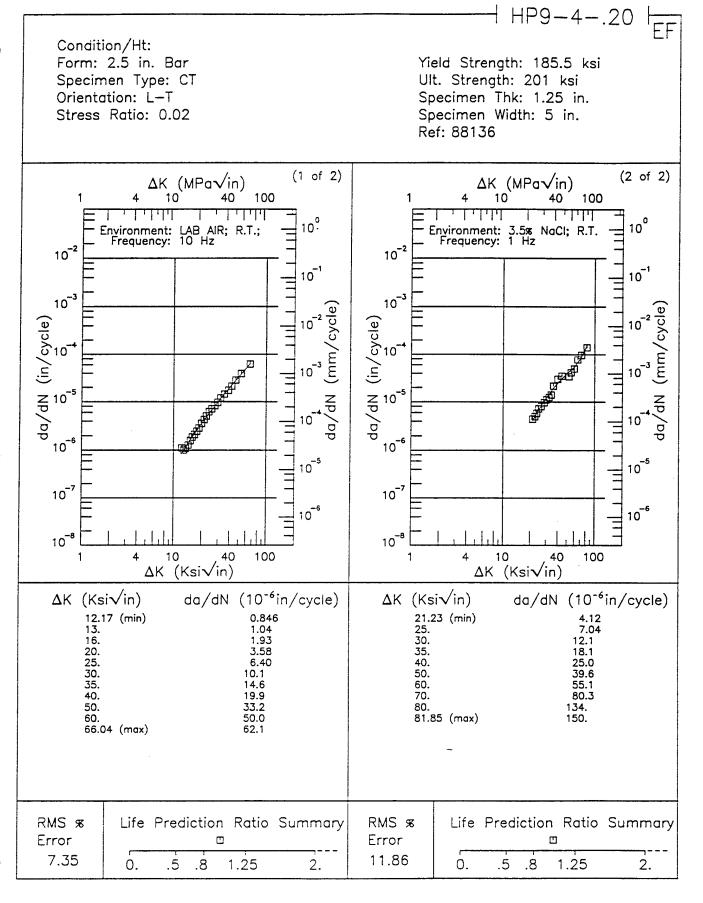


Figure 3.32.3.1.18

TABLE 3.32.3.3

K_{lsce} SUMMARY FOR ALLOY STEEL HP9-4-.20

7	£	Test	0	Yield		S	Specimen		Prod	1	,		Test		
Condition Heat Treat	Form		opec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)		(in)	Rq (Ksi√in)	Ksivin)	Time (min)	Test Date	Refer
						DCB	2	1	2.5	÷	611	103	86280	1976	Rioos
			L-T	189	S.T.W.	DCB	2	1	2.5	-	611	105	86280	1976	Riobe
						DCB	2	1	2.5		119	107	86280	1976	RIDOS
	۶	Ę				DCB	2	1	2.5	i	119	97	86280	1976	RI006
	. ,	Γ.Τ.				DCB	2	1	2.5	ı	119	93	86280	1976	RI006
			T-T	190	S.T.W.	DCB	2	1	2.5	!	119	96	86280	1976	RI006
						DCB	2	-	2.5	i	119	97	86280	1976	R1006
						DCB	2	-	2.5	:	119	104	86280	1976	RI006
						DCB	8	1	4		118	>129*	60180	1976	R1008
1525°F 2hrs OQ;					SC SC	DCB	ť	ĭ	4	1	118	>122*	09909	1976	Riose
-100° F zhrs; 1025° F 4hrs			L-T	186		DCB	2	1	4		118	<129⁺	86280	1976	RI006
					S.T.W.	DCB	2	-1	4	i	118	<126+	86280	1976	R1006
						DCB	2	1	4	:	118	110	86280	1976	RI006
		į				DCB	2	1	4	1	118	601	86280	9261	H1006
		ж ::	T-L	187	S.T.W.	DCB	2	1	4	••	118	<1.17	86280	1976	RI006
						DCB	2	1	þ		118	105	76860	1976	Rioos
						DCB	2	П	4	:	118	-62	86280	1976	RI006
			5		in e	DCB	2	П	4	i	118	75+	116820	1976	R1006
			ά	1	D. I. W.	DCB	2	1	4	1	118	-424	86280	1976	RI006
						DCB	7		4	i	118	81+	86280	1976	RI006

TABLE 3.32.3.3 (CONCLUDED)

Kisce SUMMARY FOR ALLOY STEEL HP9-4-.20

Condition	חיים	Test	2	Yield		S	Specimen		Prod	,			Toot		
Heat Treat	Form	Form (°F) Or. (Ksi)	Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)		Crack (in)	Crack Ko (in) (Ksivin)	K _{law} (Ksi√in)	Time (min)	Test Date	Refer
GTA Weld Weldment	Ъ	R.T.	ļ		Synth Seawater	TDCB	i	i	0.5	1	1	65	11	1969	74232
Quenched and	۲	Ę		180	3.5% NaCl	CANT.	1	1	1	:	210	110	:	1972	83613
Tempered	7	K.I.	:	195	3.5% NaCl	CANT		1	1	1	200	011	1	1972	83613
Unspecified	Ь	R.T.	i	·	N ₂ 0,-0.2% H ₂ O	TDCB	5.5	0.5	0.5	į	150	140+	1	1971	80667
Unspecified	Ъ	R.T.	i	ł	Synth Seawater	TDCB	į	•	0.5	i	j	110*	i	1969	74232
Thenovified	ŗ.	£ a	Ę	300	Sim. Sea	BWOL	3.083	1.247	1.25	1.37	:	92.8	195840	1977	MA005
pattinadella	•		77-7	061	Water	BWOL	3.088	1.25	1.25	1.37	:	94.5	195840	1977	MA005

* specimen thickness does not meet minimum requirements of $2.5~(rac{K_{low}}{\sigma_{yy}})$

* asterisk in specimen design column indicates that specimens are side-grooved

TABLE 3.33.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.20(CEVM) AT ROOM TEMPERATURE

ENVIRONMENT: Lab Air	AK Level (Ksk/in) 2.5 5.0 10.0 20.0 50.0 100.0	6.33 37.05
	R FREQ	0.1 5-10
.L-T	PRODUCT	FORGING
ORIENTATION: L-T	CONDITION/ HEAT TREATMENT	ANNEALED

TABLE 3.33.1.2.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK HP9-4-.20(CEVM) AT ROOM TEMPERATURE

ORIENTATION: L-T

ENVIRONMENT: S.S.W.

.0 100.0 73	KO.7 3
0.001 0.	2.5 5.0 10.0 20.0 50.0
	ΔK Level (Ksi/in)
	PCGR (10 4 in/cycle)

TABLE 3.33.1.2.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.20(CEVM) AT ROOM TEMPERATURE

ORIENTATION: T-L

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100.0		
K0.0 43.6	((0
20.0 5.78	ΔK Leval (Ksi√in)	FCGR (10 ⁴ in/cycle)
10.0 20.0	Lovel (5 (10 ⁸
6.0	ΔK	FCGI
2.5		
1-10	(Hz)	FREG
0.1	¥	
FORGING	FORM	RODUCT
		P
ANNEALED	HEAT TREATMENT	HION/
ANN	HEAT TR	COND

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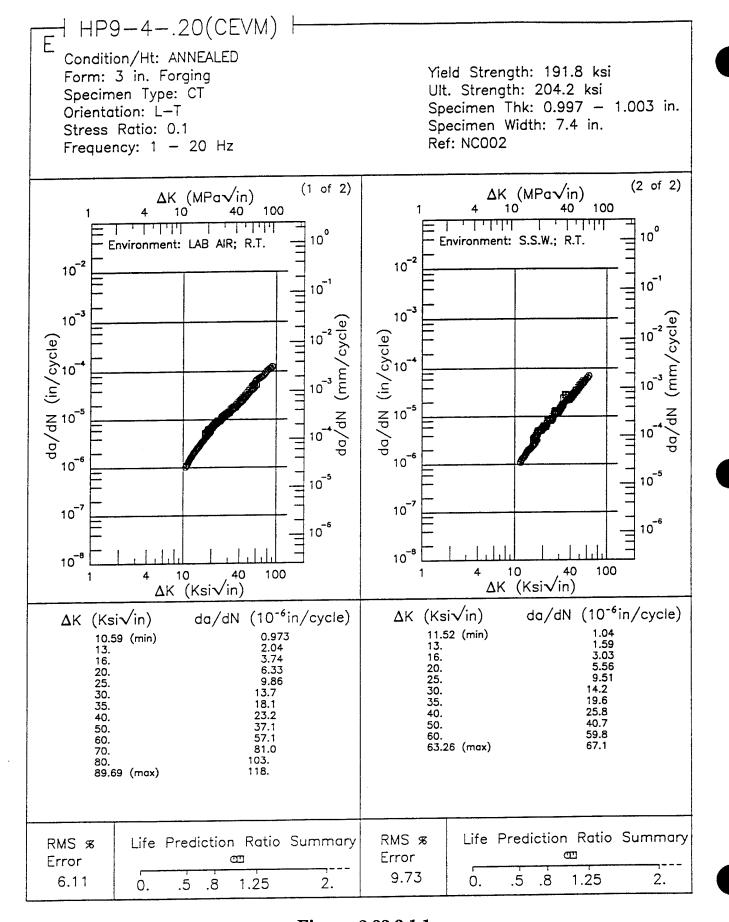


Figure 3.33.3.1.1

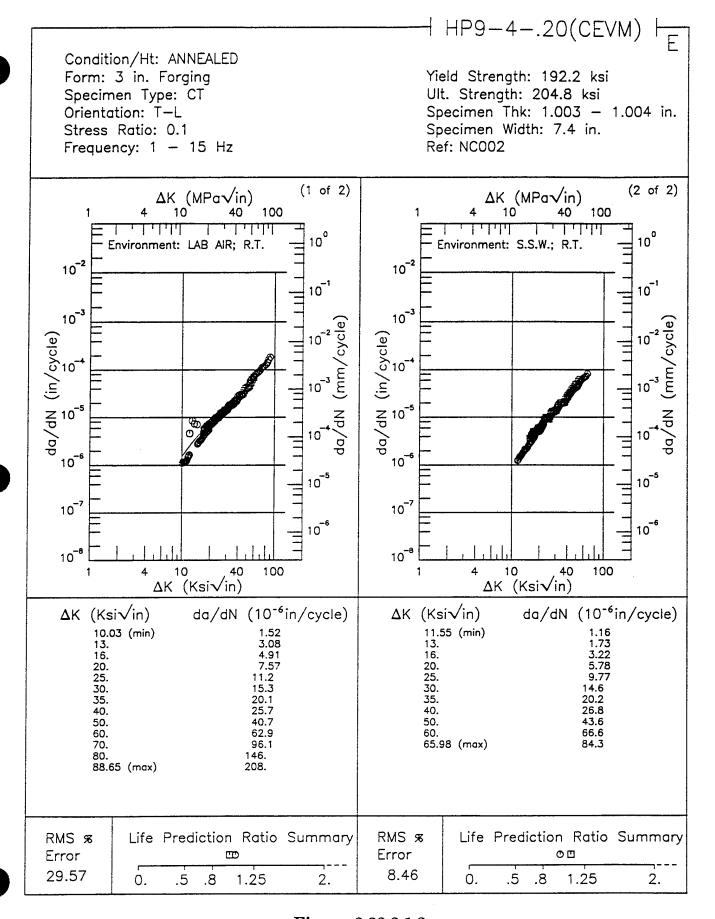


Figure 3.33.3.1.2

TABLE 3.34.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL HP 9-4-.25 (VAR) AT ROOM TEMPERATURE

					K_{lc}	$K_L~(ksi\sqrt{in})$	િ			
Froduct Form	Condition/Heat Treatment			y v	Specimen Orientation	n Orien	ntation			
			L-T			T-T			S-L	
		Mean K ₁₀	Std Dev	ч	Mean K _{le}	Std Dev	u	Mean K _{ie}	Std Dev	п
Forging	1550F 1HR OQ 1000F 2+2HR AC	:	:	:	98.9	4.6	2		i	;

1 of 1

					ALLO	ALLOY STEEL		HP 9-425 (VAR)	R) K _{Io}						
	PRO	PRODUCT					SPECIMEN	EN	CRACK			K _{to}			
CONDITION	FORM	THICK (fn.)	TEST TEMP (*F)	SPRC	YIBLD STR (Kal)	WIDTH (fn.) W	THICK (Ib.)	DESIGN	LENGTH (in.) A	(R. 7178)* (In.)	K. OKad •	K. MRAN	BTAN	DATB	REFER
1650F 1 HR OQ	Ğ	3.00	į	Ē	187.0	6.110	2.000	WOL-CT EQ.	1.834	1.08	123.00			1966	76411
1000F 2+2 HR AC	South of	3.00	2	₹	187.0	5.110	2.000	WOLCT EQ.	1.864	0.82	107.00	115.0	11.3	1966	76411
1650F 1 HR OQ		3.00	5		188.0	6.110	2.000	WOLCT EQ.	1.886	98.0	110.00			1966	76411
1000F 2+2 HR AC	rorging	3.00	Q .	3	188.0	6.110	2.000	WOL-CT EQ.	1.863	0.89	112.00	111.0	1.1	1966	76411
1550F 1 HR OQ	f	3.00		į	187.0	6.110	2.000	WOL-CT EQ.	1.837	0.82	107.00			1966	76411
1000F 2+2 HR AC	rorging	3.00	•	1	187.0	5.110	2.000	WOLCT EQ.	1.879	0.79	105.00	106.0	1.4	1966	76411
1550F 1 HR OQ		3.00	S	Ē	187.0	6.110	2.000	WOL-CT EQ.	1.868	0.79	104.00			1966	76411
1000F 2+2 HR AC	Forging	3.00	70	3	187.0	6.110	2.000	WOL-CT EQ.	1.964	0.71	99.40	101.7	3.3	1966	76411
1650F 1 HR OQ	ģ	3.00	E		175.0	6.110	2.000	WOL-CT EQ.	1.822	0.75	95.70			1966	76411
1000F 2+2 HR AC	Forging	3.00	Re. I.	3	175.0	5.110	2.000	WOLCT EQ.	1.808	0.85	102.00	8.88	9.4	1966	76411
1660F 1 HR OQ	2	3.00	Ş	<u>-</u>	180.0	6.110	2.000	WOL-CT EQ.	1.853	0.84	104.00			1966	11192
1000F 2+2 HR AC	rorging.	3.00	3	2	180.0	5.110	2.000	WOL-CT EQ.	1.855	0.78	101.00	102.6	2.1	1966	11792
1550F 1 HR OQ	Ş	3.00	Ş	Ē	175.0	5.110	2.000	WOLCT EQ.	1.834	1.00	111.00			1966	11191
1000F 2+2 HR AC	r organs	3.00	ner	3.	175.0	6.110	2.000	WOL-CT EQ.	1.824	0.92	106.00	108.5	3.6	9961	11191

TABLE 3.35.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL HP 9-4-.30 AT ROOM TEMPERATURE

Drodnot					K_{Ic}	$K_{Ic}~(ksi\!\!\sqrt{i}n)$	(ī			
Form	Condition/Heat Treatment			S	Specimen Orientation	n Orien	itation			
			L-T			T-L	,		$\mathbf{7-S}$	
		Mean Kıc	Std Dev	u	Mean K _{to}	Std Dev	u	Mean K _{le}	Std Dev	u
. Plate	HEAT TREATED TO 49 RC HARDNESS	1	:	1	82.5	ο.	2	i	;	ł
	1650F 1-2HR AC 1625F 1-2HR OQ -100F 1-3HR 1000F 4HR	106	1.4	2	89	3	3			:
Forzing	1650F 1-2HR AC 1626F 1-2HR OQ -100F 1-3HR 1026F 4HR	•••	:	:	93.6	0.7	2	:		ı
	1650F 1-2HR AC 1525F 1-2HR OQ -100F 1-3HR 1050F 4HR	i	:	ŧ	87.6	0.8	2	:	:	i
	1650F 2HR AC 1550F 2HR OQ 1000F 2+2HR AC	82	0	2	:	:		:		:

TABLE 3.35.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.30 AT ROOM TEMPERATURE

ORIENTATION: L-T

ENVIRONMENT: 3.5% NaCl

FG.0 190.0	AK Level (Kst/in) 100 200 6
	FCGR (10 ⁻⁶ in/cycle)

TABLE 3.35.1.2.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.30 AT ROOM TEMPERATURE

ENVIRONMENT:

Alt Immersion Seawater - Immersion

TABLE 3.35.1.2.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.30 AT ROOM TEMPERATURE

ENVIRONMENT:

Alt Immersion Seawater - 1st Half Dry Cycle

20.07	3.19				10	0.	BILLET	UTS=220-240KSI
25.83	2.7				-	0.		
20.0 50.0 100.0	0.02	10.0	5.0	2.5				
2								
(a)	AK Lawi (Kakin)	KInga	Y		(HZ)	¥	FORM	E
					FREG	£	PRODUCT	CONDITION
ile)	PCGR (10° in/ayele)	GB (10	FC					

TABLE 3.35.1.2.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4.30 AT ROOM TEMPERATURE

ENVIRONMENT:

Alt Immersion Seawater - 2nd Half Dry Cycle L-T

	****	T
	100.0	
la la la la la la la la la la la la la l	33.2	28.67
FCGR (10.4 in/eyele) AK Level (Ket/in)	10,0 26.0	3.43
GR (10	0'01	
OH TO	0.0	
	2.5	
FREQ (Hz)	1	10
B	0.	0.
PRODUCT		BILLET
CONDITION/ HEAT TREATMENT		UTS=220-240KSI

TABLE 3.35.1.2.5

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.30 AT ROOM TEMPERATURE

ORIENTATION: L-T

ENVIRONMENT: L.H.A.

PRODUCT
FORM
FORGED BAR
FORGED BAR
BILLET

TABLE 3.35.1.2.6

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.30 AT ROOM TEMPERATURE

TABLE 3.35.1.2.7

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK HP9-4-.30 AT ROOM TEMPERATURE

	erect _	298.27
	rcle) (m) (m)	37.72
S.W.	FCGR (10 d in/cycle) AK Level (Ksi/in)	
NT: S.	CCR (10 K Lovel	
ENVIRONMENT: S.S.W.	A A	
ENVIR	10 m	
	FREQ (Hz)	0.1-15
	R	0.02
	UCT	ING
L-T	PRODUCT	FORGING
ORIENTATION: L-T	TAI	
RIENT	CONDITION/ HEAT TREATMENT	UNSPECIFIED
	COND AT TR	UNSPE
	HE	

TABLE 3.35.1.2.8

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.30 AT ROOM TEMPERATURE

ENVIRONMENT: S.T.W.		R (Hz) AK Lovel (Ksk/in)	2.5 5.0 10.0 20.0 50.0 100.0	0.08 1 5.68 62.33	0.08 0.1 2.63 13.42	0.3 1 0.89 7.34	0.5 1 1.8 9.22
L-T	PRODUKET	FORM		FORGED BAR		FORGED BAR	
ORIENTATION: L-T	NOILIUNOS	HEAT TREATMENT		1525F 2HRS OQ -100F 2HRS 1026F 2+2HR		1550F 2HRS OQ -100F 1HR 1025F 2+2HR	

TABLE 3.35.1.2.9

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK HP9-4-.30 AT ROOM TEMPERATURE **ENVIRONMENT: 3.5% NaCl** ORIENTATION: T-L

					T T T T T T T T T T T T T T T T T T T	TECHNISM TO 0.0% MACI	MACI		
CONDITION	PRODUCT	î	FREG		PC	<i>CR</i> (10	PCGR (10 ⁴ in/cycle)	le)	
HEAT TREATMENT	FORM	¥	(HZ)		77	K Leval	ΔK Level (Ksi√in)	n)	
				2.5	0.0	0.01	20.0	50.0	100.0
		0.	15				3.02		
		0.1	0.1					114.04	
		0.1	0.1					114.04	
		0.1	0.1					114.04	
		0.1	1					56.54	
		0.1	1					56.54	
INSPECIFIED	GFA IG	0.1	1					58.54	
		0.5	0.1				18.68		
		0.5	0.1				18.68		
		0.5	0.1				18.68		
		0.5	1				11.3		
		0.5	1				11.3		
		0.5	1				11.3		
		8.0	0.1			71.25	292.97		

TABLE 3.35.1.2.10

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.30 AT ROOM TEMPERATURE

ENVIRONMENT: Alt JP-4 Jet Fuel & Distilled Water

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7.6	C ₄		
FCGR (10 ⁻⁶ lr/cyule)	ΔΚ Level (Kak/in)	*****	\dashv
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		100	
		2.5 5.0	
FREG			
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TABLE 3.35.1.2.11

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK

100.0 80.0 316.2 51.71 51.33 PCGR (10 d in/cycle) **ENVIRONMENT: Distilled Water** ΔK Level (Ksivin) 20.0 23.98 23.98 2.78 10.0 9 HP9-4..30 AT ROOM TEMPERATURE 8) (3) FREQ (Hz) 15 0.1 × 0.1 0.1 0.1 9.0 0.5 ö PRODUCT FORM PLATE ORIENTATION: T-L HEAT TREATMENT CONDITION UNSPECIFIED

TABLE 3.35.1.2.12

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.30 AT ROOM TEMPERATURE

	9)		
Air	in/cyd (Ksi/in	7.03	
Tr: Dry	GR (10*		14.93
ENVIRONMENT: Dry Air	MCA AA		
ENVIR	2.5		
1	FREQ (Hz)	0.1	1
	æ	0.5	9.0
N: T-L	PRODUCT		FLATE
ORIENTATION	CONDITION/ HEAT TREATMENT	STATE OF THE PARTY	ONSPECIFIED

TABLE 3.35.1.2.13

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.30 AT ROOM TEMPERATURE

ORIENTATION: T-	i: T-L			ENVIRONMENT: L.H.A.	ENT: L.H.	Ą		
CONDITION/ HEAT TREATMENT	PRODUCT FORM	R	FREQ (Hz)	AAR	7. Loval	d incord (Ksivin	0.0	100.0
1550F 2HRS OQ -100F 1HR 1025F 2+2HR	FORGED BAR	90'0	9			5.13		
1550F 2HRS OQ -100F 3HRS 1000F 2+2HRS	FORGED BAR	0.08	9			3.46	46.38	

TABLE 3.35.1.2.14

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK HP9-4-.30 AT ROOM TEMPERATURE

	e 8
	1733.09
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u a a a a a a a a a a a a a a a a a a a	3.14
T: Lab	10.0 0.48
MMEN	0.0
ENVIRONMENT: Lab Air FCGR (10 ⁻⁸ in/c	60
E FREQ (Hz)	0.1-20
œ	0.02
T-L PRODUCT FORM	FORGING
CONDITION/ HEAT TREATMENT	UNSPECIFIED

TABLE 3.35.1.2.15

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.30 AT ROOM TEMPERATURE

ORIENTATION: T.L

ENVIRONMENT: S.S.W.

			
		100.0	2260.23
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		₩-	22
		*****	- 24
		60.0	
		₩₩	44.09
_		₩3	4
FCGR (10 ⁴ in/cycle)		******	•
77	ΔK Level (Ksiγin)	20.0	
5		****	
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-			2.44
		***	61
100		*****	
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TABLE 3.35.1.2.16

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HP9-4-.30 AT ROOM TEMPERATURE

173.09 173.09 173.09 60.0 68.83 68.83 FCGR (10 fivorale) AK Level (Ksk/in) 20.0 9.12 9.12 4.84 ENVIRONMENT: S.T.W. 10.0 0.69 9 9 9) 9) FREQ (Hz) 0.7 0.1 0.1 0.08 0.1 0.1 0.1 0.0 0.5 ĸ 0.1 0.1 PRODUCT FORM FORGED BAR PLATE ORIENTATION: T-L 1550F 2HRS OQ -100F 1HR 1025F 2+2HR HEAT TREATMENT CONDITION UNSPECIFIED

TABLE 3.35.1.2.17

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR △K HP9-4-.30 AT ROOM TEMPERATURE

ORIENTATION:

ENVIRONMENT: Water Saturated JP-4 Jet Fuel

		100.0													
(e)	J.	20.0		63.97	63.97	63.97	51.66	49.21	51.66						
FCGR (10 ⁻⁸ in/oyule)	ΔΚ Level (Kai/m)	0.04	2.54							8.46	8.46	8.46	7.29	7.29	7.29
<i>CR</i> (10	K Love	10,0													
FC	7	6.8													
		2.5							,						
FREG	(HZ)		15	0.1	0.1	0.1	1	1	1	0.1	0.1	0.1	1	1	1
í	#		ю.	0.1	0.1	0.1	0.1	0.1	0.1	0.5	0.5	0.5	0.5	0.5	0.5
PRODUCT	FORM								PLATE						
CONDITION/	HEAT TREATMENT								UNSPECIFIED						

TABLE 3.35.2.1

				•	ALLOY STEEL	STEEL	HP 9-430		$\mathbf{K}_{\mathbf{I}_{\mathbf{o}}}$						
	PROI	PRODUCT					SPECIMEN	7	CRACK			K _{Ie}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (in.)	THICK (in.)	DESIGN	LENGTH (In.) A	2.0 (K., TYS)* (in.)	¥, ŒÌ	K. MBAN	BTAN	DATE	REFER
		1.25	ä		207.5	2.529	1.245	CT	1.273	99.0	106.10			1977	MA005
•••	Forging	1.25	18	7	207.6	2.519	1.245	LO	1.263	0.67	108.19	107.1	1.5	1977	MA005
	E	1.26	ě		208.3	2.623	1.246	CT	1.258	0.58	101.10			1977	MA005
:	rorging	1.25	16	1-I	208.3	2.534	1.246	CT	1.293	0.58	101.10	101.1	0.0	1977	MA005
1525F OQ -100F 3 HR 1050F 4HR	Forging	3.00	99-	T-L	175.0	5.000	1.900	CT	!	1.64	142.00	1	,	1974	90011
1650F ZHR AC 1550F ZHR OQ		3.25	Ę		192.0	4.003	2.015	cr	1.833	0.48	82.00			1974	88136
1000F 2+2HR AC	rorging	3.25	K.T.	Lr.I	192.0	4.014	2.016	CI	1.997	0.48	82.00	82.0	0.0	1974	88136
1650F 1-2HR AC 1625F 1-2HR OG		3.00	į	:	220.0	3.000	1.000	cT	1	0.23	67.00			1974	90011
-100F 1-3HR 1000F 4HR	Forging	3.00	දි	ЬT	220.0	3.000	1.000	cr		22:0	90.99	66.5	0.7	1974	90011
1650F 1-2HR AC 1625F 1-2HR OQ	F	3.00	Ę	E	206.0	3.000	1.000	CT		19:0	107.00			1974	90011
.100F 1.3HR 1000F 4HR	Forging	3.00	W. I.	3	206.0	3.000	1.000	ŗ.		0.65	105.00	106.0	1.4	1974	11006
		3.00			206.0	3.000	1.000	CT	1	0.43	86.00			1974	11008
1650F 1-2HR AC 1626F 1-2HR OQ -100F 1-3HR 1000F 4HR	Forging	3.00	R.T.	T-L	215.0	3.000	1.000	ÇŢ	:	0.46	92.00	89.0	3.0	1974	11006
		3.00			215.0	3.000	1.000	CT		0.43	89.00			1974	90011
1650F 1-2HR AC 1626F 1-2HR OQ -100F 1-3HR 1026F 4HR	Forging	3.00	R.T.	Γ·I	205.0	3.000	1.000	CT	:	0.80	116.00	ŀ	I	1974	90011
1650F 1-2HR AC 1525F 1-2HR OQ		3.00	E f	į	205.0	3.000	1.000	CT	1	0.52	94.00			1974	11006
-100F 1-3HR 1025F 4HR	rorging	3.00	K.T.	T-L	205.0	3.000	1.000	CT	1	0.51	93.00	93.5	0.7	1974	11006

TABLE 3.35.2.1 (CONCLUDED)

					ALLOY	ALLOY STEEL	HP 9-430		$\mathbf{K_{lc}}$						
	PROI	PRODUCT					SPECIMEN	7	CRACK			K _{Io}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC OR	YIELD STR (Kai)	WIDTH (in.)	THICK (in.)	DESIGN	LENGTH (In.) A	(K.,TYS)* (in.)	K. (Kei * √in.)	K, MBAN	STAN	DATE	REFER
1650F 1-2HR AC 1525F 1-2HR OQ		3.00	I		200.0	3.000	1.000	CT		0.48	88.10			1974	90011
.100F 1-3HR 1050F 4HR	Forging	3.00	KT.	Ţ.	200.0	3.000	1.000	CT	-	0.47	87.00	87.6	9.0	1972	84306
1650F 2HRS AC 1550F 2HR OQ -100F 2HR AC 1000F 4HR AC 1000F 4HR AC	Forging	:	R.T.	:	201.8	2.008	0.997	LO	1.024	080	114.20	ı	:	1977	AM002
1650F AC 1525F 1-2HR OQ -100F 1-3HR 1050F 4HR	Forging	3.00	R.T.	T-L	197.0	3.000	1.000	CT		29.0	102.00	1	ı	1974	90011
HEAT TREATED TO	I	3.25	8		189.0	2.006	1.005	NB	1.010	0.44	78.90			1971	84029
49 RC HARDNESS	Finte	3.25	K.I.	7:I	189.0	2.004	1.005	NB	0.990	0.52	86.00	82.5	6.0	1971	84029

HP9-4-.30 H Condition/Ht: 1525F 2HRS OQ -100F 1HR 1025F 2+2HR Yield Strength: 216 ksi Form: 3 in. Forged Bar Ult. Strength: 239 ksi Specimen Type: CT Specimen Thk: 1 in. Orientation: L-T Specimen Width: 5.01 in. Frequency: 1 Hz Ref: 88579 Environment: L.H.A.; RT (1 of 1) Δ K (MPa \sqrt{in}) $\Delta K (MPa\sqrt{in})$ 100 10 40 100 10° Stress Ratio: 0.08 10-2 10-2 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10⁻⁵ 10 -5 10⁻⁷ 10⁻⁷ 10 -6 10 6 10-8 40 100 10 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) ΔK (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) 10.79 (min) 1.65 3.89 5.32 13. 16. 19.15 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error 11.67 .5 .8 1.25 2. 0. 0. .5 .8 1.25 2.

Figure 3.35.3.1.1

Condition/Ht: 1525F 2HRS OQ -100F 2HRS 1025F 2+2HR Form: 3 in. Forged Bar Yield Strength: 216 ksi Specimen Type: CT Ult. Strength: 239 - 239.6 ksi Orientation: L-T Specimen Thk: 0.97 in. Stress Ratio: 0.08 - 0.3 Specimen Width: 4.97 in. Ref: 88579 (1 of 2)(2 of 2) Δ K (MPa \sqrt{in}) ΔK (MPa√in) 10 100 1 40 4 10 40 100 11111 10° 10° Environment: S.T.W.; R.T. Frequency: 1 Hz Environment: L.H.A.; R.T. Frequency: 6 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ cycle 10-2 da/dN (in/cycle) da/dN (in/cycle) 10 -3 10 10⁻⁶ 10-6 10⁻⁵ 10 -5 10 7 10⁻⁷ 10 -6 10⁻⁶ 10-8 10⁻⁸ 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) ΔK (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) 11.35 (min) 11.36 (min) 0.808 1.35 1.98 13. 16. 13. 16. 20. 25. 30. 5.68 20. 12.0 30. 12.8 35. 40. 35. 19.3 50. 50. 60. 63.58 (max) 422. 73.59 (max) RMS % Life Prediction Ratio Summary RMS & Life Prediction Ratio Summary □ Error Error 8.23 10.87 1.25 0. .5 .8 2. 0. .5 1.25 .8 2.

HP9-4-.30 EF

Figure 3.35.3.1.2

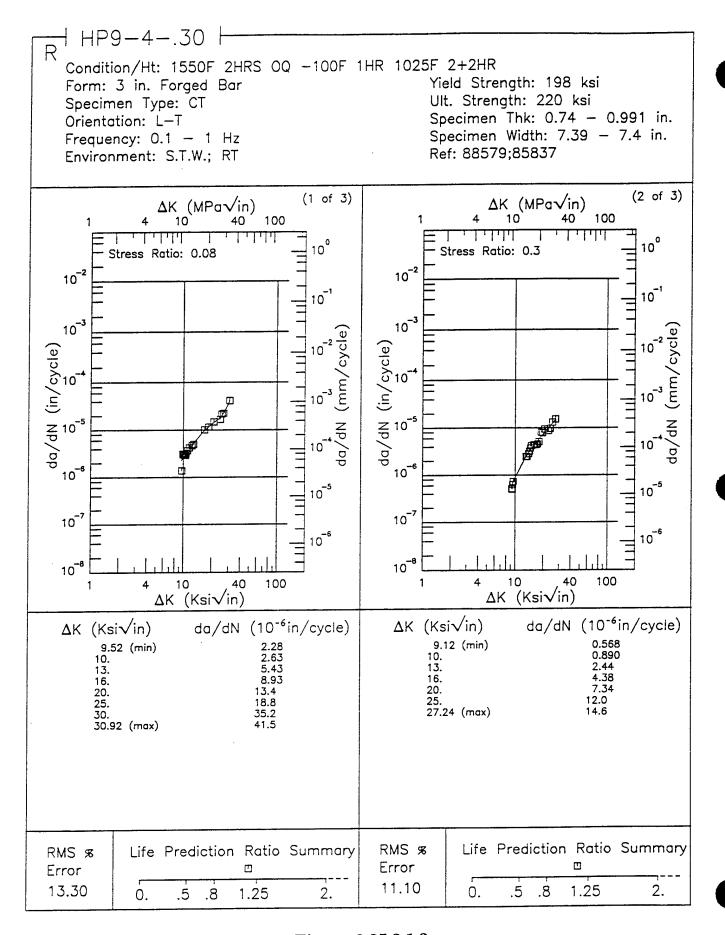


Figure 3.35.3.1.3

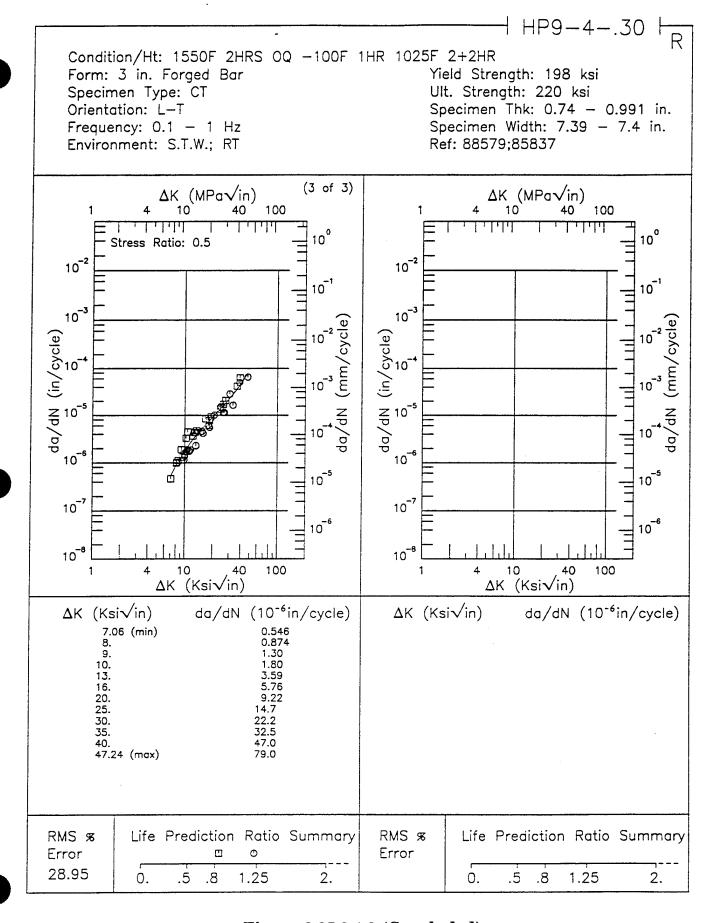


Figure 3.35.3.1.3 (Concluded)

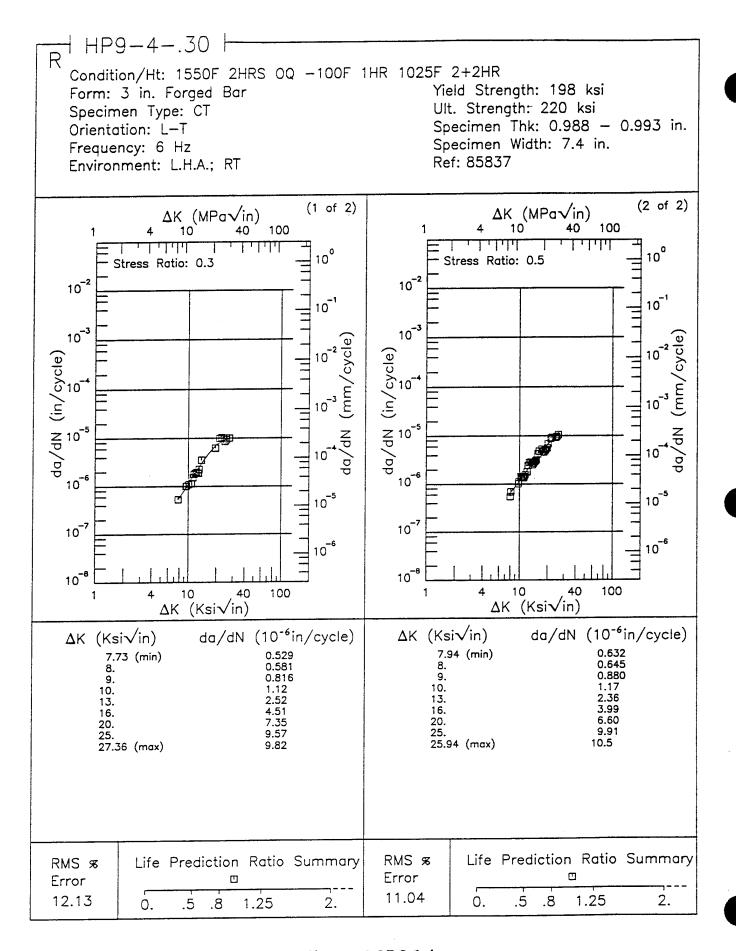


Figure 3.35.3.1.4

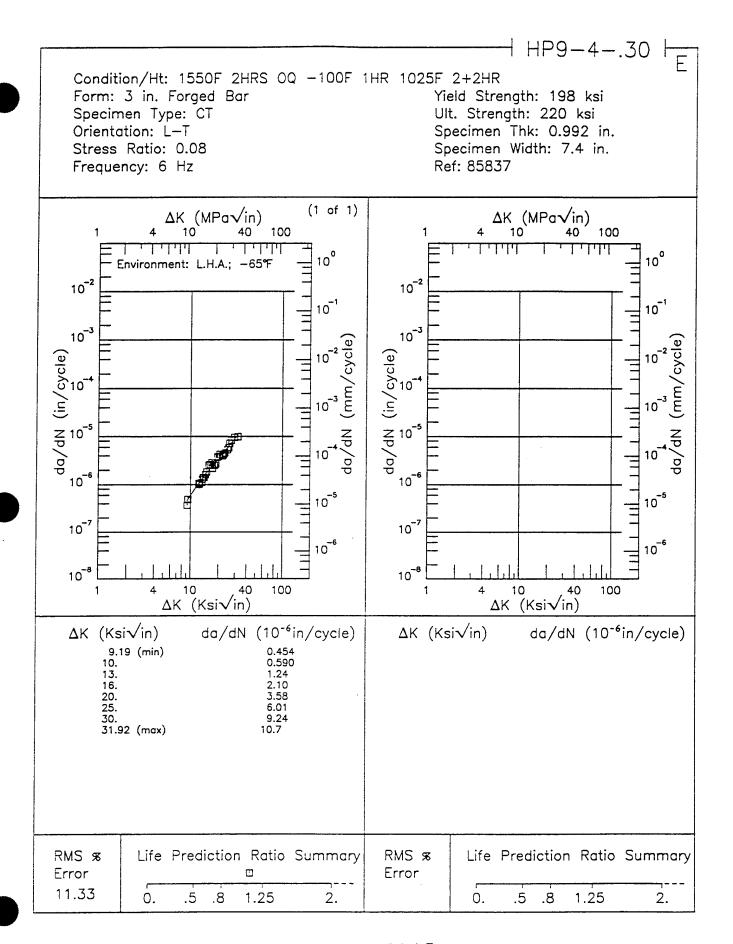


Figure 3.35.3.1.5

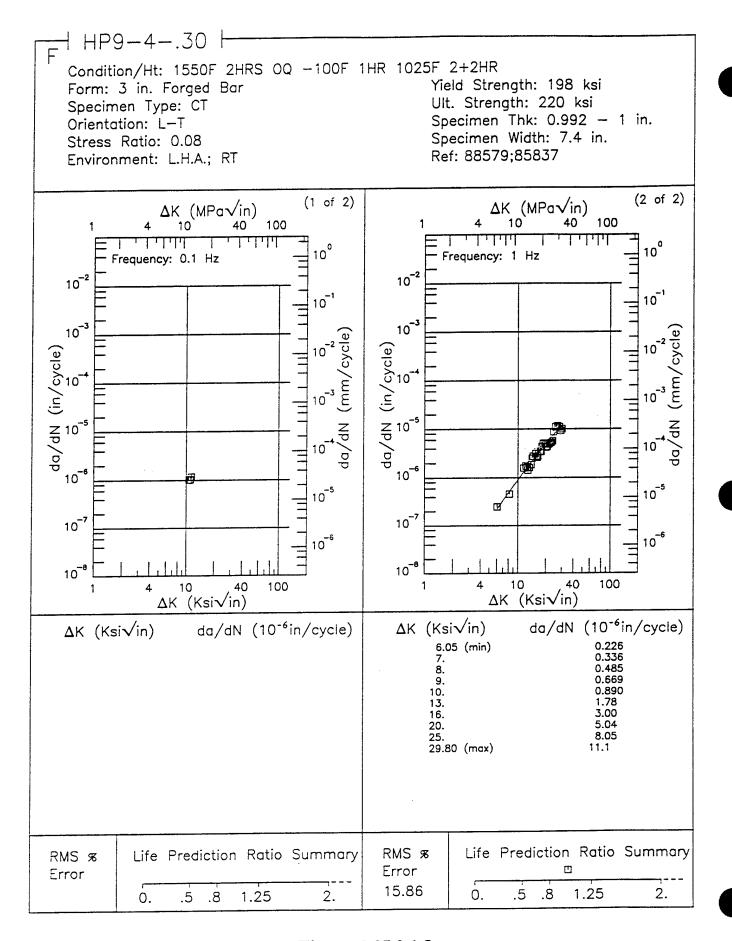


Figure 3.35.3.1.6

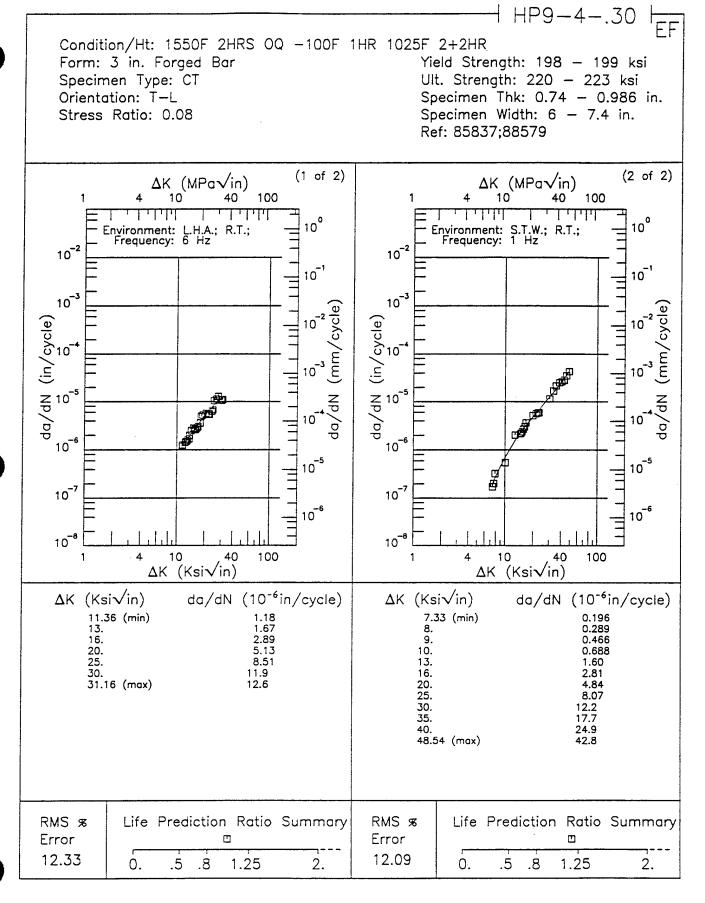


Figure 3.35.3.1.7

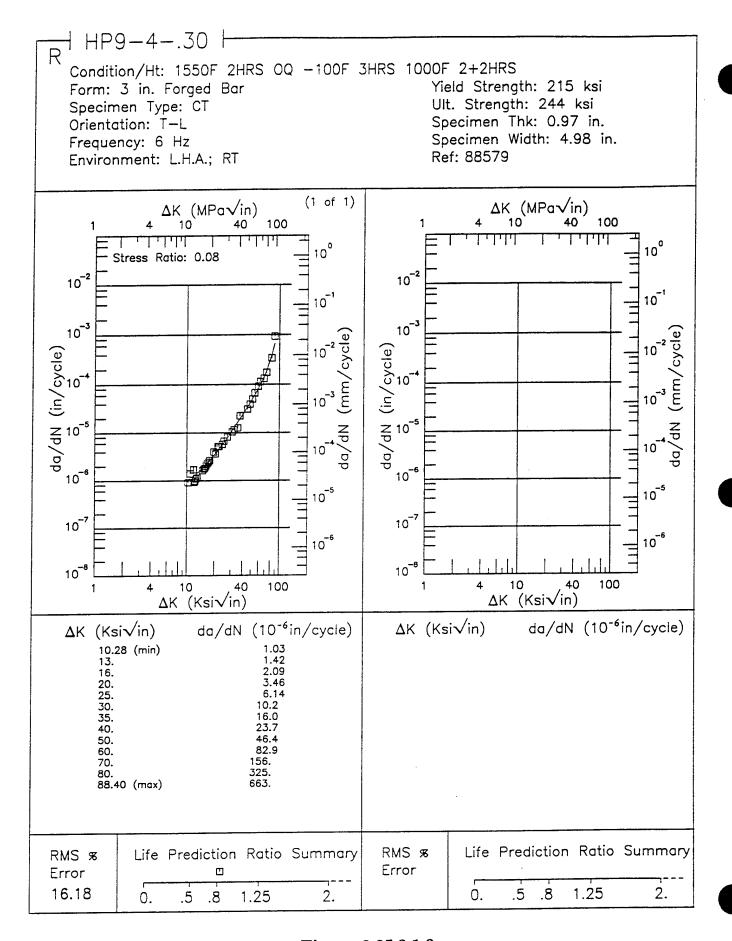


Figure 3.35.3.1.8

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HP9-4-.30Condition/Ht: UTS=220-240KSI Yield Strength: 210.5 - 212 ksi Form: 3.2 in. Billet Ult. Strength: 228.5 - 229 ksi Specimen Type: CCP (max load specified) Specimen Thk: 0.25 in. Orientation: L-T Specimen Width: 3.9 - 4 in. Frequency: 10 Hz Ref: MA007;MA010 Environment: L.H.A.; RT (2 of 3)(1 of 3)ΔK (MPa√in) Δ K (MPa \sqrt{in}) 100 10 40 40 100 10 11111 LILL 10° 10° Stress Ratio: 0. Stress Ratio: -1. 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ (mm/cycle) 10-2 da/dN (in/cycle) da/dN (in/cycle) 10 -3 10-6 10-6 10 5 10-5 10⁻⁷ 10⁻⁷ 10⁻⁶ 10 -6 10⁻⁸ 10 40 100 4 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) $da/dN (10^{-6}in/cycle)$ da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 11.75 (min) 0.729 11.76 (min) 13. 13. 16. 1.01 16. 20. 25. 30. 35. 20. 25. 30. 35. 40. 18.5 50. 60. 70. 70. 80. 99.7 90. 85.73 (max) 136. 232. 118.22 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error

Figure 3.35.3.1.9

2.

11.99

.5

0.

.8

1.25

13.30

.5

0.

.8

1.25

HP9-4-.30 | R

Condition/Ht: UTS=220-240KSI

Form: 3.2 in. Billet

Specimen Type: CCP (max load specified)

Orientation: L-T Frequency: 10 Hz Environment: L.H.A.; RT Yield Strength: 210.5 - 212 ksi Ult. Strength: 228.5 - 229 ksi

Specimen Thk: 0.25 in.

Specimen Width: 3.9 - 4 in.

Ref: MA007;MA010

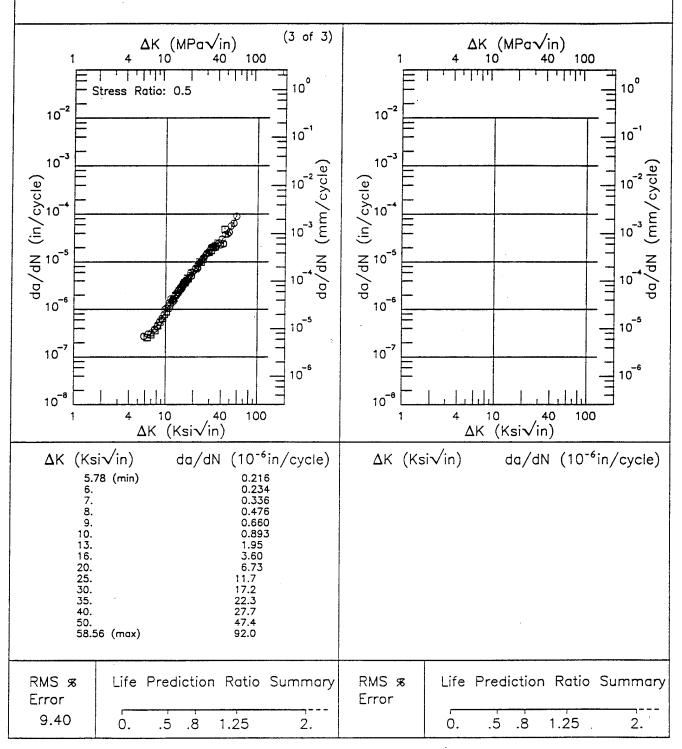


Figure 3.35.3.1.9 (Concluded)

H HP9-4-.30 H Condition/Ht: UTS=220-240KSI Yield Strength: 212 ksi Form: 3.2 in. Billet Ult. Strength: 229 ksi Specimen Type: CCP (max load specified) Specimen Thk: 0.25 in. Orientation: L-T Specimen Width: 4 in. Frequency: 0.1 Hz Ref: MA007 Environment: 3.5% NACL; RT (2 of 2)(1 of 2) $\Delta K (MPa\sqrt{in})$ Δ K (MPa \sqrt{in}) 100 40 10 100 40 10 77777 10° 10° Stress Ratio: 0.1 Stress Ratio: -1. 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁵ 10⁻⁶ 10⁻⁶ 10⁻⁵ 10 -5 10⁻⁷ 10-7 10⁻⁶ 10 6 10⁻⁸ 10 8 40 10 100 4 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) $da/dN (10^{-6}in/cycle)$ ΔK (Ksi√in) 12.78 (min) 13. 12.51 (min) 13. 16. 16. 6.12 20. 20. 25. 30. 35. 25. 30. 35. 40. 40. 50. 50. 60. 70. 60. 70. 80. 91.6 90. 166. 261. 283. 100. 93.29 (max) 120.03 (max)

Figure 3.35.3.1.10

RMS %

Error

44.06

Life Prediction Ratio Summary

1.25

2.

.5

0.

.8

2.

Life Prediction Ratio Summary

1.25

.8

.5

0.

RMS %

Error

Condition/Ht: UTS=220-240KSI

Form: 3.2 in. Billet

Specimen Type: CCP (max load specified)

Orientation: L-T Stress Ratio: 0. Yield Strength: 210.5 ksi Ult. Strength: 228.5 ksi Specimen Thk: 0.25 in. Specimen Width: 3.9 in.

Ref: MAO10

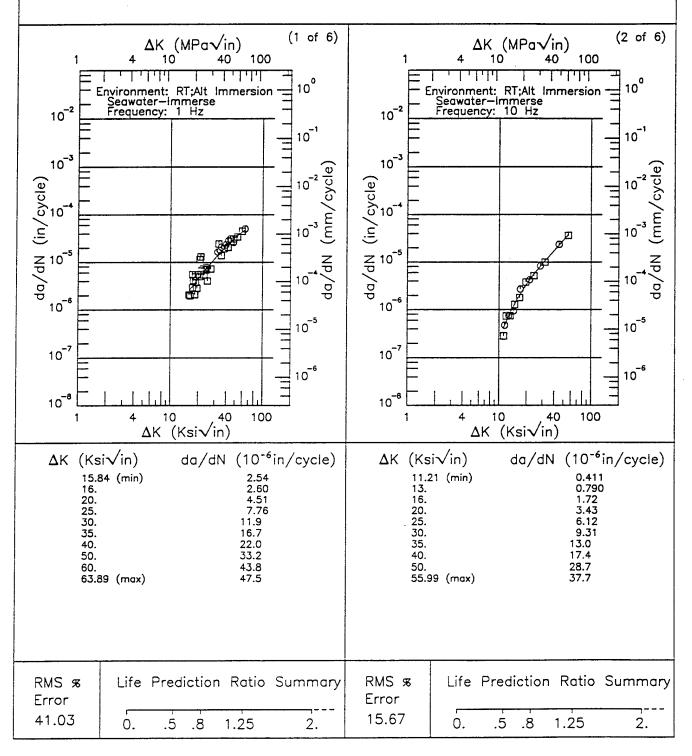


Figure 3.35.3.1.11

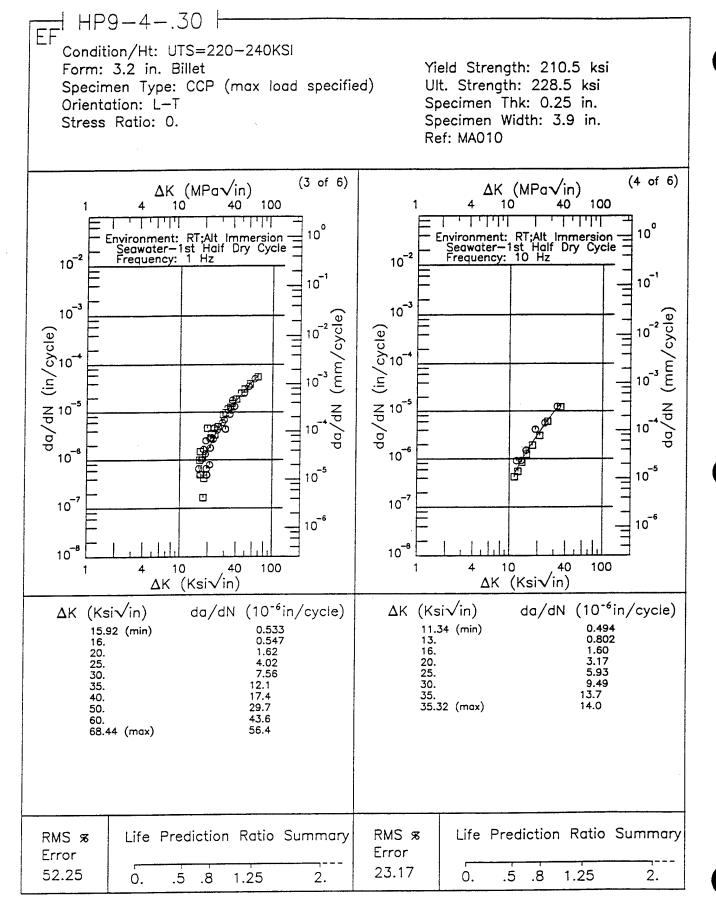


Figure 3.35.3.1.11 (Continued)

HP9-4-.30 EF Condition/Ht: UTS=220-240KSI Form: 3.2 in. Billet Yield Strength: 210.5 ksi Ult. Strength: 228.5 ksi Specimen Type: CCP (max load specified) Orientation: L-T Specimen Thk: 0.25 in. Stress Ratio: 0. Specimen Width: 3.9 in. Ref: MA010 (5 of 6) (6 of 6) ΔK (MPa√in) ΔK (MPa√in) 10 40 100 10 40 100 10° Environment: RT;Alt Immersion -Seawater—2nd Half Dry Cycle Frequency: 1 Hz Environment: RT;Alt Immersion Seawater—2nd Half Dry Cycle Frequency: 10 Hz 10-2 10-2 10-1 10 1 10⁻³ 10⁻³ da/dN (in/cycle) 10-2 da/dN (in/cycle) 10-3 ΑÑ 10 10⁻⁶ 10⁻⁶ 10⁻⁵ 10-5 10⁻⁷ 10 10⁻⁶ 10⁻⁶ 10-8 10-8 10 10 40 100 40 100 ΔK (Ksi√in) ΔK (Ksi√in) Δ K (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) $da/dN (10^{-6}in/cycle)$ ΔK (Ksi√in) 16.15 (min) 1.09 11.28 (min) 0.350 20. 25. 2.70 0.674 13. 5.59 1.53 16. 30. 8.98 20. 3.19 35. 12.6 25. 5.90 30. 9.16 16.6 40. 50. 35. 12.9 17.3 60. 40. 43.89 (max) 78.64 (max) RMS & Life Prediction Ratio Summary RMS & Life Prediction Ratio Summary Error Error 20.53 47.98 0. .5 .8 1.25 2. 0. .5 .8 1.25 2.

Figure 3.35.3.1.11 (Concluded)

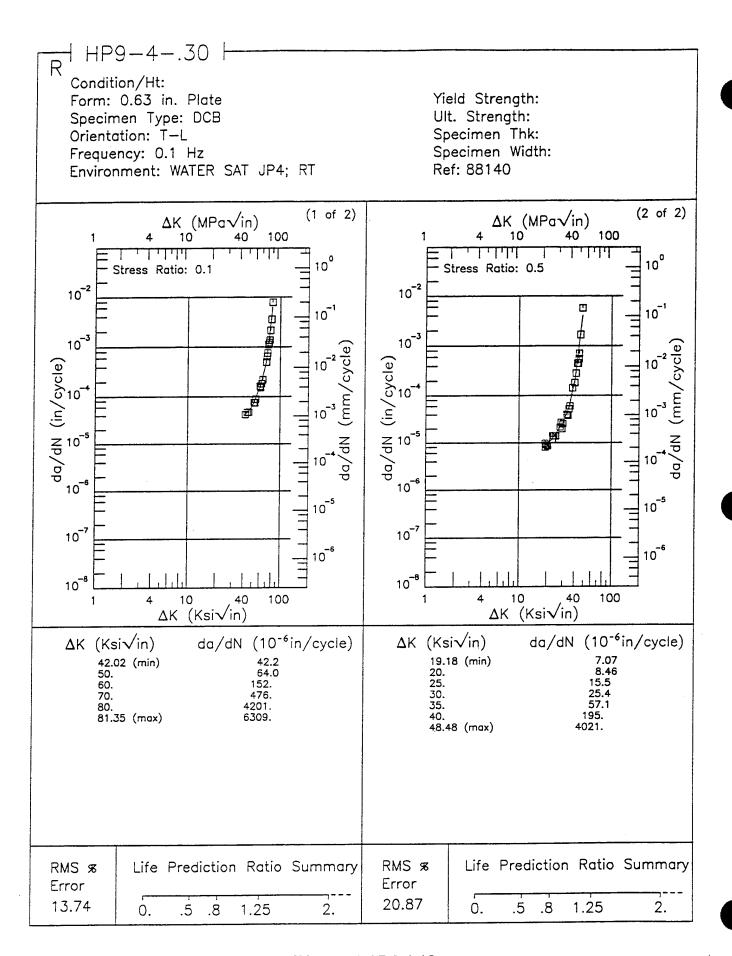


Figure 3.35.3.1.12

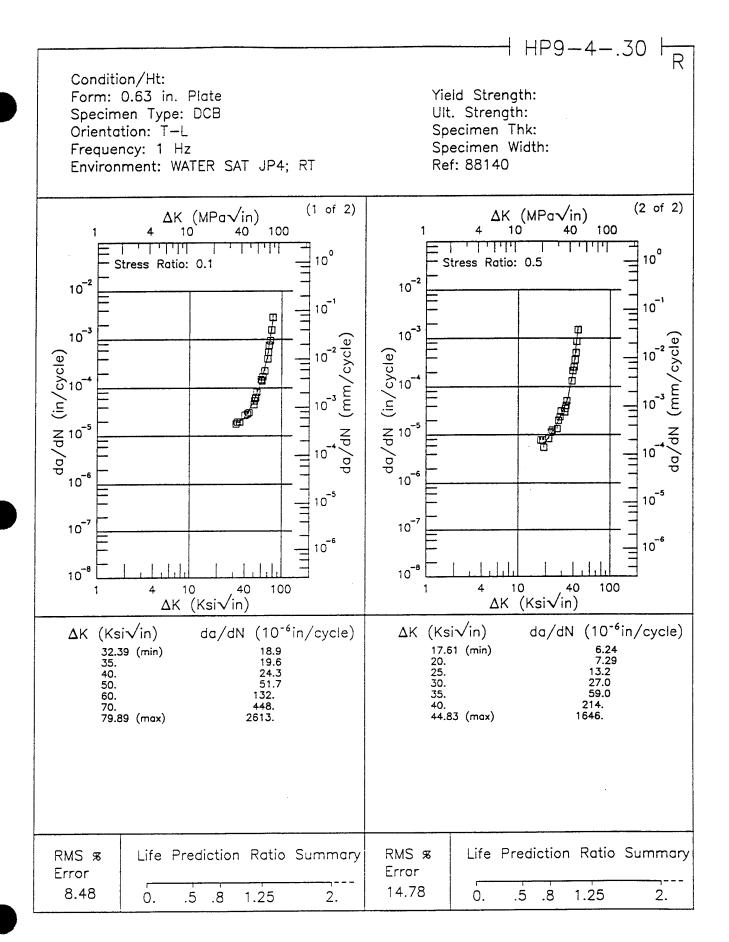


Figure 3.35.3.1.13

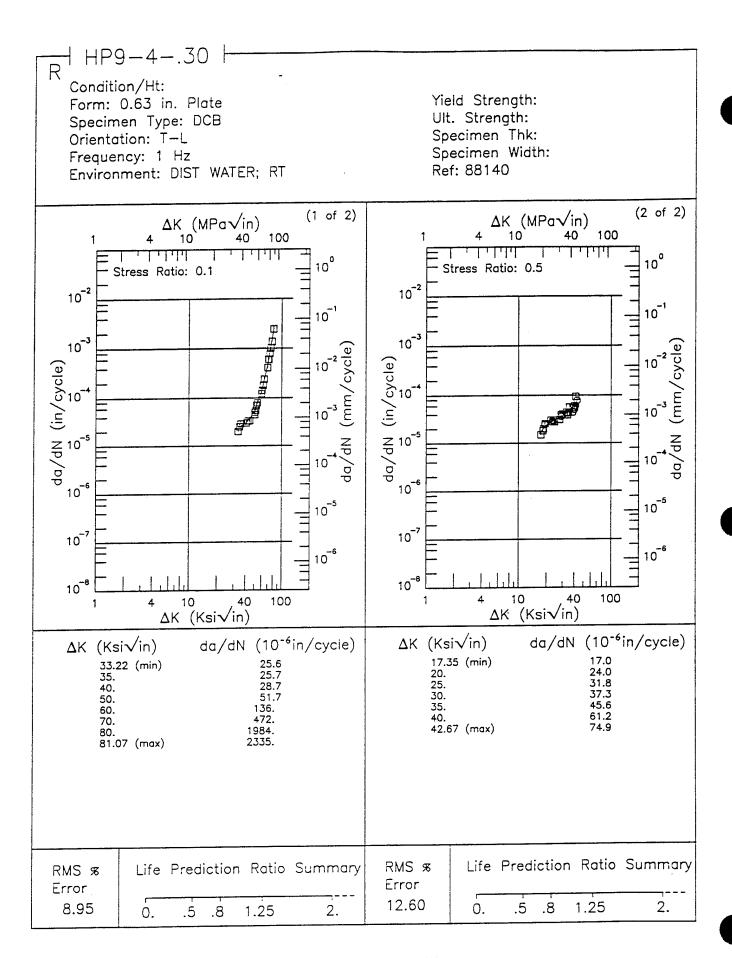


Figure 3.35.3.1.14

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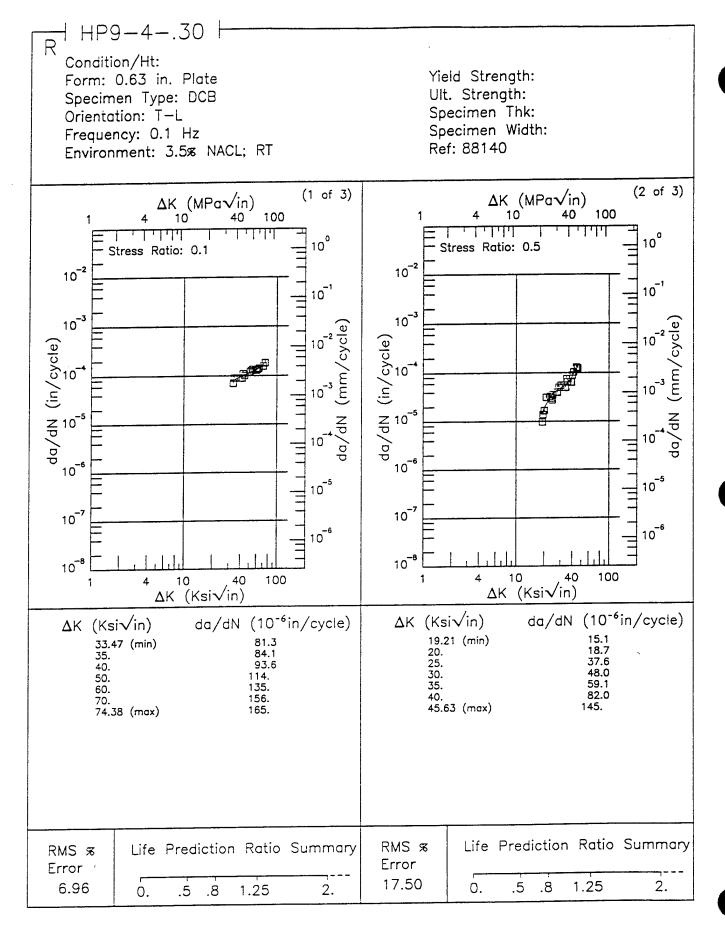


Figure 3.35.3.1.15

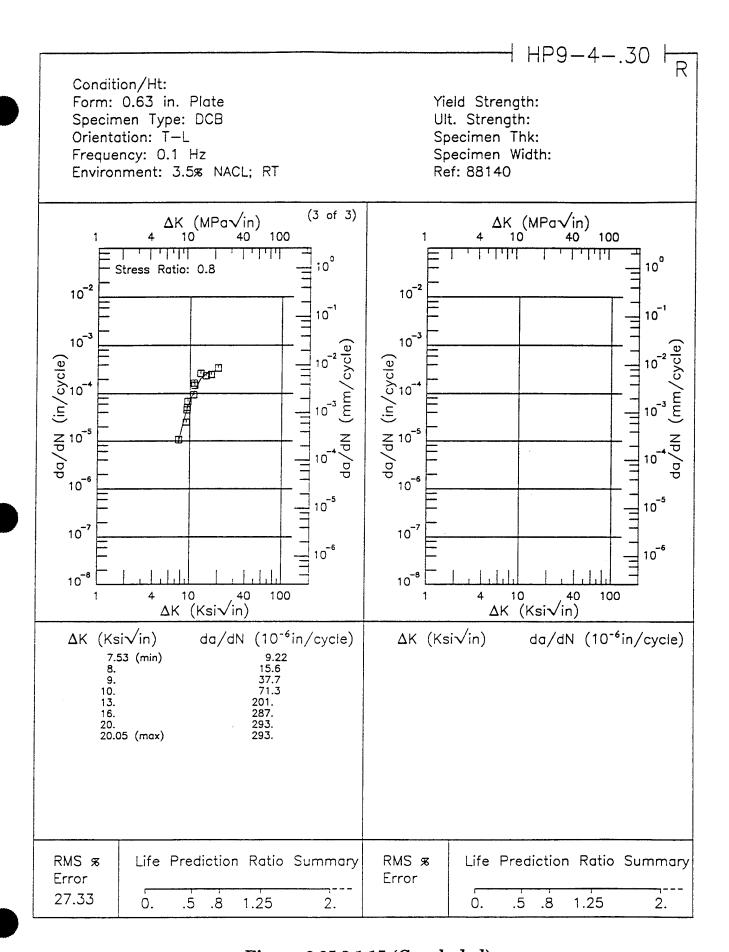


Figure 3.35.3.1.15 (Concluded)

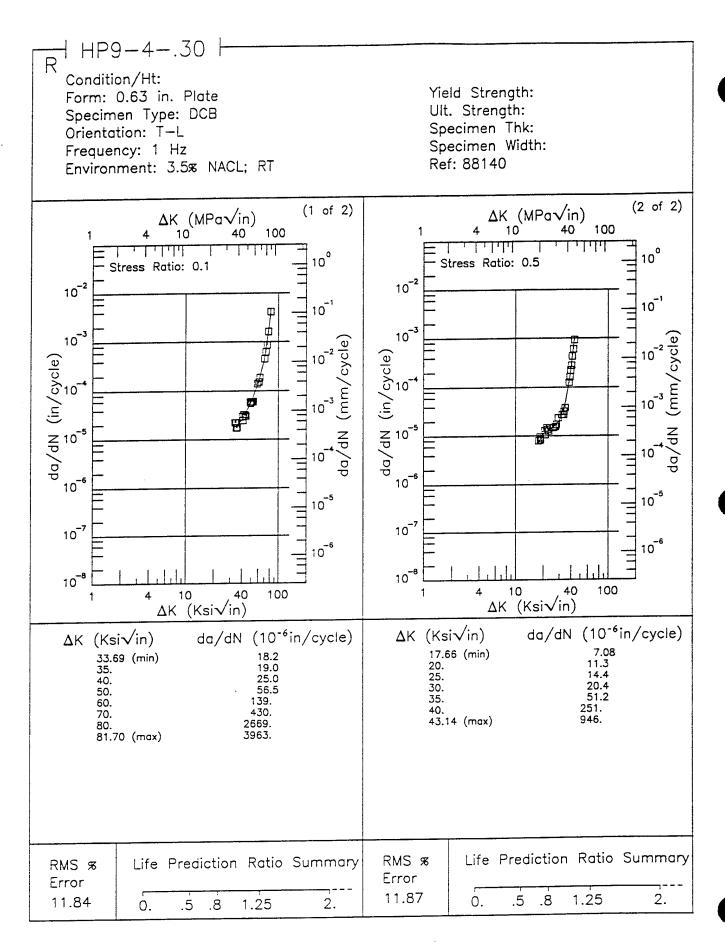


Figure 3.35.3.1.16

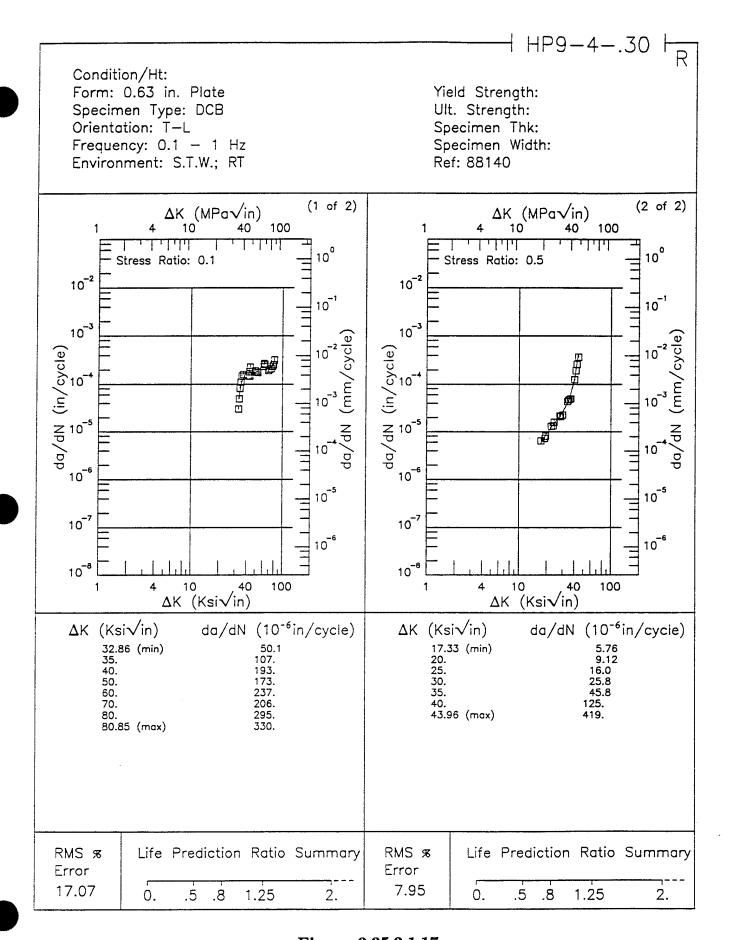


Figure 3.35.3.1.17

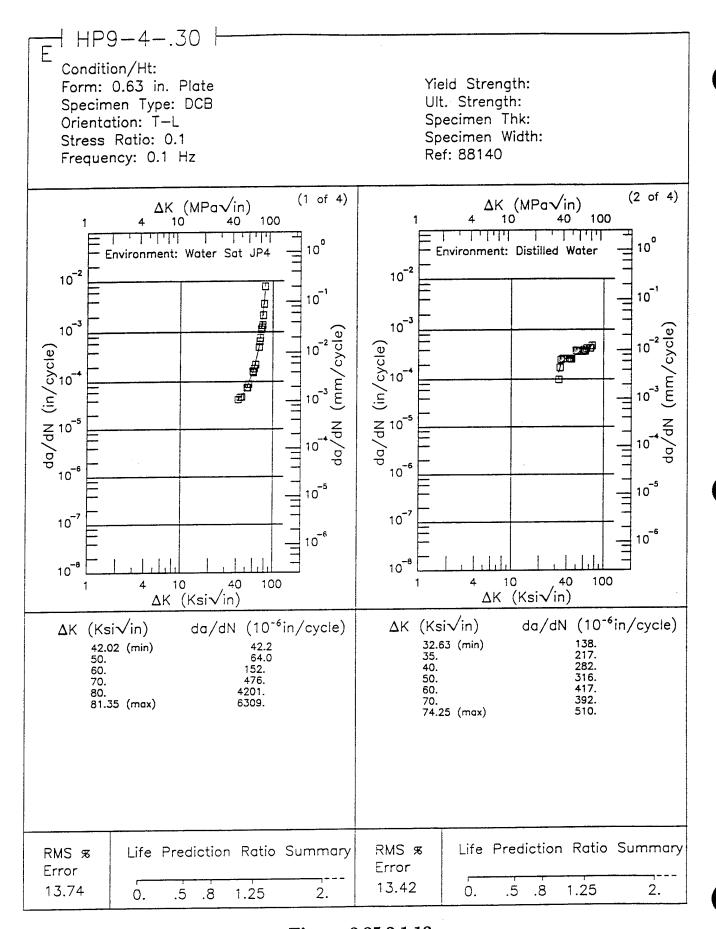


Figure 3.35.3.1.18

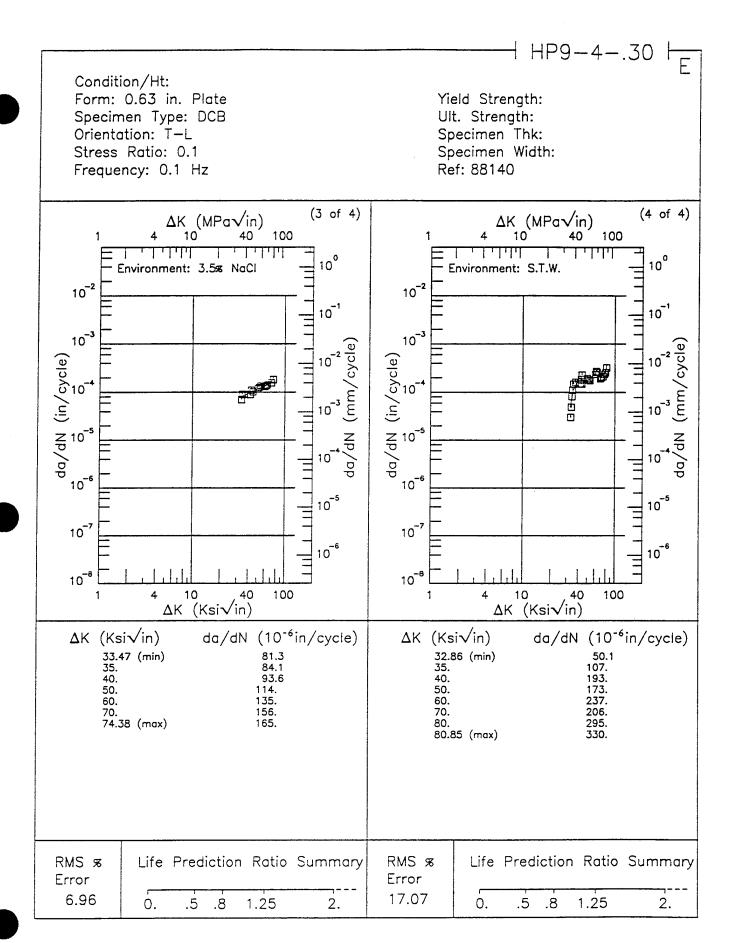


Figure 3.35.3.1.18 (Concluded)

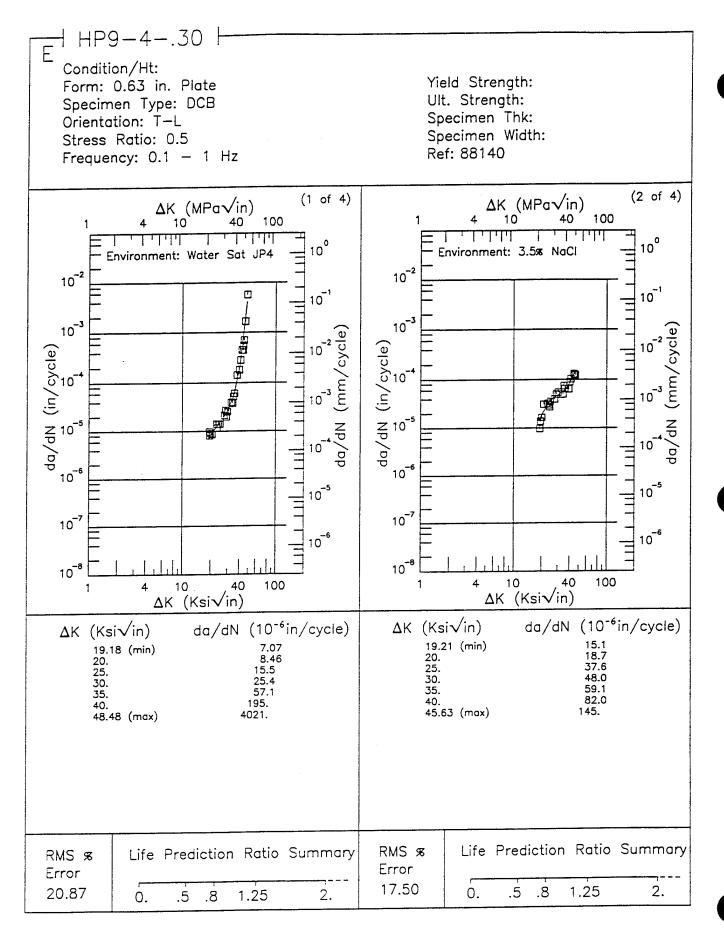


Figure 3.35.3.1.19

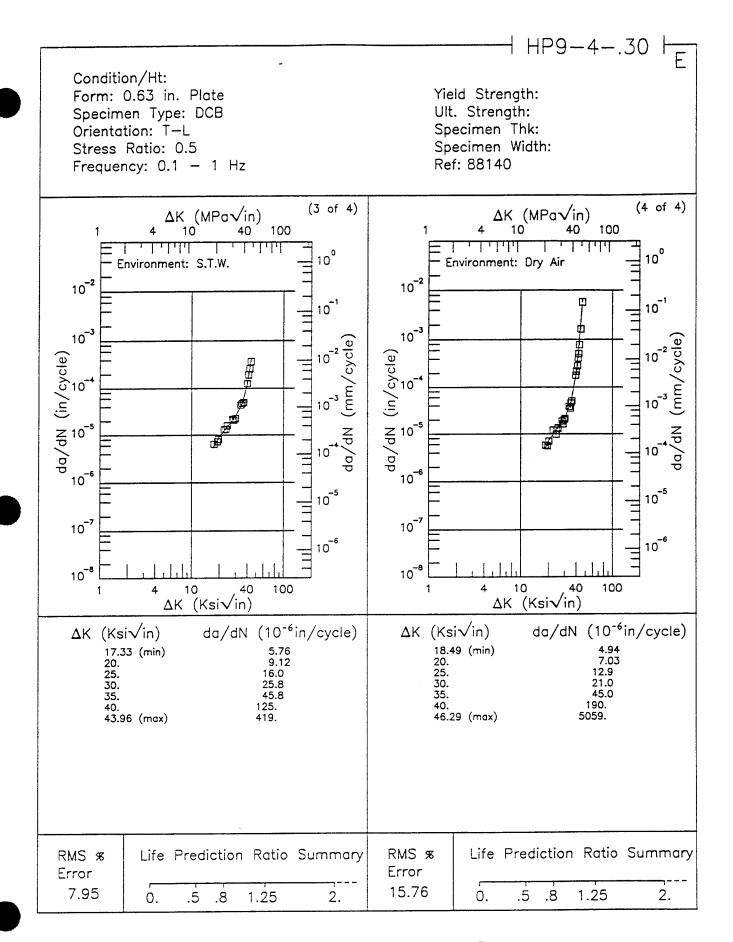


Figure 3.35.3.1.19 (Concluded)

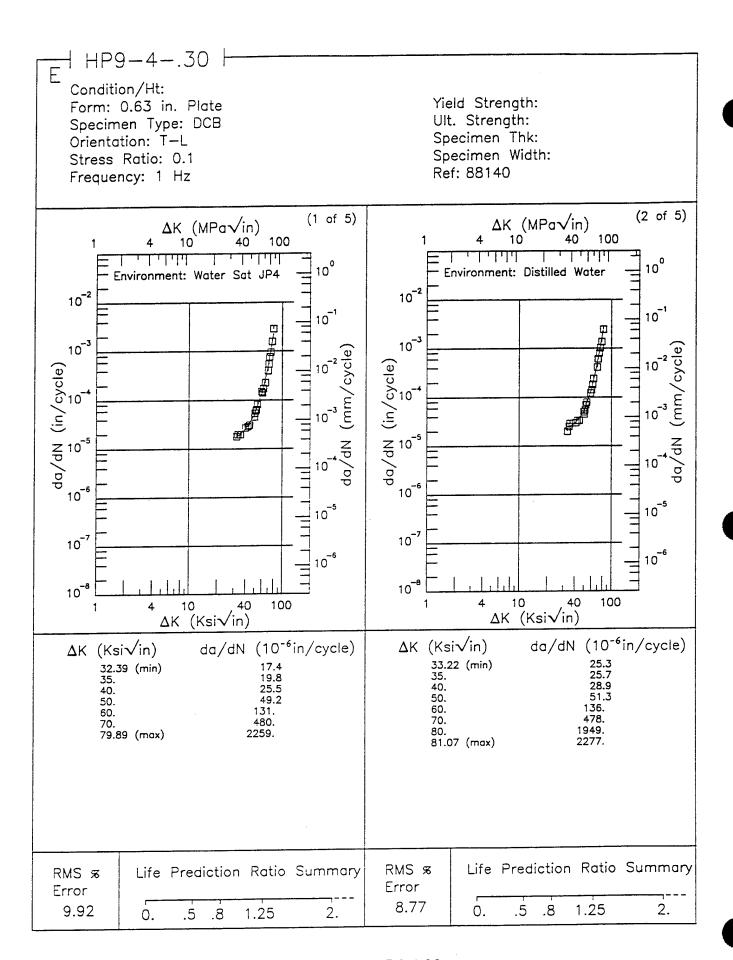


Figure 3.35.3.1.20

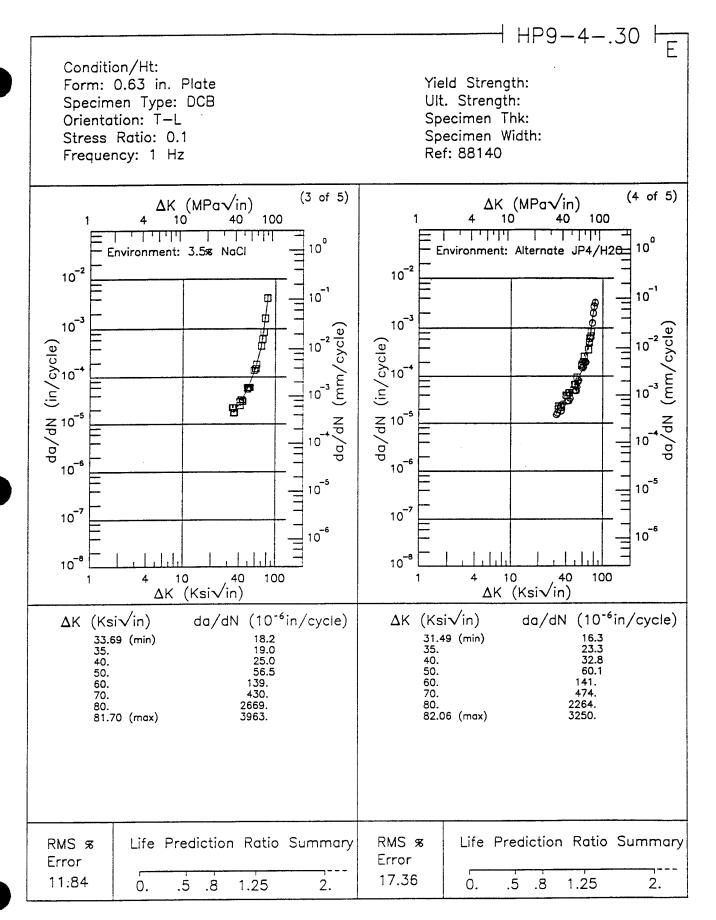


Figure 3.35.3.1.20 (Continued)

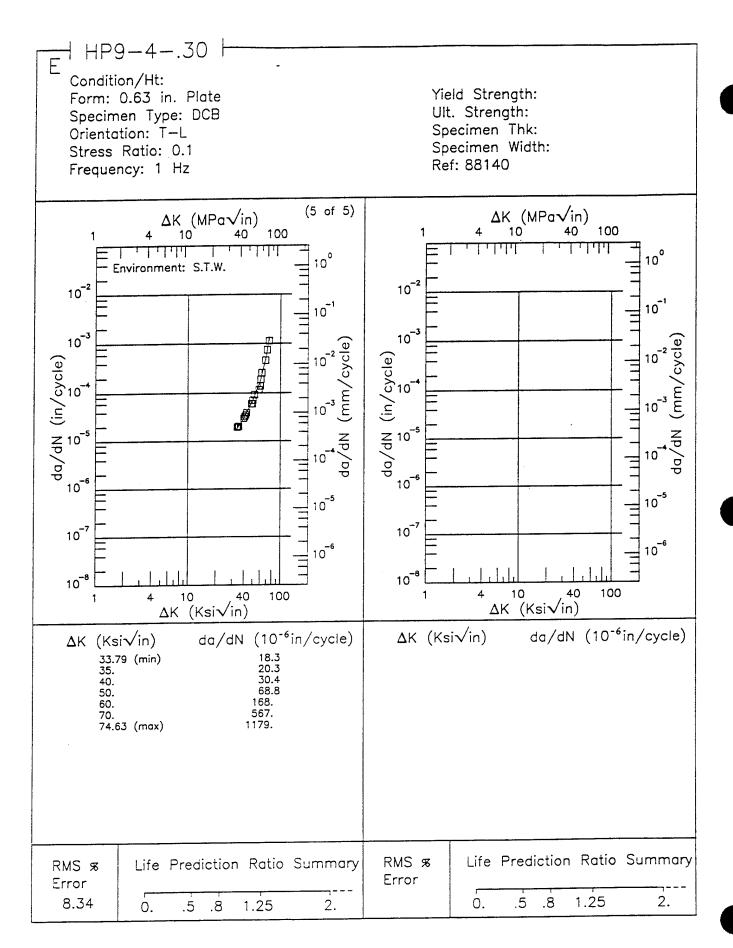


Figure 3.35.3.1.20 (Concluded)

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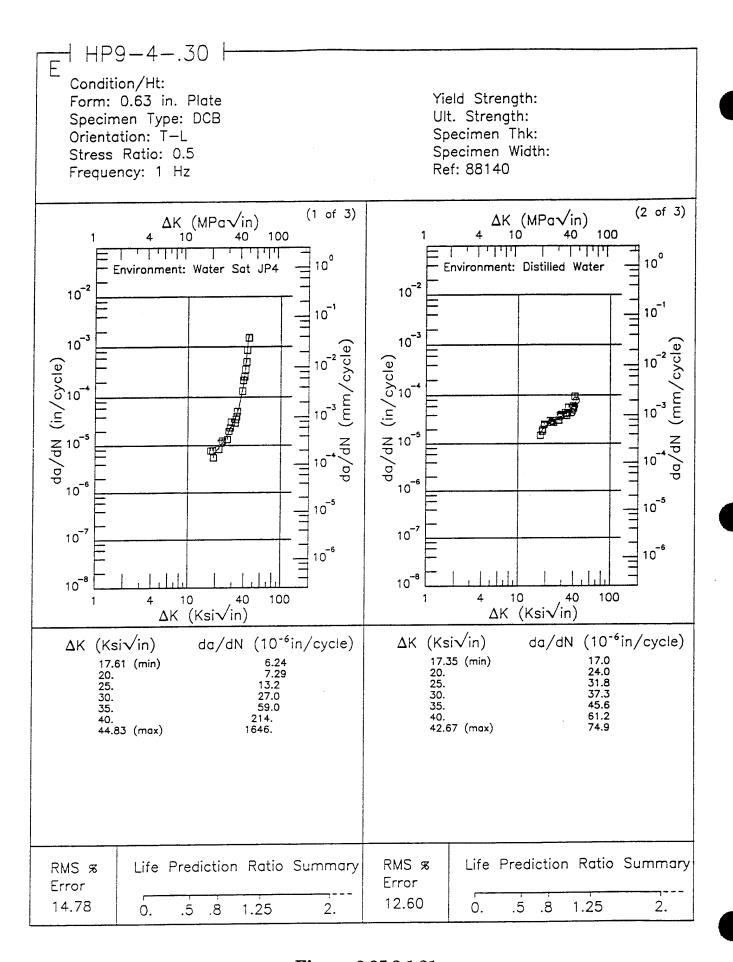


Figure 3.35.3.1.21

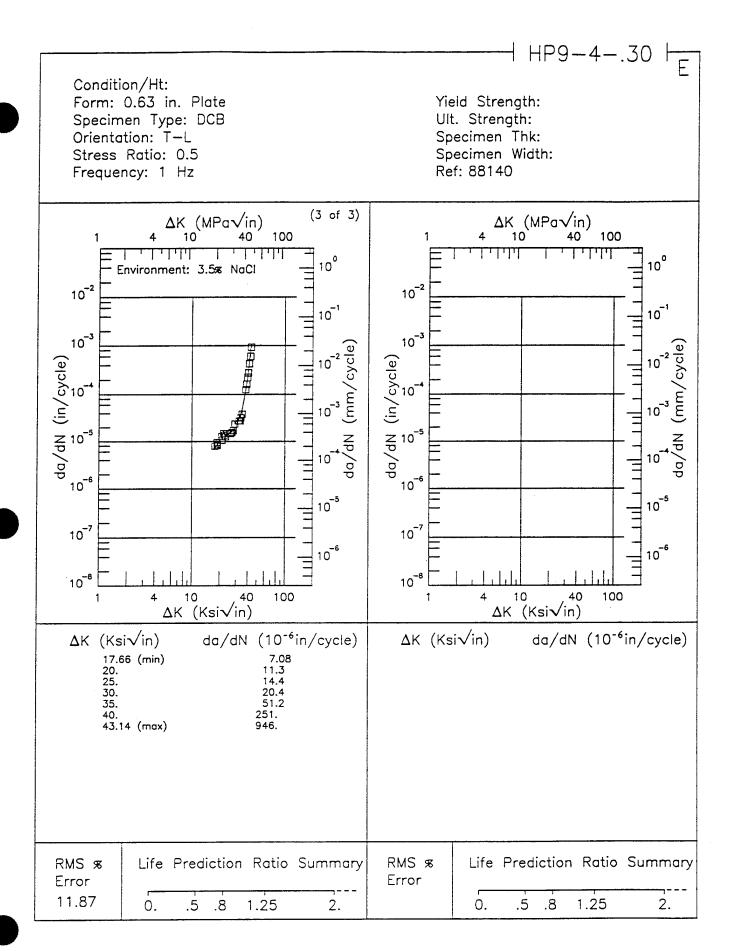


Figure 3.35.3.1.21 (Concluded)

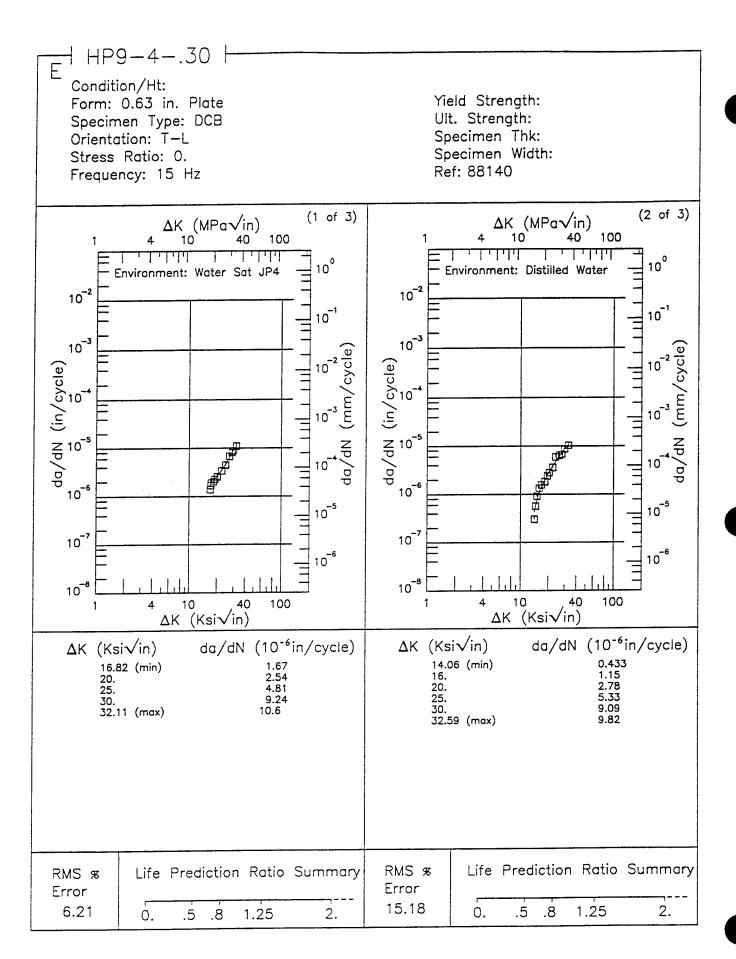


Figure 3.35.3.1.22

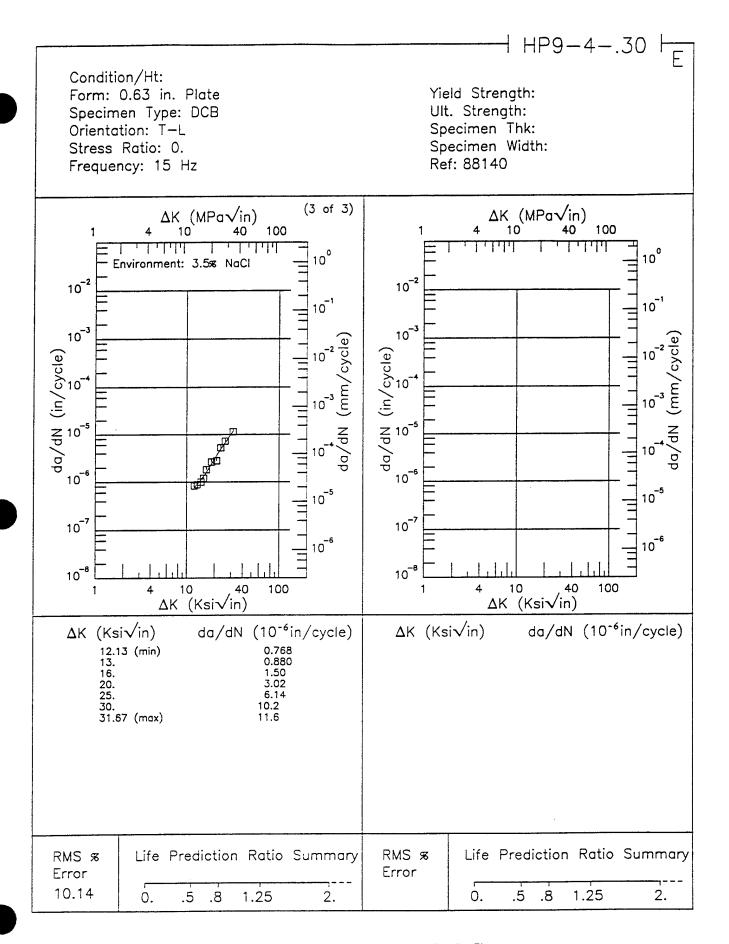


Figure 3.35.3.1.22 (Concluded)

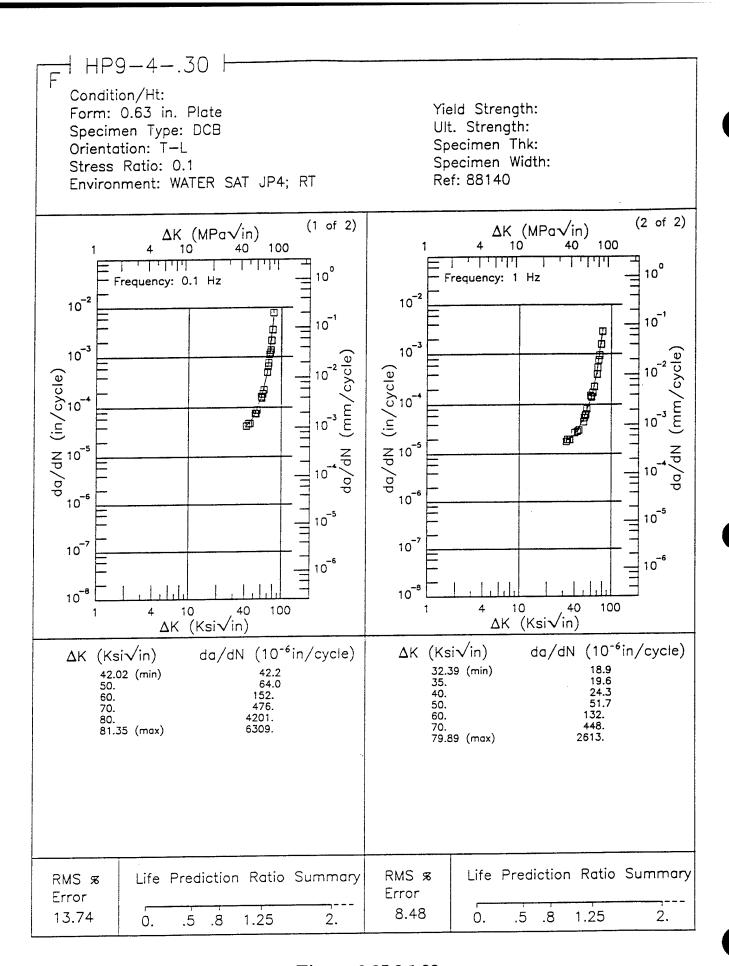


Figure 3.35.3.1.23

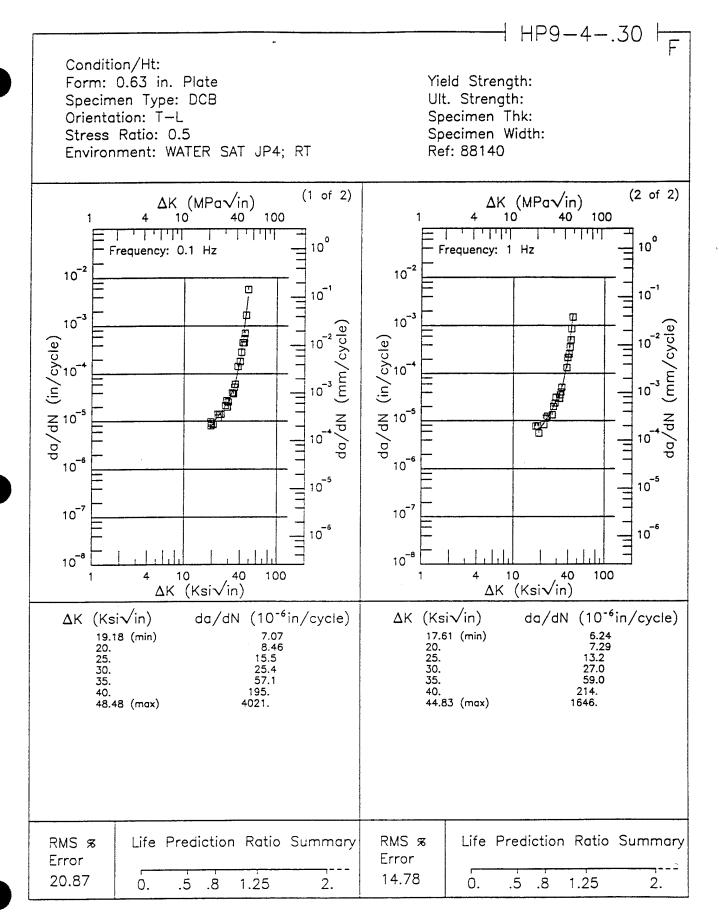


Figure 3.35.3.1.24

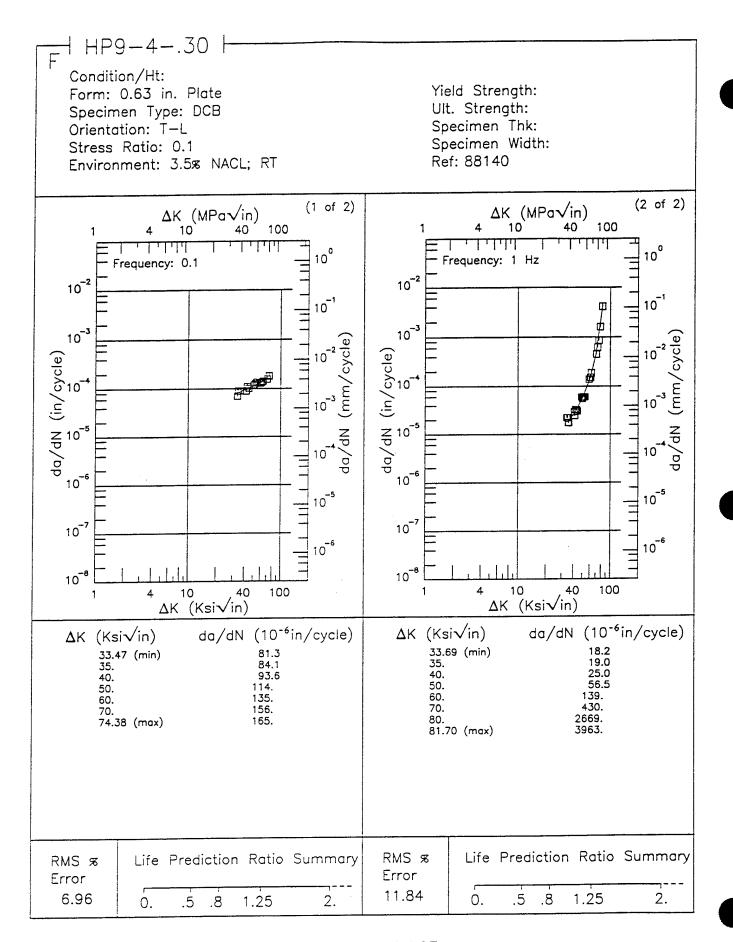


Figure 3.35.3.1.25

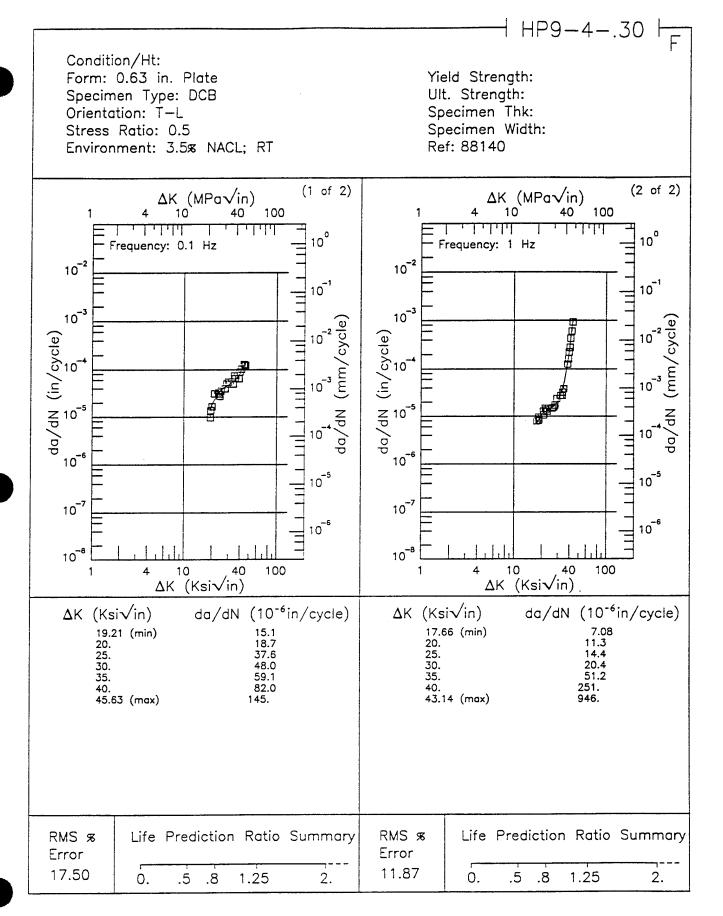


Figure 3.35.3.1.26

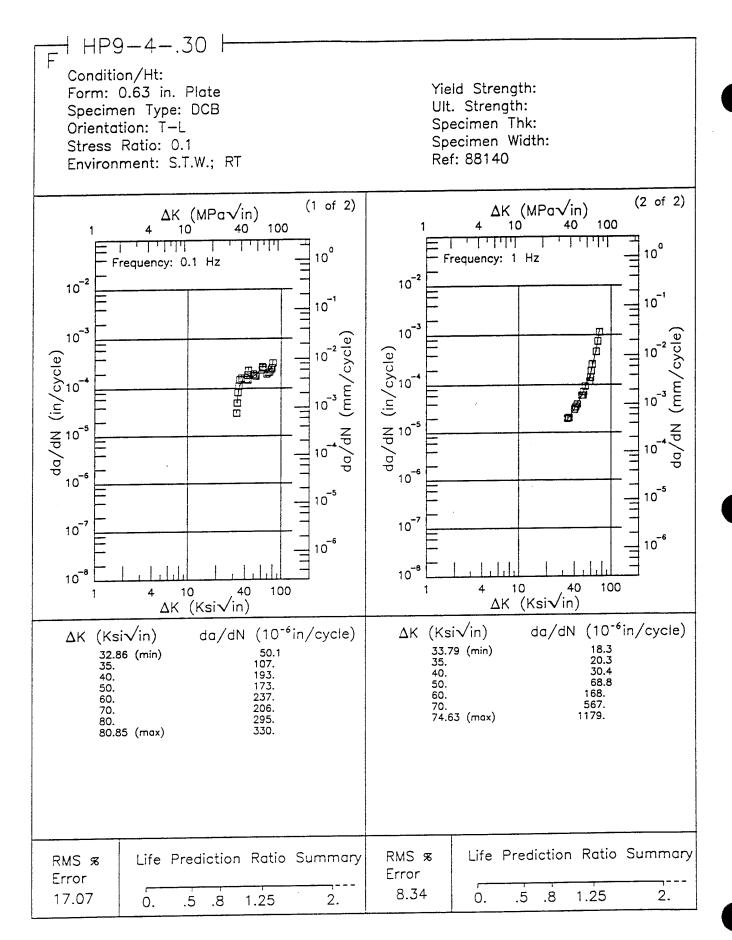


Figure 3.35.3.1.27

HP9-4-.30 F Condition/Ht: Yield Strength: Form: 0.63 in. Plate Specimen Type: DCB Ult. Strength: Orientation: T-L Specimen Thk: Specimen Width: Stress Ratio: 0.8 Ref: 88140 Environment: DRY AIR; RT (1 of 1)ΔK (MPa√in) 10 40 ΔK (MPa \sqrt{in}) 100 10 100 1111 11111 10° 10° Frequency: 1 Hz 10-2 10-2 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10-6 10 -5 10⁻⁵ 10⁻⁷ 10 7 10-6 10-6 10-8 10⁻⁸ 40 100 100 10 10 40 ΔK (Ksi√in) ΔK (Ksi√in) $\Delta K (Ksi\sqrt{in})$ da/dN ($10^{-6}in/cycle$) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) 7.57 (min) 8. 6.44 8.55 10. 35.6 13. 336. 16.27 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error 24.30 0. .5 0. .5 8. 1.25 2. .8 1.25 2.

Figure 3.35.3.1.28

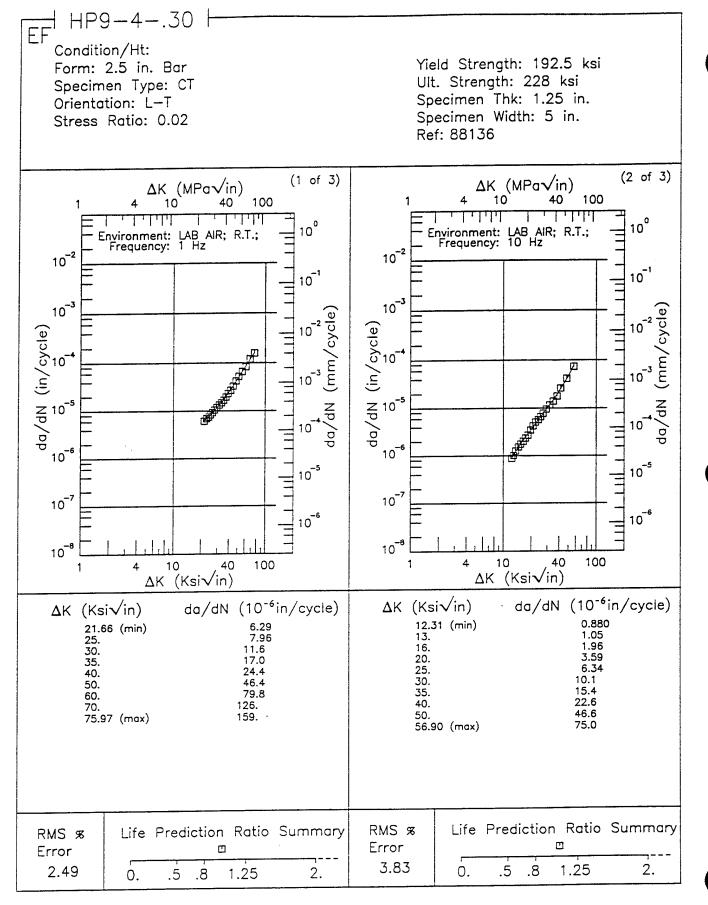


Figure 3.35.3.1.29

Condition/Ht:
Form: 2.5 in. Bar

Yield Strength: 192.5 ksi

Specimen Type: CT Orientation: L—T Stress Ratio: 0.02 Ult. Strength: 192.5 ksi Specimen Thk: 1.25 in. Specimen Width: 5 in.

Ref: 88136

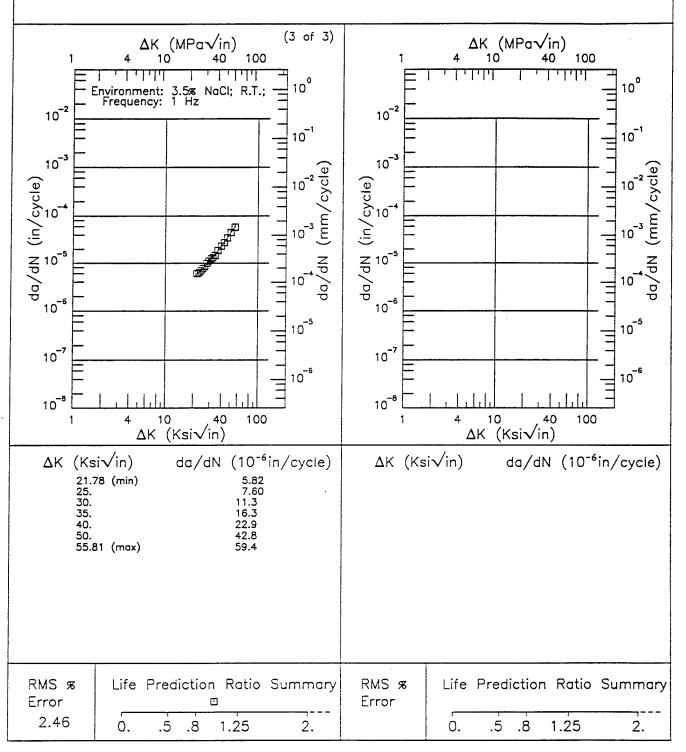


Figure 3.35.3.1.29 (Concluded)

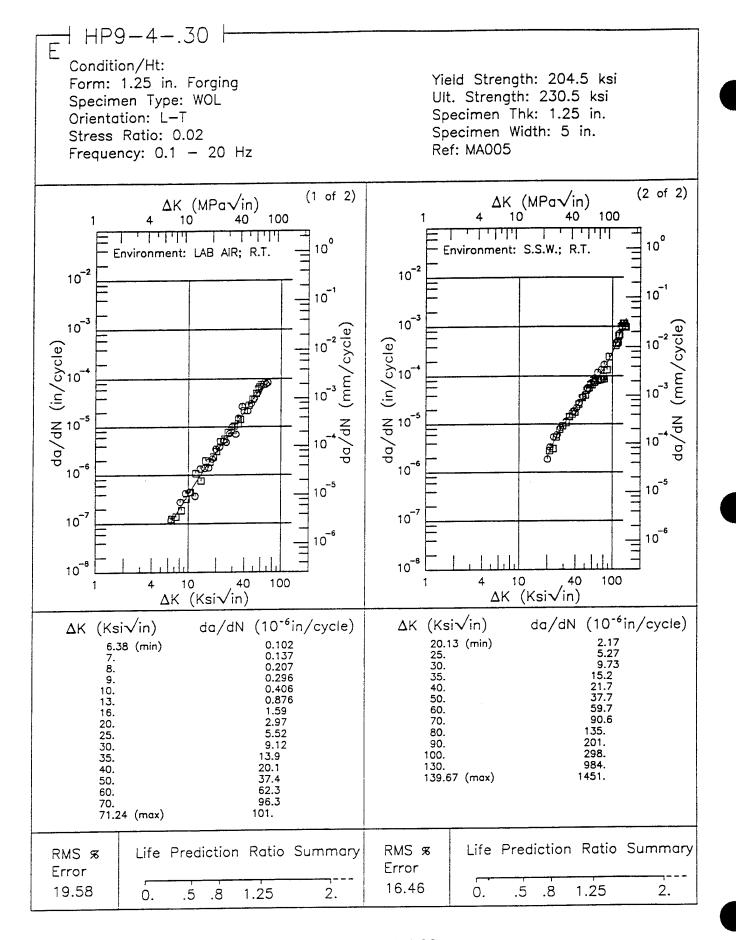


Figure 3.35.3.1.30

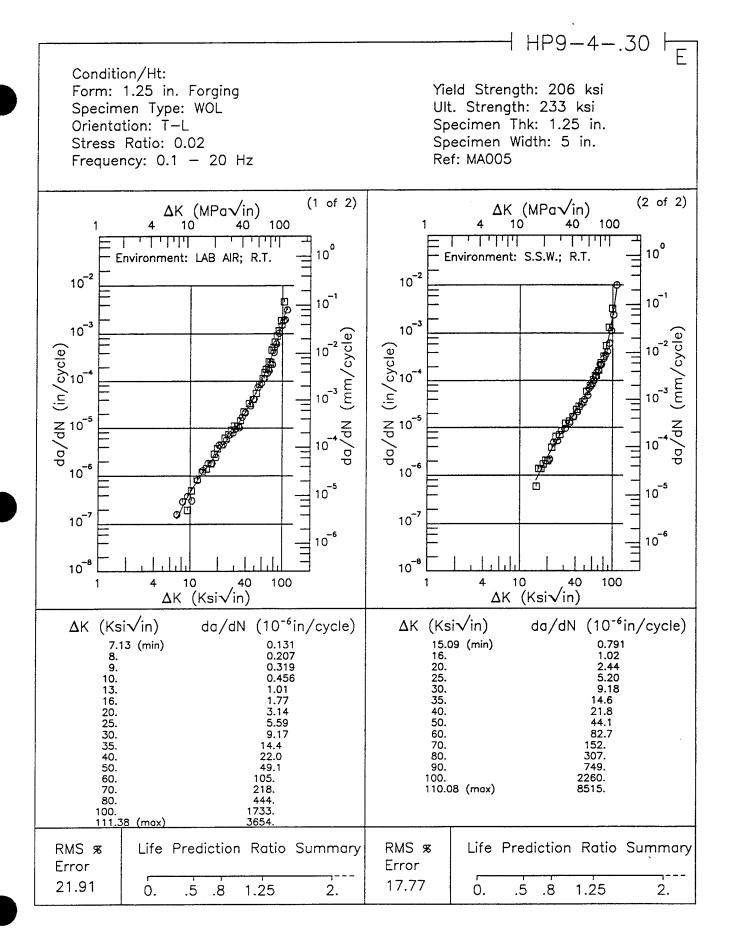


Figure 3.35.3.1.31

TABLE 3.35.3.3

K_{Isce} SUMMARY FOR ALLOY STEEL HP9-4-.30

\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	7	Test	ğ	Yield		σα	Specimen			,	1	,	Test		
Heat Treat	Form	Temp Or. Str (°F) (Ksi)	Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)	Thk (in)	Crack (in)	Crack Kq (in) (Ksi√in)	K _{lace} (Ksivin)	Time (min)	Test Date	Reference
Quenched +	٢	£		ı	3.5% NaCi	NB	1.5	5.0	0.48	0.3	116	35*	1	1961	74302
Tempered at 950°F		R. I.		200	3.5% NaCl	NB	1.5	0.48	0.48	ł	116	45	:	1961	74302
			ŀ	900	Sim. Sea	BWOL	3 085	1251	1.25	1.36		<41.3	1	1977	MAGOE
Thencoiffed	Þ	Ē	1-1	200	Water	BWOL	3.087	1.25	1.25	1.38	***	<416		1977	MAOOE
Ouspecinea	4		ē	7	Sim. Sea	BWOL	3.079	1.251	1.25	1.37		<38.6	:	1977	MA005
			D-1	204.9	Water	BWOL	3.079	1.25	1.25	1.36	i	<38.5	ţ	1977	MA005

* specimen thickness does not meet minimum requirements of $2.5~(rac{K_{L\infty}}{\sigma_{yy}})^2$

TABLE 3.36.3.3

K_{Isco} SUMMARY FOR ALLOY STEEL HP9-4-.45

	F	Test	7	Yield		S	Specimen		Prod	,		;	Test	·	
Condition/ Heat Treat	Form	Temp (°F)	Or. (Ksi)	Str (Ksi)	Envir.	Design	Width (in)	Width Thick (in) (in)	Thk (in)	Crack (in)	Crack No had (Ksivin)	_{Niso} (Ksi√in)	Time (min)	Test Date	Reference
1600°F 0.5hr AC;	٥	Ę		2,0	3N NaGl	CNT	2	0.05	0.05 0.08		1	35*	30000 1968	1968	72283
1500°F 0.33hr AC	Ω	K. I.	1	212.0	Dist. Water	CNT	7	0.05	0.08	;	1	+88	20000	1968	72283
475°F	ď	R.T.	ı	220	3.5% NaCl	NB	1.5	0.48 0.48 0.3	970	6.9	88	08	1	1971	84351

* specimen thickness does not meet minimum requirements of 2.5 $(\frac{K_{loc}}{\sigma_{rs}})^2$

TABLE 3.37.3.3

K_{lsc} SUMMARY FOR ALLOY STEEL HY-150

	2	Test	8	Yield		S	Specimen		Prod	,	;		Test		
Heat Treat	Form	Temp Or. Str (°F) Or. (Ksi)	Or.	Str (Ksi)	Envir.	Design	Width Thick (in)	Thick (in)	Thk (in)	Crack (in)	Crack Kq (in) (Ksivin) (K _{isœ} (Ksi√in)	Time (min)	Test Date	Reference
1500°F 1hr WQ	P	R.T.	-	150	3.0% NaCl CANT	CANT*	2	1	1	0.2		115+	30000	1968	73824

* specimen thickness does not meet minimum requirements of 2.5 $(\frac{K_{loc}}{\sigma_{rs}})^2$

* asterisk in specimen design column indicates that specimens are side-grooved

TABLE 3.38.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HY-180 AT ROOM TEMPERATURE

ORIENTATION: L-T

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ENVIRONMENT:	
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			100.0				
[e]		3	50.0	30.82			
8 in/eya		(Ksh/in	20.0	4.29	3.72	5.61	4.5
PCGR (10 ⁻⁸ in/cycle)		ΔK Lovel (Ksi√in)	10.0		0.48		0.53
PC		N	8.0		0.11		0.11
			8.5				
	FREQ	(Hz)		10	30	10	30
	2	2		0.1	0.1	0.5	0.5
	PRODUCT	FORM			are describe	FORGED BAR	
	CONDITION/	HEAT TREATMENT			CONA 17 WING	01A(01S=100NS)	

⊣ HY-180 | Condition/Ht: STA (UTS=180KSI) Yield Strength: 197.1 ksi Form: 1.75 in. Forged Bar Ult. Strength: 199.6 ksi Specimen Type: CT Specimen Thk: 0.377 in. Orientation: L-T Specimen Width: 1.5 - 1.501 in. Frequency: 10 Hz Ref: DA001 Environment: LAB AIR; RT (2 of 2) (1 of 2) $\Delta K (MPa\sqrt{in})$ $\Delta K (MPa\sqrt{in})$ 10 40 100 100 10 40 111111 1 1 1 1 1 1 1 10° 10° Stress Ratio: 0.5 Stress Ratio: 0.1 10⁻² 10-2 10-1 10-1 10-3 10⁻³ 10-2 da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10-6 10⁻⁵ 10⁻⁵ 10⁻⁷ 10-7 10⁻⁶ 10⁻⁶ 10⁻⁸ 10⁻⁸ 40 100 10 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) Δ K (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 11.51 (min) 13. 16. 10.71 (min) 0.899 0.645 13. 3.37 16. 5.61 20. 20. 25. 30. 25. 30. 7.04 10.1 35. 35. 13.6 40. 40. 43.61 (max) 30.8 50. 59.28 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS \$ RMS & Error

Figure 3.38.3.1.1

2.

5.54

0.

.5

.8

1.25

2.

8.

1.25

Error

3.54

0.

.5

HY-180 R

Condition/Ht: STA (UTS=180KSI)

Form: 1.75 in. Forged Bar

Specimen Type: CT Orientation: L—T Frequency: 30 Hz

Environment: LAB AIR; RT

Yield Strength: 197.1 ksi Ult. Strength: 199.6 ksi Specimen Thk: 0.253 in. Specimen Width: 1.5 in.

Ref: DA001

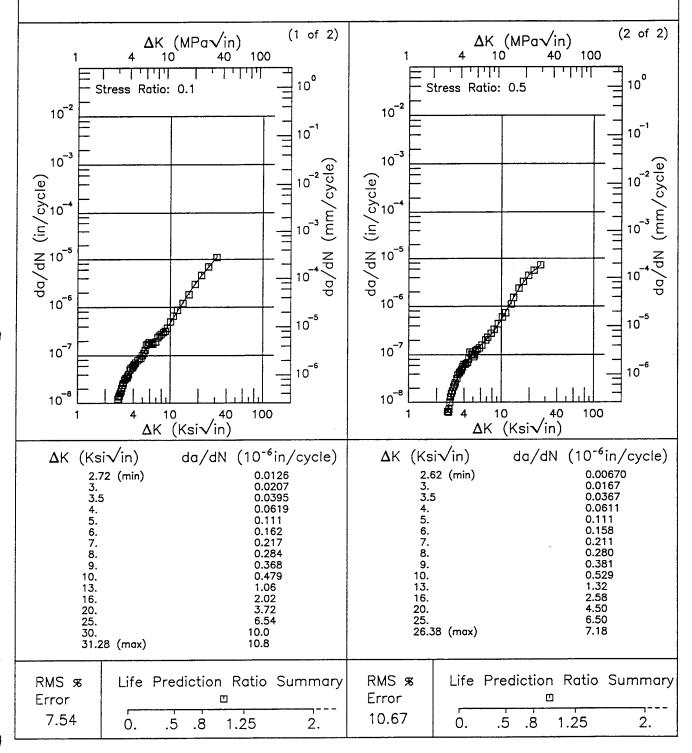


Figure 3.38.3.1.2

TABLE 3.39.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK HY-80 AT ROOM TEMPERATURE

			100.0	
			-	
			60.0	28.1
	(9)	1)	Z	ಷ
<u></u>	Cyc.	ħ/ti	-	
ENVIRONMENT: 3.5% NaCl	PCGR (10 ^d in/cycle)	AK Lovel (Kst/in)	10.0 20.0	
7 %	_# 01	rel		
3.5	B (1	Lo	0.0	
Ë	20	H.		
A	A	7	2.5 5.0	
Ž				
S				
K			oi.	
E	0	,		
	FREO	(Hz)		0.5
	3	0		
		¥		0.1
	CT	I		ED
	PRODUCT	FORM		UNSPECIFIED
ified	30	O M		INSPI
eci	Id			٦
ısp				
Ur				
Ä		Ę		
TI	/X	NE S		
TA	OH	ATI		UNSPECIFIED
E		RE		PECI
ORIENTATION: Unspeci	CONDITION	HEAT TREATMENT		SND
٦	ŭ	EA.1		
		H		

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HY-80 Condition/Ht: Yield Strength: Form: Ult. Strength: Specimen Type: WOL Specimen Thk: 0.4 in. Orientation: Specimen Width: 2.55 in. Frequency: 0.5 Hz Ref: UD007 Environment: 3.5% NACL; RT (1 of 1) $\Delta K (MPa\sqrt{in})$ $\Delta K (MPa\sqrt{in})$ 100 10 40 100 10° 10° Stress Ratio: 0.1 10-2 10-2 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) 10 -2 da/dN (in/cycle) 10-3 10 10⁻⁶ 10⁻⁶ 10 -5 10-7 10⁻⁷ 10 -6 10-6 10-8 10-8 10 40 100 40 10 100 $\Delta K (Ksi\sqrt{in})$ ΔK (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) da/dN (10⁻⁶in/cycle) ΔK (Ksi \sqrt{in}) ΔK (Ksi√in) 24.02 (min) 25. 30. 5.47 5.88 8.35 35. 28.1 50. 48.0 60. 70. 77.74 (max) 79.2 Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error .5 .8 1.25 2. 9.21 0. 0. .5 .8 1.25 2.

Figure 3.39.3.1

TABLE 3.40.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR ALLOY STEEL HY-TUF AT ROOM TEMPERATURE

Product					K_{Ic}	$K_{Ic}~(ksi\sqrt{in})$	<u>a</u>)			
Form	Condition/Heat Treatment			Sa	pecime	Specimen Orientation	ıtation			
			L-T			T-T			T-S	
		Mean K _{le}	Std Dev	и	Mean K _{le}	Std Dev	u	Mean K _{le}	Std Dev	u
Forging	1700F 1HR AC 1600F 1HR OQ 550F 2HR	:		•••	111.5	2.1	73	:	ŀ	

TABLE 3.40.2.1

		<u> </u>			-	
	RBFER	91284	91284	91284	91284	91284
	DATE	1974	1974	1974	1974	1974
	STAN DEV	i		2.1	1	ļ
Kı	K. MBAN	ı		111.5	-	ŀ
	K. (Kai • √in.)	116.00	110.00	113.00	120.00	113.00
	(K _{e,} /TYS) ² (in.)	98'0	0.76	0.81	0.92	0.80
CRACK	LENGTH (in.) A	0.983	0.977	0.973	0.988	0.977
7	DESIGN	cr	CT	СТ	CT	CT
SPECIMEN	THICK (in.) B	1.000	1.003	1.003	1.003	1.003
9	WIDTH (in.)	1.999	1.999	1.999	1.999	1.999
	YIRLD STR (Kei)	198.0	198.0	198.0	198.0	200.0
	SPEC		, II	Т·Г	LТ	T-L
	TEST TEMP (°F)		E	K.T.	R.T.	R.T.
UCT	THICK (in.)	6.50	6.50	6.50	6.50	9:90
PRODUCT	FORM	Forging	į.	rorging	Forging	Forging
	CONDITION	1700F 1HR AC 1600F 1HR OQ 550F 2HR	1700F 1HR AC 1600F 1HR OQ	660F 2HR	1700F 1HR AC 1600F 1HR + 1000F 20 MIN	1700F 1HR AC 1600F 1HR + 1000F 20 MIN

TABLE 3.41

REFERENCES FOR ALLOY STEEL DATA

60578 18Ni(300)(MAR) K,

> Christian, J. L., Yang, C. T., and Witzell, W. E., "Physical and Mechanical Properties of Pressure Vessel Materials for Application in a Cryogenic Environment", ASD-TDR-62-258, Part III, General Dynamics/Astronautics (December 1964).

63061 18Ni(300)(MAR) 4140

K_{Iscc} K_{Iscc} K_{Iscc} 4340 D6AC

Mulherin, J. H., and Hess, E. H., "Stress-Corrosion Susceptibility of Ultrahigh Strength Steel Evaluated in Terms of Fracture Toughness", Technical Report R-1782, Frankford Arsenal, Philadelphia, PA, (November 1965).

65166 12Ni-5Cr-3Mo K_{lscc} 18Ni(180)(MAR)

18Ni(250)(MAR)

Rolfe, S. T., et al., "Stress-Corrosion Testing of Ultraservice Steels Using Fatigue Cracked Specimens", Paper No. 90, Presented at the 69th Annual Meeting of the American Society for Testing and Materials in Atlantic City, NJ, June 27-July 1, 1966.

69162 18Ni(200)(MAR) K

> Sandoz, G., and Newbegin, R. L., "Stress-Corrosion Cracking Resistance of an 18Ni 200 Grade Maraging Steel Base Plate and Weld", NRL Report 1772, Naval Research Laboratory, Washington, D.C., (March 1967).

70887 12Ni-5Cr-3Mo K_{lscc} 18Ni(200)(MAR) da/dt 18Ni(250) da/dt; K_{iscc}

4340

Peterson, M. H., Brown, B. F., Newbegin, R. L., and Groover, R. E., "Stress Corrosion Cracking of High Strength Steels and Titanium Alloys in Chloride Solutions at

Ambient Temperature", Corrosion, 23 (5), 142-148 (May 1967).

72283 18Ni(250)(MAR) 4340 D6AC H11 HP9-4-.45

> Benjamin, W. D., and Steigerwald, E. A., "Environmentally Induced Delayed Failures Martensitic-High-Strength Steels", Second Yearly Summary Report, AFML-TR-68-80, TRW, Inc., Cleveland, OH, Contract AF33(615)-3651(P) (April 1968).

73300	300M (AM)	K_{Ic}
	300M (VAR)	K_{ic}
	4340 (AM)	K_{lc}
	4340 (DH)	K_{Ic}
	4340 (VAR)	K_{tc}

Hauser, J. J., et al., "Inclusions in High-Strength Steels, Their Dependence on Processing Variables and Their Effect on Engineering Properties", Report AFML-TR-66-222, Crucible Steel Corporation, Pittsburgh, PA, (August 1968).

73612 18Ni(250)(MAR) K_{Ic}

Srawley, J. E., "Plane Strain Fracture Toughness Tests on Two-Inch-Thick Maraging Steel Plates at Various Strength Levels", NASA TN K-52470, Lewis Research Center, Cleveland, OH, (1968).

73824 HY-150 K_{Iscc}

Smith, J. H., and Rolfe, S. T., "Effect of Composition on the K_{Iscc} of Experimental HY-150 Steels", Technical Report No. 39.018-016(10), United States Steel Corporation, Applied Research Laboratory, Monroeville, PA, Contract NObs-94535 (FBM) (December 20, 1968).

73829 18Ni(250)(MAR) K_{fscc}

Novak, S. R., and Rolfe, S. T., "Comparison of Fracture-Mechanics and Normal-Stress Analyses in Stress-Corrosion Testing", Report No. 89.018-026(3), United States Steel Corporation, Applied Research Laboratory, Monroeville, PA, Contract NObs-94535 (FBM) (December 20, 1968).

73988 300M K_e

Pendelberry, S. L., Simenz, R. F., and Walker, E. K., "Fracture Toughness and Crack Propagation of 300M Steel", FAA Technical Report No. DS-68-18 (August 1968).

Sinclair, G. M., and Rolfe, S. T., "Analytical Procedure for Relating Subcritical Crack Growth to Inspection Requirements", University of Illinois, Urbana, Ill., and United States Steel Corporation, Applied Research Laboratory, Monroeville, PA, Paper presented at the Metals Engineering Conference of ASME, Washington, D.C., on March 31 to April 2, 1969.

74302 300M K_{Isc} HP9-4-.30 K_{Isc}

Carter, C. S., "Crack Extension in Several High-Strength Steels Loaded in 3.5% Sodium Chloride Solution", Research Report D6-19770, The Boeing Company, Renton, Wash., ARPA Contract N00014-66-C-0365 (November 1967).

Carter, C. S., "The Effect of Silicon on the Stress Corrosion Resistance of Low-Alloy, High-Strength Steels", Research Report D6-23872, The Boeing Company, Renton, Wash., ARPA Contract N00014-66-C-0365 (March 1965).

74719 18Ni(300) da/dt 18Ni(350) da/dt

Carter, C. S., "Stress Corrosion Crack Branching in High-Strength Steels", Research Report D6-23781, The Boeing Company, Renton, Wash., ARPA Contract N00014-66-C-0365 (March 1965).

75025 4340 K_{isec}

Procter, R. P., and Paxton, H. W., "The Effect of Prior Austenite Grain Size on the Stress Corrosion Cracking Susceptibility of A.I.S.I. 4340 Steel", Research Project, Carnegie-Mellon University, Pittsburgh, PA (January 1969).

75111 H11 da/dt

Wei, R. P., and Landes, J. D., "Correlation Between Sustained-Load and Fatigue Crack Growth on High-Strength Steels", Materials Research and Standards, <u>9</u> (7), 25-28 (July 1969).

75677 18Ni(350)(MAR) K_{Isc}

Carter, C. S., "The Effect of Heat Treatment on the Fracture Toughness and Subcritical Crack Growth Characteristics of a 350-Grade Maraging Steel", Report D6-22978, The Boeing Company, Renton, Wash., Contract N00014-66-C0365 (June 1969).

76411 18Ni(200)(MAR) K_{lc} HP9-4-.25(VAR) K_{rc}

Wessel, E. T., et al., "Engineering Methods for the Design and Selection of Materials Against Fracture", Final Technical Report, Westinghouse Research Laboratories, Pittsburgh, PA, Contract DA-30-069-AMC-602 (T) (June 24, 1966).

76972

4340 4340V K_{iscc} da/dt

Colangelo, V. J., and Ferguson, M. S., "The Role of the Strain Hardening Exponent in Stress Corrosion Cracking of a High Strength Steel", Corrosion, 25 (12) 509-514 (December 1969).

77716

18Ni(300)(MAR)

 K_{lscc}

Stavros, A. J., and Paxton, H. W., "Stress-Corrosion Cracking Behavior of an 18% Ni Maraging Steel", Homer Research Laboratories, Bethlehem Steel Corporation, Bethlehem, PA, and Carnegie-Mellon University, Pittsburgh, PA, ARPA Contract Nonr-760(31) (April 1970).

78065

18Ni(250)(MAR)

 K_{lscc}

Novak, S. R., and Rolfe, S. T., "Comparison of Fracture Mechanics and Nominal Stress Analysis in Stress Corrosion Cracking", Corrosion, 26(4) 121-130(April 1970).

78305

300M

 $\begin{array}{c} K_{ic}; \; K_{isce} \\ K_{ic} \end{array}$

300M (VM)

Webster, D., "Effect of Grain Refinement on the Microstructure and Mechanical Properties of 4340M", Summary Report D6-25220, The Boeing Company, Seattle, Wash., ARPA Contract N00014-66-C-0365 (April 1970).

78313

18Ni(250)

da/dt

300M

da/dt

Hyatt, M. V., "Use of Precracked Specimens in Stress-Corrosion Testing of High-Strength Aluminum Alloys", Summary Report D6-24466, The Boeing Company, Renton, Wash., ARPA Contract N00014-66-C-0365 (November 1969).

78425

18Ni(300)(MAR)

K_{Ic}; da/dN; K_{Iscc}

Carter, C. S., "Evaluation of a High-Purity 18Ni (300) Maraging Steel Forging", Report AFML-TR-70-139, The Boeing Company, Renton, Wash., Contract F33615-69-C-1620 (June 1970).

78761

18Ni(300)(MAR)

 K_{lsc}

4340

Carter, C. S., "Effect of Prestressing on the Stress-Corrosion Resistance of Two High-Strength Steels", Report D6-25275, The Boeing Company, Seattle, Wash., Contract N00014-66-C-0365 (May 1970).

80423

4340

 K_{lscc}

4340 (MOD)

Sandoz, G., "The Effects of Alloying Elements on the Susceptibility to Stress-Corrosion Cracking of Martensitic Steels in Salt Water", ASM Metallurgical Transactions, 2 (4) 1055-1063 (April 1971).

80667

18Ni(200)(MAR)

 $\begin{matrix} K_{\rm Isce} \\ K_{\rm Isce} \end{matrix}$

HP9-4-.20

Raymond, L., and Usell, R. J., Jr., "The Effect of N2O4 and UDMH on Subcritical Crack Growth in Various High-Toughness Low-Strength Steels", Report No. SAMSO-TR-71-106, TR-0059(6250-10)-8, The Aerospace Corporation, El Segundo, CA, Contract F04701-70-C-0059 (June 15, 1971).

80824

18Ni(200)(MAR)

 $\begin{matrix} K_{_{Iscc}} \\ K_{_{Iscc}} \end{matrix}$

18Ni(250)(MAR)

Syrett, B. C., "Stress Corrosion Cracking in 18% Ni (250) Maraging Steel", Corrosion, 27 (7), 270-280 (July 1971).

81004

18Ni(180)(MAR)

 K_{lscc}

18Ni(200)(MAR)

K

Kenyon, N., Kirk, W. W., and Van Rooyen, D., "Corrosion of 18Ni 180 and 18Ni 200 Maraging Steels in Chloride Environments", Corrosion, 27 (9), 390-400 (September 1971).

81814

4340

da/dt: K....

Gallagher, J. P., "Corrosion Fatigue Crack Growth Behavior Above and Below K_{Iscc} in Steels", Journal of Materials, 6 (4) 941-964 (December 1971).

82164

18Ni(280)(MAR)

K_{Isce}

Floreen, S., Hayden, H. W., and Kanyon, N., "Stress Corrosion Cracking Behavior of Maraging Steel Composites", Corrosion, 27 (12), 519-524 (December 1971).

82543

D6AC

K_t; a-vs-N; da/dN

Feddersen, C. E., et al., "Crack Behavior in D6AC Steel", Report MCIC-72-04, Metals and Ceramics Information Center, Battelle Columbus Laboratories, Columbus, OH (January 1971).

83611 4340 (EFM) da/dt

Dull, D. L., and Raymond, L., "Stress History Effect on Incubation Time for Stress Corrosion Crack Growth in E-4340 HR Steel", Air Force Report No. SAMSO-TR-72-168, Aerospace Report No. TR-0712 (2250-10)-7, The Aerospace Corporation, El Segundo, CA, Contract No. F04701-71-C-0172 (June 15, 1972).

 $18Ni(250)(MAR) K_{is}$

HP9-4-.20 K_{Is}

Sandoz, G., "The Resistance of Some High Strength Steels to Slow Crack Growth in Salt Water", NRL Memorandum Report 2454, Naval Research Laboratory, Washington, D.C. (February 1972).

83834 18Ni(200)(MAR) K_{tc} 18Ni(250)(MAR) K_{tc}

Fisher, D. M., and Repko, A. J., "Plane Strain Fracture Toughness Tests on 2.4 and 3.9-Inch-Thick Maraging Steel Specimens at Various Yield Strength Levels", Journal of Materials, 7 (2) 167-174 (June 1972).

Garland, K., "Fracture Toughness of Several High Strength Steels", Report 513-965, McDonnell Aircraft Company, McDonnell Douglas Corporation, St. Louis, MO, (June 7, 1971).

Maller, R., "The Effect of Heat Treatment Variations on the Fracture Toughness of D6AC Steel", Report No. M&P/MWE-1-TR-72-2, Grumman Aerospace Company, Bethpage, NY (March 13, 1972).

84278 300M (VM) K_{ic}

Maller, R., "The Effect of Heat Treatment Variations on the Fracture Toughness of 300M Steel", Report No. M&P/MWE-1-TR-72-5, Grumman Aerospace Company, Bethpage, NY (April 13, 1972).

84280 300M

K

4340 (DH)

 K_{tc}

Gunderson, A. W., and Harmsworth, C. L., "MAAE Engineering and Design Data, Material 300 M", Test Memo No. MAAE 70-5, Air Force Materials Laboratory, Wright-Patterson AFB, Ohio (September 24, 1970).

84290

4340

Kisco

Smith, H. R., Piper, D. E., and Downey, F. K., "A Study of Stress-Corrosion Cracking by Wedge Force Loading", Engineering Fracture Mechanics, <u>1</u>, p 123-128 (1968), Pergamon Press.

84306

HP9-4-.20

 K_{lc}

HP9-4-.30

K,

Harrigan, M. J., "B-1 Fracture Mechanics Data for Air Force Handbook Usage", Report TFD-72-501, North American Rockwell, Los Angeles Division, Los Angeles, CA (April 21, 1972).

84309

4340

da/dt

H11

da/dt

Landes, J. D., "Kinetics of Sub-Critical Crack Growth and Deformation in a High Strength Steel", A Dissertation Presented to the Graduate Facility of Lehigh University in Candidacy for the Degree of Doctor of Philosophy in Applied Mechanics, Lehigh University, Bethlehem, PA, (1970).

84310

18Ni(250)

da/dt

18Ni(300)

da/dt

4340

da/dt

Wei, R. P., "The Effect of Temperature and Environment on Subcritical Crack Growth", Report IFSM-72-14, Lehigh University, Bethlehem, PA (April 1972).

84313

4340

da/dt

Wei, R. P., Novak, S. R., and Williams, D. P., "Some Important Considerations in the Development of Stress Corrosion Cracking Test Methods", Presented at the 33rd AGARD (NATO) Structures and Materials Panel Meeting, Brussels, Belgium, October 4-8, 1971.

84317

12Ni-5Cr-3Mo

 K_{lscc}

Novak, S. R., and Rolfe, S. T., "Modified WOL Specimen for K_{lscc} Environment Testing", Journal of Materials, $\underline{4}$ (3), 701-728 (September 1969).

84342

12Ni-5Cr-3Mo

 K_{lscc}

18Ni(200)(MAR)

Crooker, T. W., and Lange, E. A., "The Influence of Salt Water on Fatigue-Crack Growth in High-Strength Structural Steels", ASTM STP 462, "Effects of Environment and Complex Load History on Fatigue Life", p 258-271 (1970).

84351

18Ni(250)(MAR)

 K_{lscc}

18Ni(350)(MAR)

 K_{Iscc}

300M

4330V H11

HP9-4-.45

Carter, C. S., "Stress Corrosion Crack Branching in High Strength Steels", Engineering Fracture Mechanics, 3, p 1-13 (July 1971).

84356

18Ni(300)(MAR)

4340

 $\begin{matrix} K_{Iscc} \\ K_{Iscc} \end{matrix}$

Carter, C. S., "Effect of Prestressing on the Stress Corrosion Resistance of Two High-Strength Steels", Metallurgical Trans., 3, p 584-587 (February 1972).

84963

4140

K_{Iscc}

Bucci, R. J., Paris, P. C., Loushin, L. L., and Johnson, H. H., "Fracture Mechanics Consideration of Hydrogen Sulfide Cracking in High Strength Steels", Stress Analysis and Growth of Cracks, Proceedings of the 1971 National Symposium on Fracture Mechanics, Part I, ASTM STP 513, p 292-307, American Society for Testing and Materials, Philadelphia, PA (1972).

85545

300M

da/dt

Speidel, M. O., "Dynamic and Static Embrittlement of a High-Strength Steel in Water", preprint from L'Hydrogene Dans Les Metaux, 1, Editions Science et Industrie, Paris, France (no date).

85633

HP9-4-.20

 K_{ic}

"Fracture Toughness and Tensile Properties Data for HP9-4-20 Steel", Shultz Steel Company, South Gate, CA, attached to memo from Ed Cawthorne dated March 9, 1973.

85836

300M

 $\begin{matrix} K_{le} \\ K_{le} \end{matrix}$

HP9-4-.20

"B-1 Fracture Toughness Data (K_{Ic}) - Rockwell International", Rockwell International Corporation, Los Angeles, CA (April 24, 1973).

a-vs-N; da/dN 85837 HP9-4-.20 a-vs-N; da/dN HP9-4-.30

"Fracture Toughness Data Collection, Rockwell International Corporation, from B-1

Program", Rockwell International Corporation, Los Angeles, CA (April 1973).

 K_{lc} 85857 HP9-4-.20

"Shultz Steel Company - Fracture Toughness Data - May 10, 1973", per memo from

Ed Cawthorne of May 10, 1973.

K_{Ic} HP9-4-.20 85879

"Fracture Toughness Data - Shultz Steel Company - May 15, 1973", per memo from

Ed Cawthorne of May 15, 1973.

 K_{Ic} 85883 300M D6AC

> Weiss, V., Sengupta, M., and Sanford, W., "The Significance of Material Ductility to the Reliability and Load Carrying Capacity of Peak Performance Structures", Final Report, Syracuse University, Syracuse, NY, Contract N00019-72-C-214 (January 1973).

86428 HP9-4-.20 K_{Ic}

> "Fracture Toughness Data for HP9-4-20 Forgings - Shultz Steel Company, July 5, 1973", test reports attached to memo from E. W. Cawthorne to J. E. Campbell (July

5, 1973).

86582 18Ni(300)(MAR) 4340

> McCabe, D. E., "Evaluation of the Compact Tension Specimen for Determining Plane Strain Fracture Toughness of High-Strength Materials", Journal of Materials, 7 (4)

449-454 (December 1972).

87241 300M

> 4140 4330V (MOD) 4340

Wood, W. E., Parker, E. R., and Zackay, V. F., "An Investigation of Metallurgical Factors Which Affect Fracture Toughness of Ultra-High Strength Steels", Report AMMRC CTR-73-24, LBL-1474, University of California, Lawrence Berkeley Laboratory, Berkeley, CA, Contracts DAAG46-72-C-8200 and W-7405-eng-48 (May 1973).

88136

300M

HP9-4-.20

K_{Ie}; a-vs-N; da/dN

HP9-4-.30

K, a-vs-N; da/dN

Dill, H. D., "Evaluation of Steel Alloys 300 M, HP-9Ni-4Co-.20, HP-9Ni-4Co-.30, and PH 13-8Mo", Report MDC-A2639, McDonnell Aircraft Company, McDonnell Douglas Corporation, St. Louis, MO, (December 21, 1973), with data supplement received May 2, 1974.

88140

HP9-4-.30

da/dN

Hall, L. R., Finger, R. W., and Spurr, W. F., "Corrosion Fatigue Crack Growth in Aircraft Structural Materials", Report AFML-TR-73-204, Boeing Aerospace Company, Seattle, WA. Contract AF33615-71-C-1687 (September 1973).

88575

10NI STEEL

a-vs-N; da/dN

"Advanced Metallic Air Vehicle Structure Program", Material Property Data Test Report Phase II, Report FZM-6148A, General Dynamics, Convair Aerospace Division, Fort Worth, TX, Contract AF33615-73-C-3001 (January 1974).

88579

HP9-4-.20

a-vs-N; da/dN

HP9-4-.30

a-vs-N; da/dN

"B-1 Program da/dN Data for Aluminum Alloys", Rockwell International Corporation, memorandum to H. D. Moran from E. W. Cawthorne, Battelle's Columbus Laboratories (April 3, 1974).

89311

4340

da/dN

Kortovich, C. S., "Corrosion Fatigue Behavior of 4340 and D6AC Steels Below K_{Isoc}", Report ER-7717, TRW Incorporated, Cleveland, OH, Contract N00014-69-C-0286 (April 1974).

90011

HP9-4-.20

 $\begin{matrix} K_{ic} \\ K_{ic} \end{matrix}$

HP9-4-.30

"Rockwell International, B-1 Program Fracture Toughness Data of August 5, 1974", with memorandum from E. W. Cawthorne to H. D. Moran of Battelle's Columbus Laboratories (August 5, 1974).

90012

HP9-4-.20

 K_{tc}

"Ti-6Al-4V Fracture Toughness Data - Shultz Steel Company, South Gate, CA, of August 8, 1974", with memorandum from E. W. Cawthorne to H. D. Moran of Battelle's Columbus Laboratories (August 8, 1974).

90981

18Ni(250)(MAR)

 K_{l_c}

Krupp, W. E., Wimmer, F. T., Pettit, D. E., and Hoeppner, D. W., Data Sheets for Final Report on "Investigation of the Effects of Stress and Chemical Environments on the Prediction of Fracture in Aircraft Structural Materials", Rye Canyon Research Laboratory, Lockheed-California Company, Burbank, Ca, Contract F33615-71-C-1688, data sheets received October 21, 1974.

91284

HY-TUF

K,

Hauser, J. J., "Data on Vacuum-Arc-Remelted (VAR) HY_Tuf", letter to J. E. Campbell, Battelle's Columbus Laboratories, Columbus, OH, from J. J. Hauser, Crucible, Incorporated, Materials Research Center, Pittsburgh, PA (December 3, 1974).

91838

18Ni(300)(MAR)

da/dN

Van Swam, L. F., et al., "Fatigue Behavior of Maraging Steel 300", Metallurgical Transactions A, 6A, 45-54 (January 1975).

AM002

HP9-4-.30

 K_{ic}

Fracture Toughness Data for HP9-4-.30 Steel sent from T. Matsuda, Airesearch Manufacturing Co., Torrence, CA, Data produced July 1977.

BW001

4340

da/dN

Horsley, J. J., and Harris, C. E., "Durability and Damage Tolerance Assessment (DADTA) of B-52 G/H Structure, Task II, Damage Tolerance Assessment Final Report", Boeing Company, Wichita, KS, Contract No. F34601-79-C-1515, Document No. D3-11560-3, June 1980.

BW002

4340

da/dN

Lambert, G., Mecham, P., and Mah, T., "Durability and Damage Tolerance Assessment (DADTA) of B-52 G/H Structure, Task III, Individual Airplane Crack Growth Tracking Program", Boeing Company, Wichita, KS, Contract No. F34601-79-C-2258, Document No. D3-11560-6, November 1981.

DA001

12-9-2 (MAR)

K_{ic}; da/dN

12-9-2 MAR

a-vs-N

4340

K_{1c}; a-vs-N; da/dN

H11

a-vs-N; da/dN

HY-180

a-vs-N; da/dN

Fatigue Crack Growth Rate Data Sheets on Aluminum Alloys 2024, 7010, 7050, 7075 and 7475, Stainless Steel Alloys 17-4PH and 17-7PH, and Alloy Steels 4340, A286, H-11, HY-180 and 12-9-2, Sent from Mr. Paul Abelkis, Douglas Aircraft Company, McDonnell Douglas Corporation, Long Beach, CA, March 1982.

HD006

A286

a-vs-N; da/dN

James, L. A., "The Effect of Temperatures on the Fatigue-Crack Propagation Behavior of A286 Steel", Report HEDL-TME 75-82, Westinghouse Hanford Company, Richland, WA, January 1976.

MA004

AF1410

a-vs-N; da/dN

Fatigue Crack Growth Rate Data on AF1410 Steel in Bar Form, McDonnell Aircraft Company, St. Louis, MO, Data Submitted by D. L. Rich, Attachment #4, received March 12, 1982.

MA005

300M

K_{ic}; da/dN; K_{isce}

HP9-4-.20

K_{Ic}; da/dN; K_{Iscc} K_{Ic}; da/dN; K_{Iscc}

HP9-4-.30

Garland, K., and Krieg, J. F., "Final Report - Basic Fracture Data for F-18 Material", McDonnell Aircraft Company, St. Louis, MO, Report No. 3 NA-66-7KW, Attachment #5, March 1977.

MA006

300M

da/dN

Garland, K., and Krieg, J. F., "Evaluation of the Effect of Material Cyclic Softening and Hardening on Crack Initiation Life and Crack Growth, with and without Overload as a Function of Stress Ratio", McDonnell Aircraft Company, St. Louis, MO, April 1978.

MA007

300M

da/dN

HP9-4-.30

da/dN

Garland, K., and Krieg, J. F., "Environment-Load Interaction Effects on Crack Growth", McDonnell Aircracft Company, St. Louis, MO, Report No. 703-116, June 1978.

MA010

300M

da/dN

HP9-4-.30

da/dN

Garland, K., and Krieg, J. F., "Environment-Load Interaction Effects on Crack Growth in Landing Gear Steels", McDonnell Aircraft Company, St. Louis, MO, Report No. TR 703-535, TM 256-6627, February 1981.

MA011

4330V (MOD)

 K_{ic} ; da/dN

"Final Report, F/RF-4C/D Damage Tolerance and Life Assessment Study - Vol. II", McDonnell Aircraft Company, St. Louis, MO, Contract No. AFSC F33657-73-A-0062, Report No. MDC A2883, February 1975.

MA012

4340

da/dN

Model F-4E Slatted Airplane Fatigue and Damage Tolerance Assessment, Vol. II", McDonnell Aircraft Company, St. Louis, MO, Contract No. F33657-73-A-0004-0015. Report No. MDC A3390, July 1975.

MA018

AF1410

 K_{t_c}

Data submitted by Mr. Eric Tuegel, McDonnel Aircraft Co., 253.09.0227.01, October 1990.

MD001

D6AC

K_{Ic}

Davis, R. J., and Rowe, R. A., "Mechanical Properties of SRB Rolled-Ring Forgings and Large Hand Forgings", McDonnell Douglas Astronautics Company, Huntington Beach, CA, Report MDC G8545, June 1980.

MR002

4140

4340

 $\begin{matrix} K_{Ic} \\ K_{Ic} \end{matrix}$

"Damage Tolerant Test Data on 4140 and 4340 Steel", Materials Research Laboratory, Inc., Glenwood, IL, Under Contract to ARRAD COM (DAAKIO-79-C-0358), November 1980.

NC001

HP9-4-.20

 K_{ic}

Plane Strain Fracture Toughness Data Sets on Aluminum, Steel, and Titanium Alloys, Data sent from P. G. Porter of Northrop Corporation, March 1, 1982.

NC002

HP9-4-.20(CEVM)

a-vs-N; da/dN

Fatigue Crack Growth Rate Data on Aluminum, Steel, and Titanium Alloys, Data sent from P. G. Porter of Northrop Corporation, March 1, 1982.

RI001

AF1410

AF1410(VIM-VAR)

K_{Ie} a-vs-N; da/dN

Routh, W. E., "Lower Cost by Substituting Steel for Titanium", Rockwell International Corporation, Los Angeles, CA, Contract No. F33615-75-C-3109, Report No. AFFDL-TR-77-73, June 1977.

RI006

300M

da/dN; K_{terr}

HP9-4-.20

Ferguson, R. R., and Berryman, R. C., "Fracture Mechanics Evaluation of B-1 Materials", Rockwell International, B-1 Division, Los Angeles, CA, Contract No. F33657-70-C-0800, Report No. AFML-TR-76-137, October 1976.

TABLE 3.41 (CONCLUDED)

RI011

AF1410

a-vs-N; da/dN

Demonet, R. J., Newland, J. C., and Diaz, J. H., "Cyclic Crack Growth Rate Testing of AF 1410 Steel - Phase II", Rockwell International, LTR 2296-4166, August 1977.

SW001

4340

a-vs-N; da/dN

Data submitted by Mr. Jack Fitzgerald, Southwest Research Institute, San Antonio, TX.

UD007

HY-80

da/dN

Ruschau, J. J., "Navy Round Robin Corrosion Fatigue Crack Growth Rate Test Results for HY-80", University of Dayton Research Institute, Dayton, OH, Contract No. F33615-80-C-5011, Technical Memorandum UDR-TM-81-37, November 1981.

WL005

4340

a-vs-N; da/dN

Data submitted by Mr. Jim Harter from ASTM round robin, Wright-Patterson Materials Lab, April 1992.

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TABLE 4.0.1

Alloy	Condition/ Heat Treatment	Product Form	K _{Ie}	Ke	R Curve	da/dN	da/dt	$K_{ m Iscc}$
		Rolled Bar	10					
	H900	Bar						3
		Forging	12			22		
	H1025	Rolled Bar	2					
15.6PH		Bar				4		
	001111	Rolled Bar	3					
	H1150M	Bar						8
	TUS=150-165KSI	Billet				8		
	TYS=150-165KSI	Forging	3					,
	Н900	Forging						1
15-5PH(AM)	H1000	Forging						1
	H900	Forging						1
16-5PH(VM)	H1000	Forging						1
		Plate				2		
	H800	Bar						1
	Н976	Rolled Bar	1		•			
17-4PH	H1000	Bar						1
		Casting				2		
	H1025	Round Bar	1			7		
	RH950	Bar						1
17:7PH	Vary value	Rolled Bar	ဗ					
	KH 1050	Bar						8

Alloy	Condition/ Heat Treatment	Product Form	K _{Ic}	Ke	R Curve	da/dN	da/dt	Klace
17-7РН		Plate				3		
(Cont'd)	TH1050	Bar						1
21-6-9 NI40	ANNEALED	Sheet				9		
	1	Sheet				12		
304	ANNEALED	Plate				12		
	ANNEALED & AGED	Plate				1		
	ANNEALED	Plate				9		
316	ANNEALED AT 1950F 1HR WQ	Plate				1		
	0.050 IN. FROM CENTERLINE	Weldment				1		
347	AT CENTERLINE	Weldment				1		
	AT HEAT AFFECTED ZONE	Weldment				1		
	2200F 1HR 1900F 1HR OQ -100F 1HR -320F 1HR 800F 2+2HR	Plate						1
,	2200F 1HR 1900F 1HR OQ -100F 1HR -320F 1HR 900F 2+2HR	Plate						1
Arc 260	2200F 1HR 1900F 1HR OQ -100F 1HR -320F 1HR 1900F 2+2HR	Plate						1
	2200F 1HR 1900F 1HR OQ -100F 1HR -320P 1HR 1050P 2+2HR	Plate						1
	1800F 1HR OQ -100F 0.5HR 500F 2+2HR (COARSE GRAIN)	Plate						1
AFC 77	1800F 1HR OQ -100F 0.5HR 500F 2+2HR (FINE GRAIN)	Plate						1
	1800F 1HR OQ -100F 0.5HR 700F 2+2HR (COARSE GRAIN)	Plate						

Alloy	Condition/ Heat Treatment	Product Form	K _{Ie}	К	R Curve	da/dN	da/dt	K _{Isce}
	1800F 1HR OG -100F 0.5HR 700F 2+2HR (FINE GRAIN)	Plate	1					
	1800F 1HR OQ -100F 0.5HR 800F 2+2HR (COARSE GRAIN)	Plate	1					
	1800F 1HR OQ -100F 0.5HR 800F 2+2HR (FINE GRAIN)	Plate	1					
	1800F 1HR OQ-100F 0.5HR 1000F 2+2HR (COARSE GRAIN)	Plate	1					1
	1800F 1HR OQ-100F 0.5IIR 1000F 2+2HR (FINE GRAIN)	Plate	1					1
	1800F 1HR OQ -100F 1HR 700F 2+2HR	Round Bar	1					
	1800F 1HR OQ -100F 1HR 800F 2+2HR	Round Bar	1					
ļ	1900F 1HR OQ -100F 1HR 800F 2+2HR	Round Bar	1					
Arc 77 (Cont'd)	2000f 1HR OQ -100F 0.5HR 500F 2+2HR	Bar						1
	2000F 1HR OQ -100F 0.5HR 500F 2+2HR + 10 PCT CW	Bar						8
	2000F 1HR OQ -100F 0.5HR 500F 2+2HR + 20 PCT CW	Bar						1
	2000F 11IR OQ -100F 0.5HR 700F 2+2HR	Bar						1
	2000F 1HR OQ -100F 0.5HR 800F 2+2HR	Bar						1
	2000F 1HR OQ -100F 0.5HR 900F 2+2HR	Bar						. 1
	2000F 1HR OQ -100F 0.5HR 1100F 2+2HR	Bar						1
	2000F 1HR OQ -100F 0.5HR 1400F 2+2HR	Bar						1
	2000F 1HR OQ .100F 1HR 800F 2+2HR	Round Bar	1					
	2000F 1HR OQ -100F 1HR 900F 2+2HR	Round Bar	2					

Alloy	Condition/ Heat Treatment	Product Form	K _{Ic}	K	R Curve	da/dN	da/dt	$ m K_{Iscc}$
A PC 27	2100F 1HR FC TO 1900F HOLD 1HR OQ -100F 4HR 500F 2+2HR	Forging						2
(Cont'd)	AUSTENITIZED AT 2010F QUENCHED & TEMPERED AT 810F	Sheet					pol .	
	1700F 1HR OQ 2100F 1HR MOVE TO FCE AT 1933F HELD 1HR OQ -100F 24HR 900	Forging	18					
AFC 77 (VAR)	2100F 1HR MOVED TO FCE AT 1900F HELD 1HR OQ -100F 4HR 600F 2+2HR	Forging	7					
	MOD SCT1000	Bar						-
		Plate						8
AM 355	SCT 850	Bar						4
		Plate						က
	SCT1000	Bar						4
	006Н	Bar						1
AM 362	H1000	Bar						
	H850	Forging						-
AM 364	096Н	Forging						-
	1500F 1HR OQ 900F 4HR AC	Forging	ဇ					
	1500F 1HR OQ 950F 4HR AC	Forging	8					
CUSTOM 465	006H	Forging						-
	096H	Forging						-
	H1000	Forging				11		
	Unspecified	Extruded Bar				4		
PH13-8Mo	ANNEALED	Forging	111					

Alloy	Condition/ Heat Treatment	Product Form	K _{Ic}	К¢	R Curve	da/dN	da/dt	Klscc
	AUSTENITE COND AND TRANSFORMED AT 38F AGED 1016F	Forged Bar	4					
		Sheet	9					
		Forging	9					1
	Н960	Forged Bar						10
		Rolled Bar	12					
		Ваг						8
		Sheet	10					
		Plate	4					
		Forging	24			8		
- 710 611111		Extrusion	20					8
(Cont'd)	H1000	Forged Bar	9			22		ы
		Billet				8		
		Extruded Bar				4		
		Rolled Bar	4			14		11
		Bar				1		
	H1025	Sheet	1					
		Forging	11			22		
	H1050	Rolled Bar	11					
		Bar						8
	MILL 1700F LAB 1050F 4HR	Forging	1					
	MILL 1700F LAB 1500F 1000F 4HR	Forging	1					

TABLE 4.0.1 (CONCLUDED)

Alloy	Condition/ Heat Treatment	Product Form	K _{Ie}	К°	R Curve	da/dN	da/dt	Klecc
	MILL 1700F LAB 1600F 1000F 4HR	Forging	#					
		Round Bar						7
	КПРВО	Rolled Bar	4					
	and Care	Round Bar						8
	KH9/0	Rolled Bar	3					
PH13-8Mo		Round Bar						8
(Cont'd)	KH 1000	Rolled Bar	1					
	TYS=140KSI	Plate						1
	TYS-180KSI	Plate						1
	TYS-190KSI	Plate						1
	TYS-200KSI	Plate						1
	TYS-210KSI	Plate						1
PH14-8Mo	SRH1050	Sheet		7				
		Rolled Bar	2					
1	KHBBO	Ваг						1
PHID-7M0	RH1060	Rolled Bar	8					
	TH1050	Ваг						1

TABLE 4.0.2

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF STAINLESS STEEL ALLOYS
AT ROOM TEMPERATURE

											-			,		_
			Std Dev	;	i	1	i	ı	ı	ı	i	i	ı	1	i	2.1
		T-S	Mean	:	ı	;	!	ı	ı			-	ı	-		74.1
		02	ď	:	;	i	1		ı	-			i	-	i	8
			Min Spec Thk	i	i	i	1	i	1	1	i	ı	i	i	i	0.75
	ation		Std Dev	4.5	21.9	6.9	2.0	1.3	2.9	ı	ı	22.4	1.8	16.1	i	1.7
$K_{Ic}~(Ksi\sqrt{in})$	Specimen Orientation	T-L	Mean	72.7	119.4	94.8	47.0	60.8	108.0		-	99.6	89.6	69.4	-	63.5
Le (J	nen	T	ď	9	4	3	3	7	2	1	1	9	2	4	i	9
K	Specin		Min Spec Thk	1.00	19:1	1.50	1.00	0.50	2.01			1.00	1.63	•	:	1.00
			Std Dev	:	:		:	3.1	5.0	3.3	7.8	16.7	19.4	6.5	16.0	2.9
		L-T	Mean	:	:	:		48.6	110.5	46.2	72.1	114.1	103.0	58.4	70.3	6.99
		Γ	и	;	ï	;	:	7	2	3	2	2	2	2	8	3
			Min Spec Thk	:	:	ı	ŀ	0.50	2.01	0.48	0.48	1.01	1.63	1.00	1	1.00
Range of	Product	Thickness	(III.)	2.25	1.50-3.00	***	1.25	6.00	6.00	4.00	4.00	3.00	2.20	1.00-2.25	4.00-8.00	2.25
	Product	Form		Rolled Bar	Forging	Forging	Rolled Bar	Forging	Forging	Forging	Forging	Forging	Forged Bar	Sheet	Forging	Rolled Bar
	Condition/	Heat Treatment		006 H	H1025	TYS=150-165KSI	RH1050	1700F 1HR OQ 2100F 1HR MOVE TO FCE AT 1933F HELD 1HR OQ -100F 24IR 900	2100F 1HR MOVED TO FCE AT 1900F HELD 1HR OQ -100F 4HR 500F 2+2HR	1500F 1HR OQ 900F 4HR AC	1500F 1HR OQ 950F 4HR AC	ANNEALED	AUSTENITE COND AND TRANSFORMED AT 38F AGED 1016F		H 950	
	Allow	Source Source			16-5PH		17.7PH		AFC 77 (VAR)		CUSTOM 455			PH13-8Mo		

TABLE 4.0.2 (CONCLUDED)

PLANE STRAIN FRACTURE TOUGHNESS VALUES OF STAINLESS STEEL ALLOYS AT ROOM TEMPERATURE

TABLE 4.0.4.1

AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK FOR STAINLESS STEEL ALLOYS IN LAB AIR AT ROOM TEMPERATURE FATIGUE CRACK GROWTH RATE (FCGR) COMPARISON

ORIENT	ORIENTATION: Unspecified	STRESS RATIO: 0.05 - 0.1	ATIO: 0.05	- 0.1		FREG	FREQUENCY: 1.67 - 30. Hz	1.67	30. Hz	
THE STATE OF THE S	A STATE STATE OF THE STATE OF T			Š		FC	FCGR (10 4 in/cycle)	⁸ tn/cycl	G	
TOTAL OF THE PROPERTY OF THE P	HEAT TREATMENT	FORM	Ħ	FIREQ (HR)		ΔR	AK Level (Kaklin)	ľ (Katý)	(11)	
					2.5	6,0	10.0	20.0	0.08	100.0
			0.05	10			0.2	3.06		
			0.05	15			0.13	2.83		
	ANDRALED		0.05	10-15			0.14	3.09		
304	Gallaghan	Sheet	0.1	1.67				2.82		
			0.1	9				2.78		
			0.1	1.67-6				2.59		
	ANNEALED & AGED	PLATE	0.05	8				1.39		
316	ANNEALED	PLATE	0.05	10				2.49		
	.060 IN. FROM CENTERLINE	WELDMENT	0.1	30					10.26	
347	AT CENTERLINE	WELDMENT	0.1	30					13.37	
	AT HEAT AFFECTED ZONE	WELDMENT	0.1	30					16.47	

TABLE 4.0.4.2

FATIGUE CRACK GROWTH RATE (FCGR) COMPARISON AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK FOR STAINLESS STEEL ALLOYS IN LAB AIR AT ROOM TEMPERATURE

ORIE	ORIENTATION: L-T	STRESS RATIO: -1 0.8	ATIO: -1.	9.0		FREQU	FREQUENCY: 0.03 - 30. Hz	0.03 - 8	30. Hz	
						MO	PCCIR (10° tr/cycle)	tr/cycle	(6	
ALLOY	CONDITION/ HEAT TREATMENT	PRODUCT	R	FREQ (Hz)		ΔK	ΔK Level (Ksiγlin)	(Ksi/i	(n)	
				1	2.5	6.0	10.0	20.0	50.0	100.0
			1-	5			0.3	2.76	21.46	
			0.1	10-20				2.62	23.26	
15-5PH	H1025	FORGING	0.4	10-15		0.05	0.42	2.85	24.48	
			0.8	20-30			0.54	4.03		
		BAR	0.5	10					23.64	102.42
17-4PH	Н 900	PLATE	0.08	20			0.31	3.41	53.01	
17-7PH	TH1050	PLATE	0.1	20		0.03	0.45			
		1	0.	0.03					66:99	
304	ANNEALED	PLATE	Ö.	6.67				1.95	27.99	
ALC SECURITION	6 6 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		0.1	10-30				2.76		
CUSIUM 466	HIOOO	FORGING	0.3	20-30				3.72		
	666.	FORGING	0.1	6.10				5.7	30.78	127.33
	DOOLU	BAR	0.02	10					31.58	
			-1	2			0.31	3.31	26.63	
			0.1	ŭ			0.36	3.64	28.08	
PH13-8Mo			0.1	20				3.5	24.45	183.59
	H1050	FORGING	0.4	5		90.0	0.56	4.82		
			0.4	6-20		0.06	0.53	4.55	32.68	
			0.4	20		0.05	0.53	4.28	31.06	
			8.0	15-30		0.1	0.89	5.33		

TABLE 4.0.4.3

AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK FOR STAINLESS STEEL ALLOYS IN LAB AIR AT ROOM TEMPERATURE FATIGUE CRACK GROWTH RATE (FCGR) COMPARISON

FREQUENCY: 5. - 30. Hz STRESS RATIO: 0. - 0.8 ORIENTATION: T.L

	32.46	1.86				/0.0		A LUCALIA		
								STOP ACT	CA IVENIA	708
	71.4	3.95	0.4			!	0.2			
	78.59	3.56	0.56				0.1	SHEET	ANNEALED	21-6-9 NI40
	67.29	2.35	0.34				0.01			
		4.59	0.38	0.02		20	0.1	PLATE	TH1050	17-7PH
			0.51	0.04		30	0.5			
			0.51	0.03		30	0.5			
		5.88				10	0.5	WOOND BAR		 - -
		5.88				10	0.5	n v a charlo	H1095	17-4PH
		2.04	90:0			30	0.1			
		2.01	90:0			30	0.1			
151.46	14.43					10	0.05	BAR		
			7.0			20-30	0.8			;
		3.53	0.46	90:0		15-20	0.4	FORGING	H 1008	15-5PH
	26.12	2.88				15	0.1			
100.0	0.00	20.0	10.0	8.0	2.5					
	ii)	(Ksiv.	ΔΚ Level (Ksiγin)	ΔÆ		(Hz)	R	FORM	HEAT TREATMENT	
	(e)	^d in/cycl	PCGR (10 4 In/cycle)	FK		Charles		monatore	/NORBIGINAL	ATLOV
		000000000000000000000000000000000000000								

TABLE 4.0.4.3 (CONCLUDED)

FOR STAINLESS STEEL ALLOYS IN LAB AIR AT ROOM TEMPERATURE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK FATIGUE CRACK GROWTH RATE (FCGR) COMPARISON

STRESS RATIO: 0. - 0.8

ORIENTATION: T.L

FREQUENCY: 5. - 30. Hz

ATTAN	1.4.COMMANA.4.4.COD	monate out		S I		5	GR (10	FCGR (10 ° in/cycle)	(6	
IST	HEAT TREATMENT	FORM	Ħ	(Hg)		ΔK	Level	ΔΚ Level (Κείγίπ)	<i>1</i>)	
					2.5	8.0	10.0	20.0	50.0	100.0
			0.1	10					22	
CUSTOM 455	H1000	FORGING	0.1	20				3.11		
			0.1	20-30				2.52		
	H1000	FORGING	0.1	5-10				5.74	31.6	139.72
			0.1	20		0.03	0.27	2.99	23.2	
Dute own			0.1	7-20		0.04	0.31	3.07	25.59	
0,00-0111	H1050	FORGING	0.4	20		0.05	0.53	4.3	27.43	
			0.4	5-20		0.08	0.54	4.43	29.07	
			0.8	15-30		0.1	0.91	5.42		

TABLE 4.0.5 (CONCLUDED)

	INDIVIDUAL STRESS CORROSION CRACKING THRESHOLD DATA FOR STAINLESS STEEL ALLOYS AT ROOM TEMPERATURE	RROSIO	N CRACK OYS AT RO	S CORROSION CRACKING THRESHOLD DA STEEL ALLOYS AT ROOM TEMPERATURE	SHOLD	DATA E	or	
		PRODUCT	SPECIMEN		K	$K_{Isoc}~(Ksi\sqrt{in})$	/ <u>in</u>)	
ALLOY	CONDITIONAL	FORM	ORIENTATION			ENVIRONMENTS	TTS	
				BUMP TANK WATER	8.6% NACL	20% NACL	SEACOAST ATMOSPHERE	INDUSTRIAL
1 1 1 0 moi 10	Н900	Forging	ï		09			
CUSTOM 455	Н960	Forging	1		72			
	нео	Forging	T-L		74			
		Forged Bar	LT	48				
		Bar	T·L			46	31	69
	H1000	Extrusion	LT	55				
PH13-8Mo		Forged Bar	LT	88				
		Forged Bar	T-L	100				
		Rolled Bar	LT	70				
	H1050	Bar	T-L			99	44	693
	TYS = 210 KSI	Plate	T:L		120			
	RH 950	Bar	1		71			
PH16-7Mo	RH 1060	Bar	i		18			
16.5 PH	006Н	Bar	1			83	36	89
16-5 PH(VM)	006Н	Forging			99			
17-4 PH	006Н	Bar			62			
	0301HB	Bar	T-L			99	12	24
17-7 PH	TH1050	Bar			16			

TABLE 4.1.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR STAINLESS STEEL ALLOY 15-5PH AT ROOM TEMPERATURE

Product					K_{Ic}	$K_{Ic}~(ksi\!\sqrt{in})$	<u>a</u>)			
Form	Condition/Heat Treatment			53	Specimen Orientation	n Orie	ntation			
			L-T			T-T			S-L	
		Mean K _{lo}	Std Dev	ď	Mean K _{Ie}	Std Dev	ч	Mean K _{to}	Std Dev	E
F	H1025				119.4	21.9	4	:	i	i
rorging	TYS=150-165KSI	:	•••	:	94.8	6'9	3		!	i
Rolled Bar	H900	1	•••		72.7	4.5	9	:	ŀ	:

1 of 1

TABLE 4.1.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 15-5PH AT ROOM TEMPERATURE

	0.001	
	(t)	
=	cyale (Nin)	
ENVIRONMENT: 3.5% NaCl	FCGR (10 ^d in/cycle) AK Level (Ksiv/in)	9.97
2%	(10 evel	
ľ: 3.	GR C	
EZ	PCI AI	
ZZ		
IRO	8.8	
N		
H	FREQ (Hz)	-
	E	
	R	0.6
		ľ
	N W	
	PRODUCT	BAR
${f T}$	PR	
V: L-		
ORIENTATION: L-T	ı	
TAI	EN	
IEN	NO WILL	
OR	DIT REA	H1025
	CONDITION/ HEAT TREATMENT	
	C	
	H	

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK

				8 888888888		
				100.0		
	i.	le)	3)	20.0 50.0	94.12	
	d Wate	⁶ in/cyc	(Ksi/ü		8.74	10.18
	ENVIRONMENT: Distilled Water	PCGR (10 ⁻⁸ in/cycle)	AK Level (Ksiyin)	10.0	0.26	1.12
	ENT: I	P.C.	ΔJ	8.0		90:0
TURE	RONM			2.5		
MPERA	ENV	FREG	(HZ)		1	1
OOM TE			H		0.1	8.0
15-5PH AT ROOM TEMPERATURE	. L-T	PRODUCT	FORM		2000	FORGING
	ORIENTATION: L-'	NOILIGNOD	HEAT TREATMENT			HIOZO

TABLE 4.1.1.2.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 15-5PH AT ROOM TEMPERATURE

ORIENTATION: L-T	: L-T		H	NVIRO	NMEN	ENVIRONMENT: Lab Air	Air		
CONDITION/	PRODUCT		FREO		PC	PCGR (10 ⁶ in/cycle)	⁶ in/cyc	(9)	
HEAT TREATMENT	FORM	K	(HZ)		Δ.	AK Lovel (Kst/In)	(Ksi/ü	1)	
				8.9	5.0	10.0	20.0	50.0	100.0
		-1	מי			0.3	2.76	21.46	
	DNIDGOZ	0.1	10-20				2.62	23.26	
H1025	Children	0.4	10-15		0.05	0.42	2.85	24.48	
		0.8	20-30			0.54	4.03		
	BAR	0.5	10					23.64	102.42

TABLE 4.1.1.2.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 15-5PH AT ROOM TEMPERATURE

	yele) /in) 50.0 100.0	39.38
ENVIRONMENT: 3.5% NaCl	FCGR (10 ⁶ in/cycle) AK Lovel (Ksiv/in) 8.0 10.0 20.0	
ENVIRON	FREQ (Hz)	1
	R	0.05
: T-L	PRODUCT FORM	BAR
ORIENTATION: T-1	CONDITION/ HEAT TREATMENT	H1025

TABLE 4.1.1.2.5

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 16-5PH AT ROOM TEMPERATURE

ORIENTATION: T-L

ENVIRONMENT: Distilled Water

TABLE 4.1.1.2.6

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 15-5PH AT ROOM TEMPERATURE

ORIENTATION:	: T-L		ENVI	ENVIRONMENT: H.H.A.	H.H.A.		
CONDITION	PRODUCT		EQ	FCGR	FCGR (10 ^d in/cycle)	ycle)	
HEAT TREATMENT	FORM	H)	(Hz)	AK Le	ΔK Level (Ksivin)	(ii)	
			2.5	5.0 10.	10.0 20.0	50.0	100.0
		-1		0.26	8 4.04	44.99	1703.72
T113-150-16KSI	11.1 EM	-0.2		0.14	4 3.17	32.97	1088.2
		0.04		0.14	3.05	33.26	1126.65
		0.4		0.76	6 5.12	126.15	

TABLE 4.1.1.2.7

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 15-5PH AT ROOM TEMPERATURE

ORIENTATION: T-L

ENVIRONMENT: Lab Air

		100.0				151.46
(6)	9	50.0	26.12			14.43
in/cye	(Ksh/ir	20.0	2.88	3.53		
FCGR (10 ⁻⁶ in/cycle)	AK Lovel (Kok/in)	10.0		0.46	0.7	
PCC	ΔÆ	5.0		0.05		
		2.5				
	FREQ (Hz)	i	15	15-20	20-30	10
	æ		0.1	0.4	0.8	0.05
	FORM			FORGING		BAR
	CONDITION/ HEAT TREATMENT				HIOZD	

TABLE 4.1.1.2.8

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR △K

PCGR (10⁻⁸ in/cycle) ΔK Lovel (Ksivin) 90.08 4.78 4.78 3.46 3.46 ENVIRONMENT: H.H.A. 10.0 9.0 15-5PH AT ROOM TEMPERATURE 8.8 FREQ (Hz) -0.2 -0.2 0.04 ĸ 7 PRODUCT FORM BILLET ORIENTATION: S-L HEAT TREATMENT CONDITION TUS=150-165KSI

0.001

80.0

51.6 51.6 39.64 37.87 37.87

> 3.18 6.04 6.04

0.04

0.4 0.4

39.64

	K _{Ie}	K. STAN DATE REFER	1973 86688	1973 86688	1973 86688	72.7 4.5 1973 86688	1973 86688	1973 86688	1972 84212	1987 DA007	1987 DA007	66.6 6.5 1987 DA006	1987 DA006	1987 DA007	1987 DA007	65.5 1.8 1987 DA006	1987 DA006	1987 DA007	1987 DA007	119.4 21.9 1987 DA006	1987 DA006	1982 NH007	61.2 1.6 1992 NH007
		(fin.) (Kel • vin.)	0.54 79.40	0.49 75.80	0.38 66.50	0.46 79.10	0.43 70.90	0.42 70.50	0.55 86.90	0.48 73.80	0.43 70.20	0.31 60.30	0.32 62.00	0.30 58.10	0.27 65.00	0.25 54.40	0.25 64.30	1.95 139.60	1.87 138.60	0.91 87.00	1.05 104.20	0.35 62.30	0.33 60.10
$\mathbf{K}_{\mathbf{Io}}$	CRACK		2.068	1.061	1.040	1.049	2.067	2.064	1.000	1.016	1.010	1.512	1.533	1.028	1.021	1.560	1.551	2.036	2.036	1.567	1.543		ı
15-5PH	z	DRSIGN	CT	CT	cr	cr	cr	CT	NB	CT	CT	CT	CT	cr	CT	CT	cr	CT	CT	СI	CT	CT	СŢ
	SPECIMEN	THICK (In.)	2.000	1.000	1.000	1.000	2.000	2.000	1.000	1.000	1.000	1.501	1.500	1.001	1.000	1.494	1.492	1.998	1.999	1.613	1.514	1.500	1.500
STAINLESS STEEL		WIDTH (fa.) W	4.000	2.000	2.000	2.000	4.000	4.000	2.000	1.997	1.997	3.005	3.008	2.000	1.996	3.010	3.008	4.007	4.008	3.000	3.001	2.960	2.960
STAINL		YIELD STR (Kal)	171.0	171.0	171.0	171.0	171.0	171.0	185.0	169.0	169.0	172.3	172.3	167.9	167.9	171.3	171.9	158.0	158.0	160.6	160.6	166.0	166.0
V2		SPEC	_		Ě	7.			LR			<u></u>			i]: 			Ě	1.			ž
		TEST TEMP (°F)			,	.; *			R.T.		,	ş 				ş 			i i	<u>;</u>		,	-
	JCT	THICK (In.)	2.25	2.25	2.25	2.25	2.25	2.25	4.00	3.00	3:00	1.50	1.50	3:00	3.00	1.60	1.50	3.00	3.00	1.50	1.50	4.00	4.00
	PRODUCT	FORM			F F	Kolled Bar			Rolled Bar		ſ	rorging				Forgue		-	F	rorging		:	Kolled Bar
		CONDITION			XV	008 H			Н 900		10071	n 1020			Ì	0701H			i co	970111			H1026

TABLE 4.1.1.3 (CONCLUDED)

				U 2	STAINLESS STEEL	SS STE		15-5PH	$\mathbf{K}_{\mathbf{I}\sigma}$						
	PRODUCT	UCT					SPECIMEN	7.				K _{le}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kal)	WIDTH (fn.)	THICK (In.)	DESIGN	LENGTH (fn.) A	(K _w ,TYS)* (in.)	K. (Kal •	K. MEAN	STAN	DATE	REFER
		4.00			147.3	1.960	1.500	LO	1	0.72	79.00			1992	NH007
H1100	Rolled Bar	4.00	٥	S.S.	147.3	2.960	1.500	CT	1	0.90	88.50	202	7.1	1982	NH007
		4.00			166.0	2.960	1.500	cr	!	0.50	74.60			1992	NH007
		4.00			171.6	2.960	1.500	CT	1	0.24	63.30			1992	NH007
H900	Rolled Bar	4.00	•	a C	171.6	2.960	1.500	CT	į	0.19	47.20	808	3.2	1992	NH007
		4.00			171.5	2.960	1.500	CT	ì	0.23	61.80			7661	NH007
		i			155.0	3.000	1.500	CT	:	1.09	102.50			1978	BW007
TYS-160-165KSI	Forging	ı	R.T.	J:L	155.0	3.000	1.500	CI	i	68'0	92.70	94.8	6.9	1978	BW007
		ı			155.0	3.000	1.500	CT	:	0.83	89.20			1978	BW007

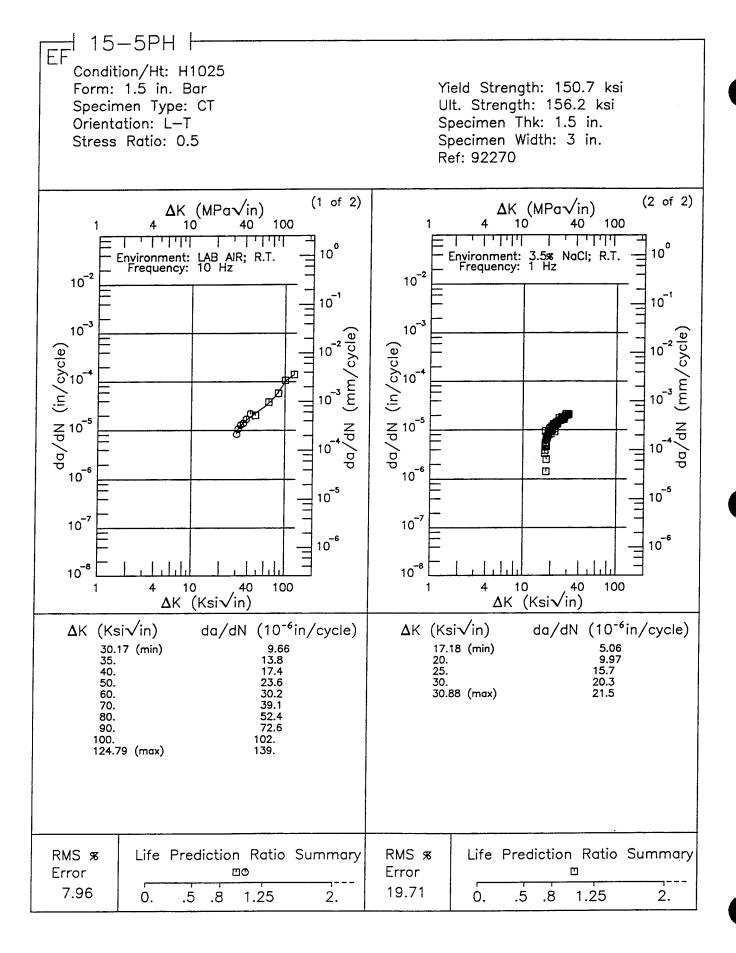


Figure 4.1.3.1.1

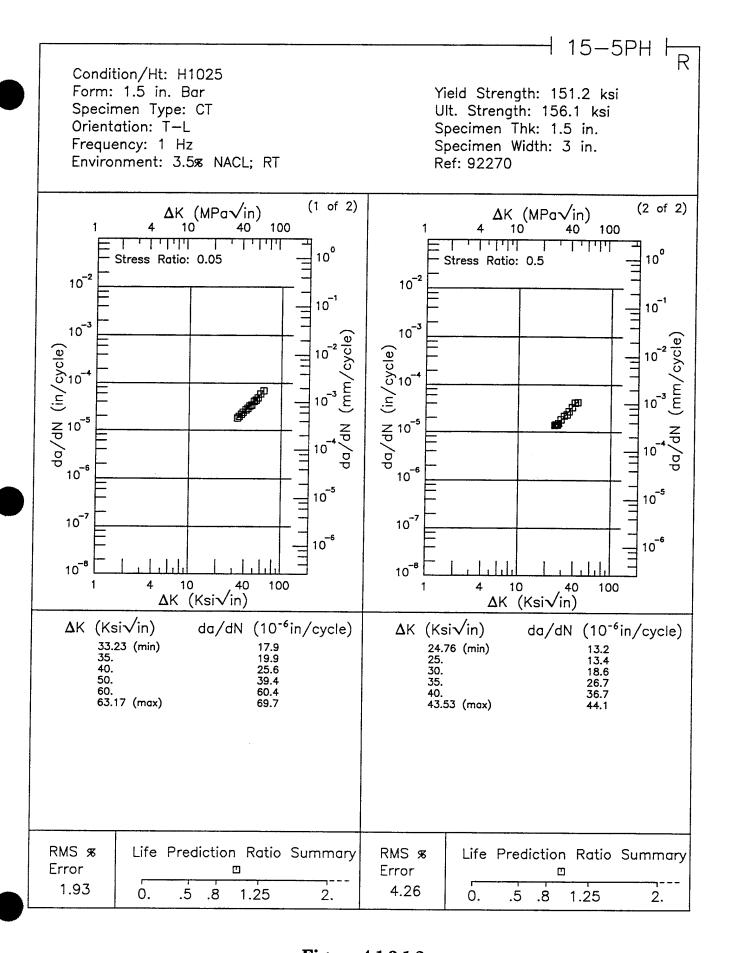


Figure 4.1.3.1.2

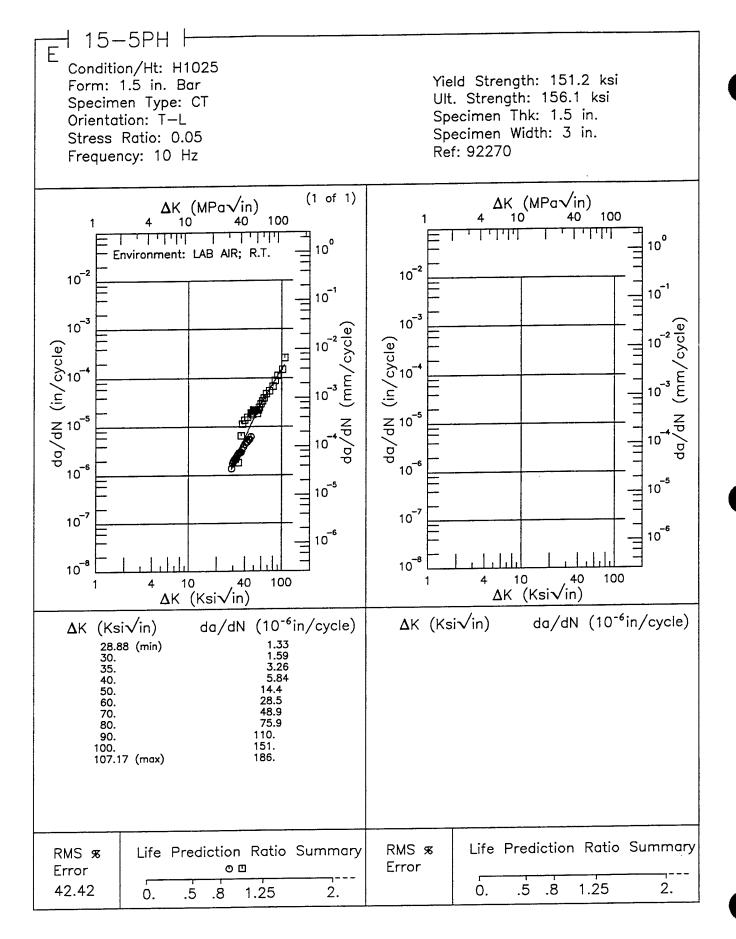


Figure 4.1.3.1.3

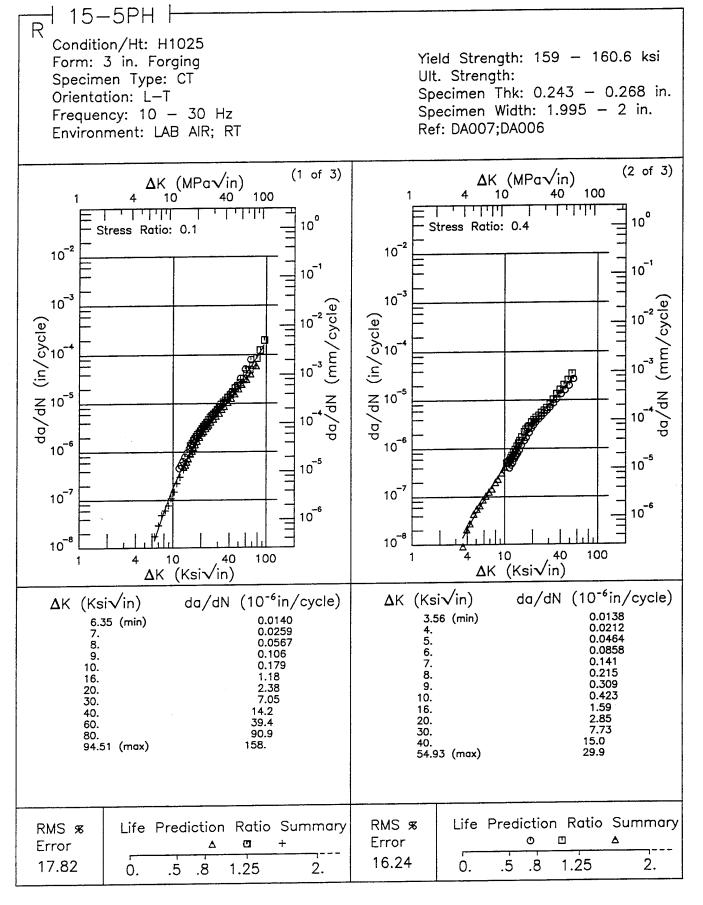


Figure 4.1.3.1.4

Condition/Ht: H1025 Form: 3 in. Forging Yield Strength: 159 - 160.6 ksi Ult. Strength: Specimen Type: CT Specimen Thk: 0.243 - 0.268 in. Orientation: L-T Specimen Width: 1.995 - 2 in. Frequency: 10 - 30 Hz Ref: DA007;DA006 Environment: LAB AIR; RT (3 of 3) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 10 100 100 ليليليا 10° 10° Stress Ratio: 0.8 10-2 10-2 10-1 10⁻¹ 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10 10⁻⁶ 10-6 10 5 10 -5 10⁻⁷ 10⁻⁷ 10 6 10⁻⁶ 10 8 10⁻⁸ 10 40 100 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) ΔK (Ksi√in) 3.69 (min) 4. 5. 0.0667 10. 13. 2.26 4.06 22.80 (max) Life Prediction Ratio Summary RMS % RMS % Life Prediction Ratio Summary Error Δ□ Error 13.26 1.25 0. .5 8. 2. Ö. 1.25 2. .5 .8

15-5PH F

Figure 4.1.3.1.4 (Concluded)

┨ 15―5PH ┞ Condition/Ht: H1025 Yield Strength: 159 - 160.6 ksi Form: 3 in. Forging Ult. Strength: Specimen Type: CT Specimen Thk: 0.25 - 0.267 in. Orientation: L-T Specimen Width: 1.995 - 1.998 in Frequency: 1 Hz Ref: DA006; DA007 Environment: DIST WATER; RT (2 of 2) (1 of 2) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 10 40 100 10 100 40 1 1 1 1 1 1 1 11111 10° 10° Stress Ratio: 0.8 Stress Ratio: 0.1 10-2 10-2 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN · (in/cycle) 10 6 10⁻⁶ 10⁻⁵ 10⁻⁵ 10⁻⁷ 10⁻⁷ 10⁻⁶ 10 6 10 8 10⁻⁸ 10 40 100 40 10 100 ∆K (Ksi√in) **Δ**K (Ksi√in) da/dN ($10^{-6}in/cycle$) da/dN (10⁻⁶in/cycle) **Δ**K (Ksi√in) **Δ**K (Ksi√in) 8.65 (min) 0.524 11.80 (min) 0.766 9. 10. 0.699 13. 16. 20. 25. 30. 1.28 13. 16. 6.09 20. 20.62 (max) 10.6 68.13 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Ш Error ത 🏻 Error 4.17 14.27 0. .5 1.25 2. .8 2. 1.25 0. .5 .8

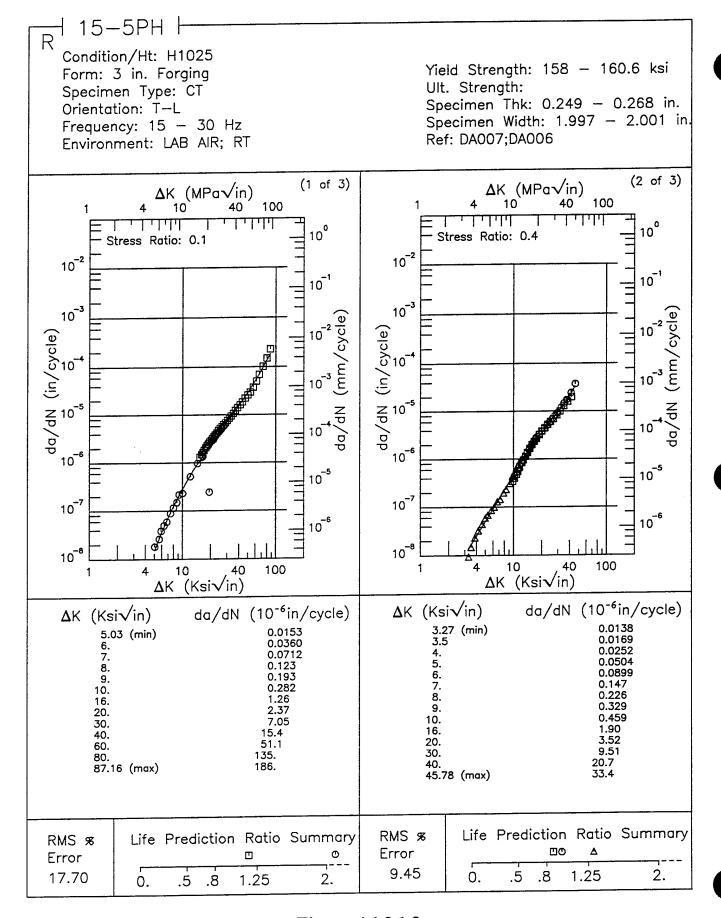


Figure 4.1.3.1.6

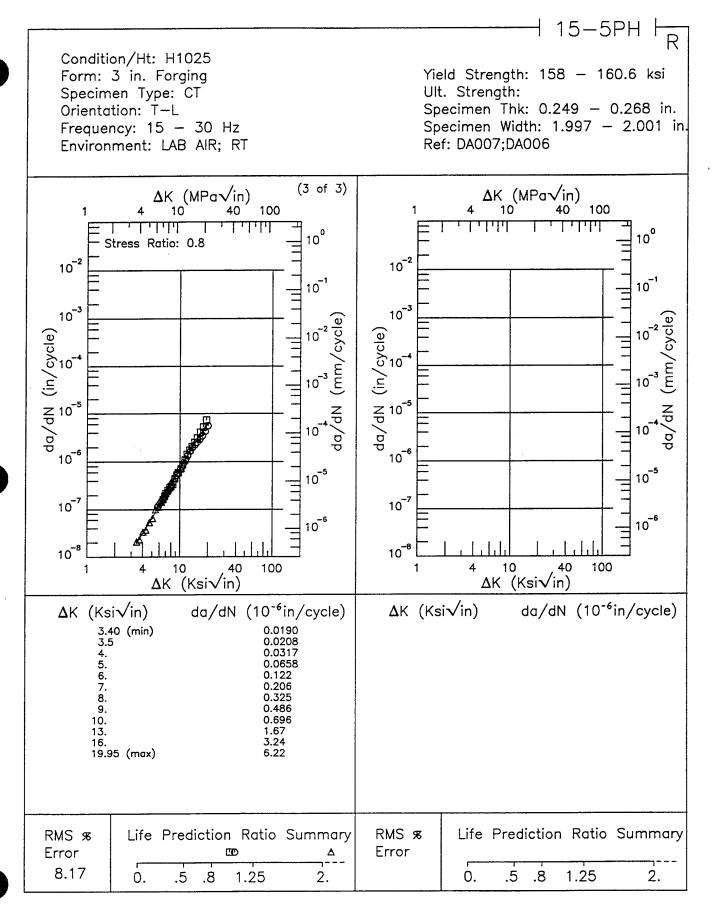


Figure 4.1.3.1.6 (Concluded)

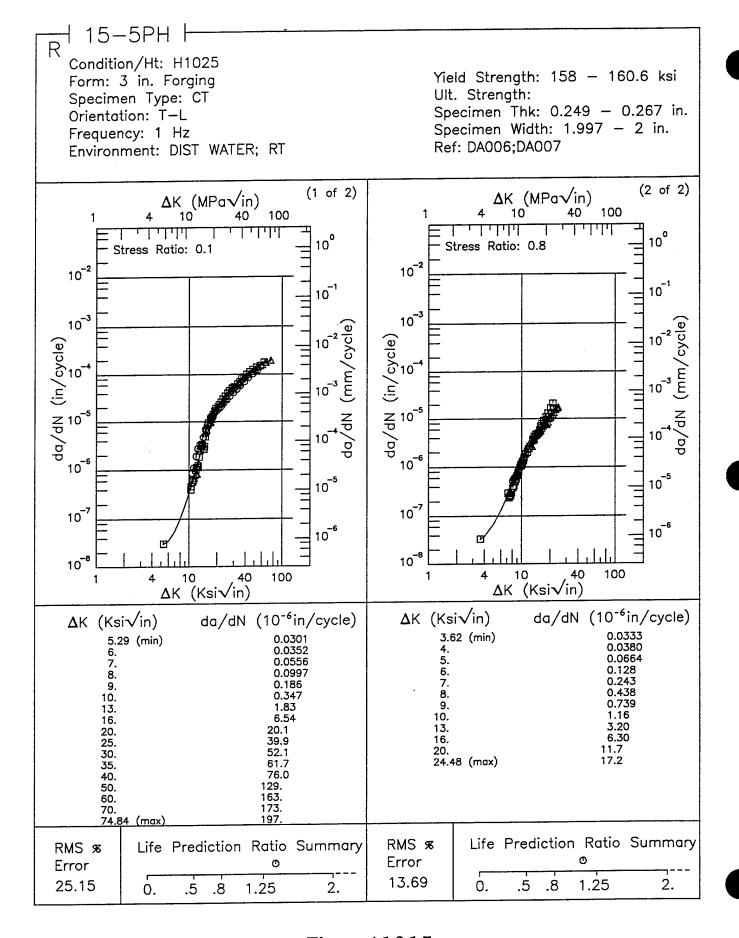


Figure 4.1.3.1.7

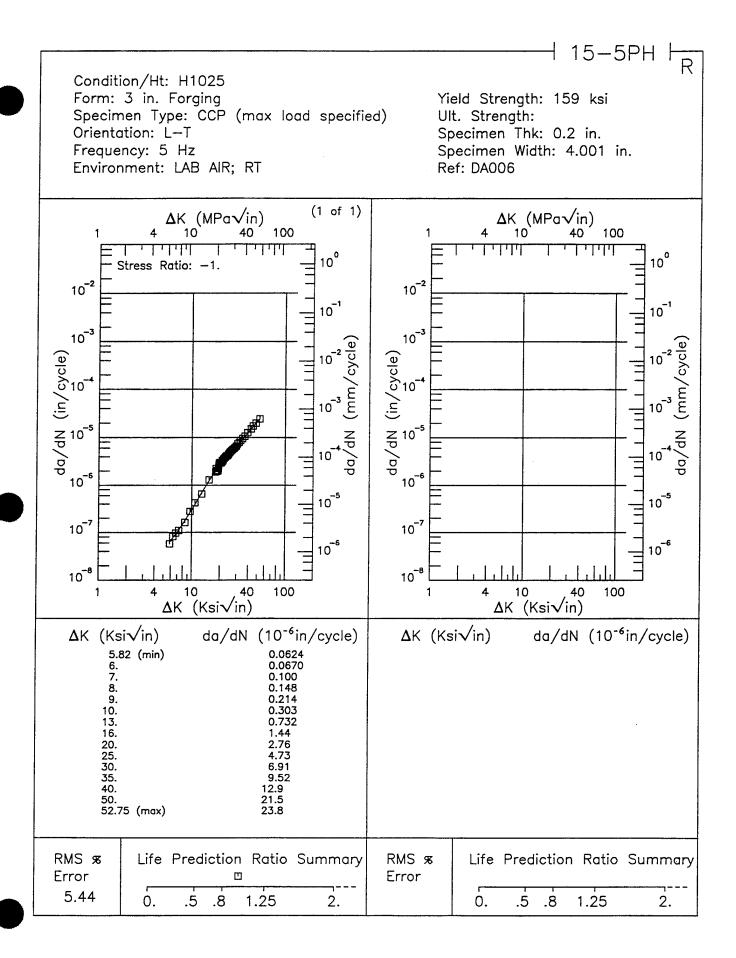


Figure 4.1.3.1.8

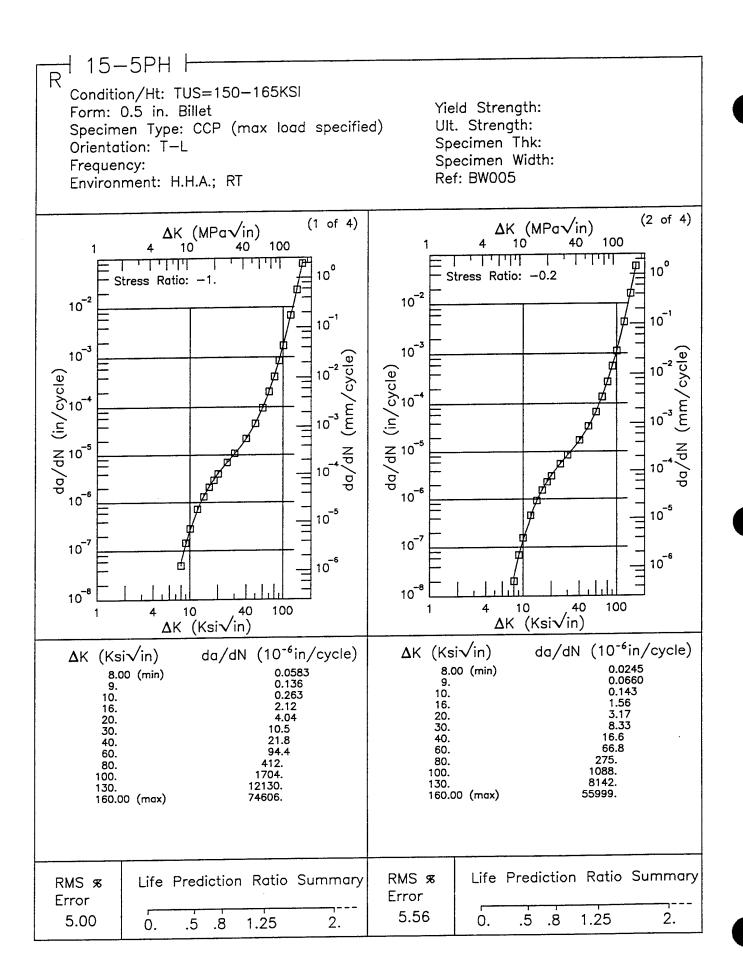


Figure 4.1.3.1.9

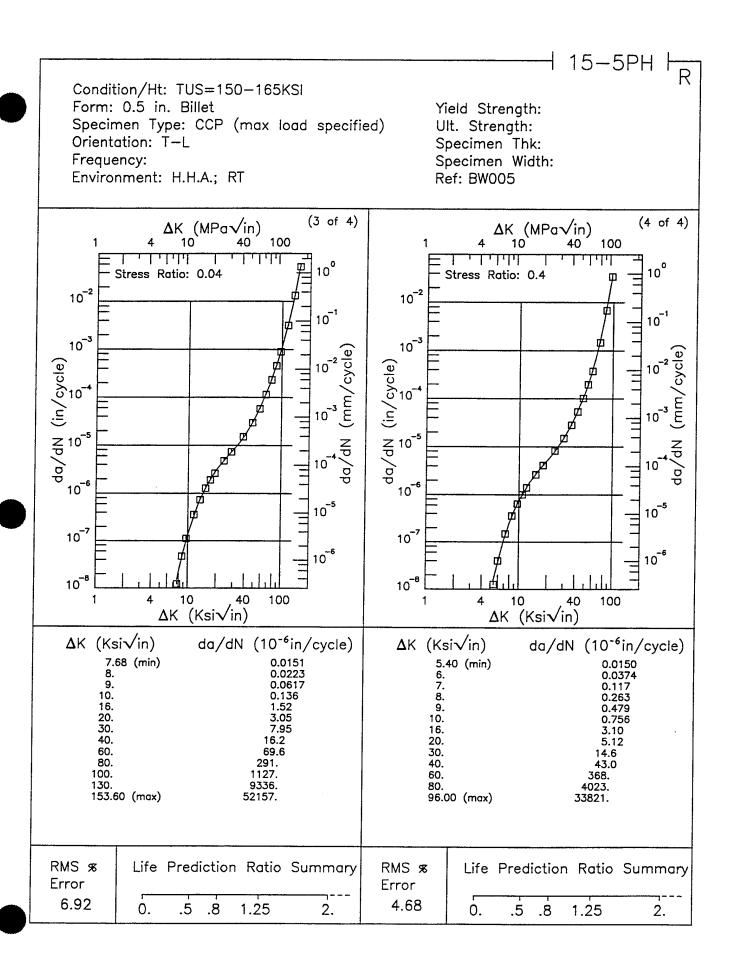


Figure 4.1.3.1.9 (Concluded)

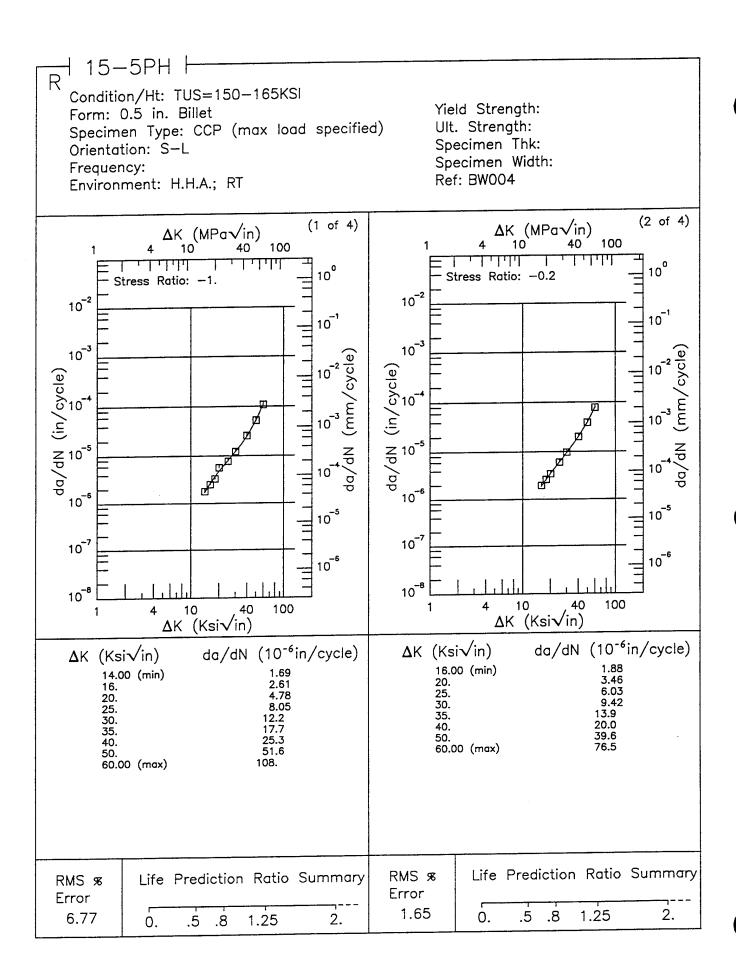


Figure 4.1.3.1.10

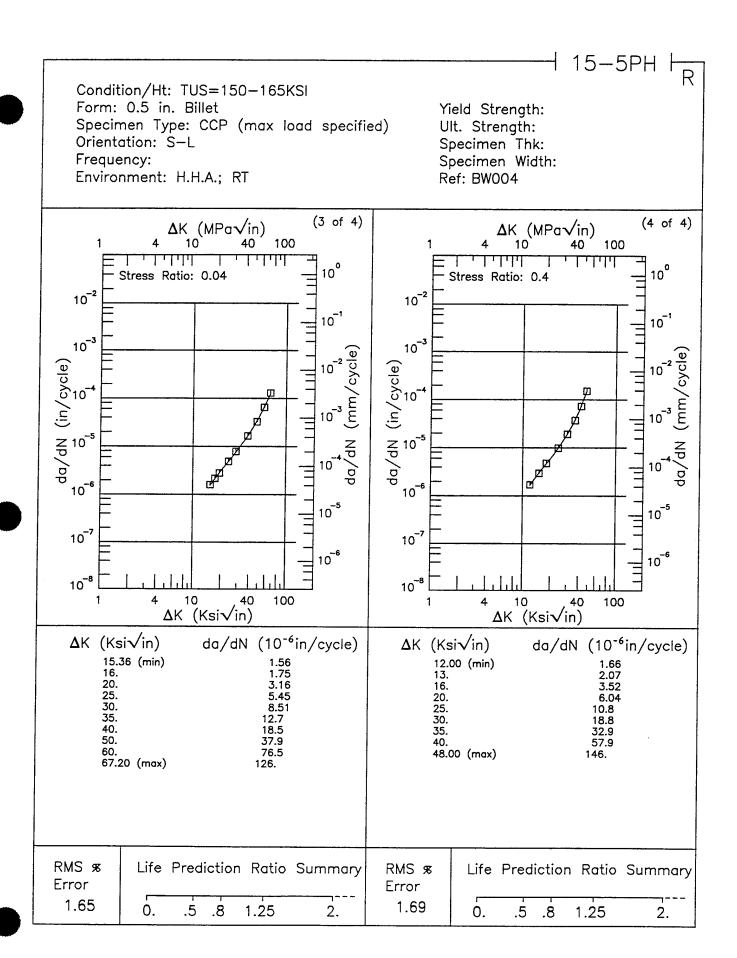


Figure 4.1.3.1.10 (Concluded)

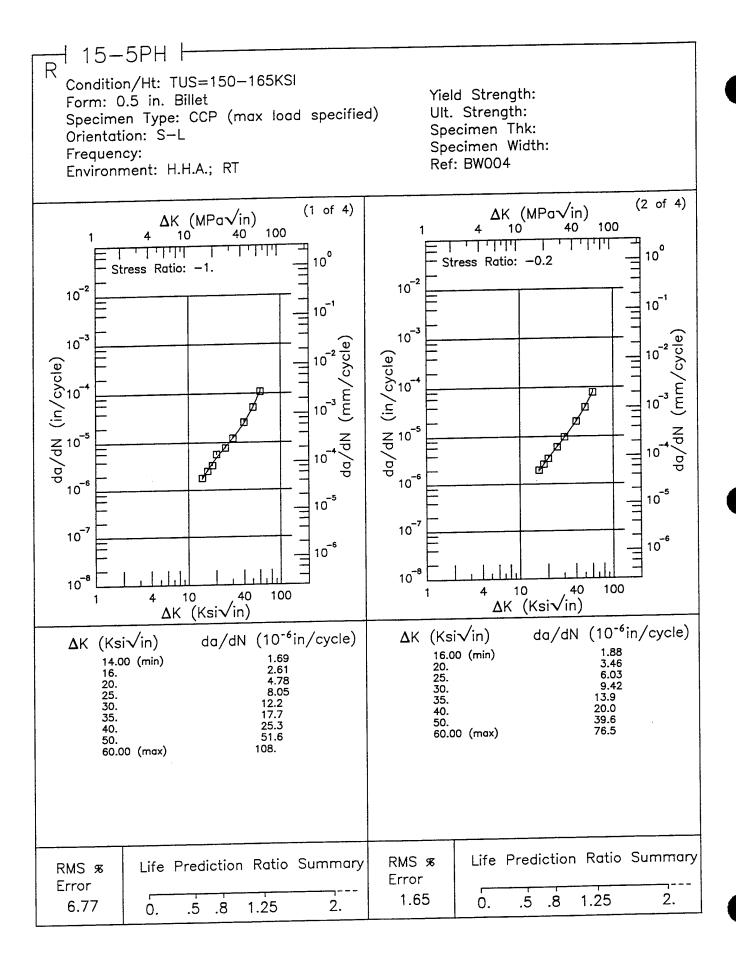


Figure 4.1.3.1.11

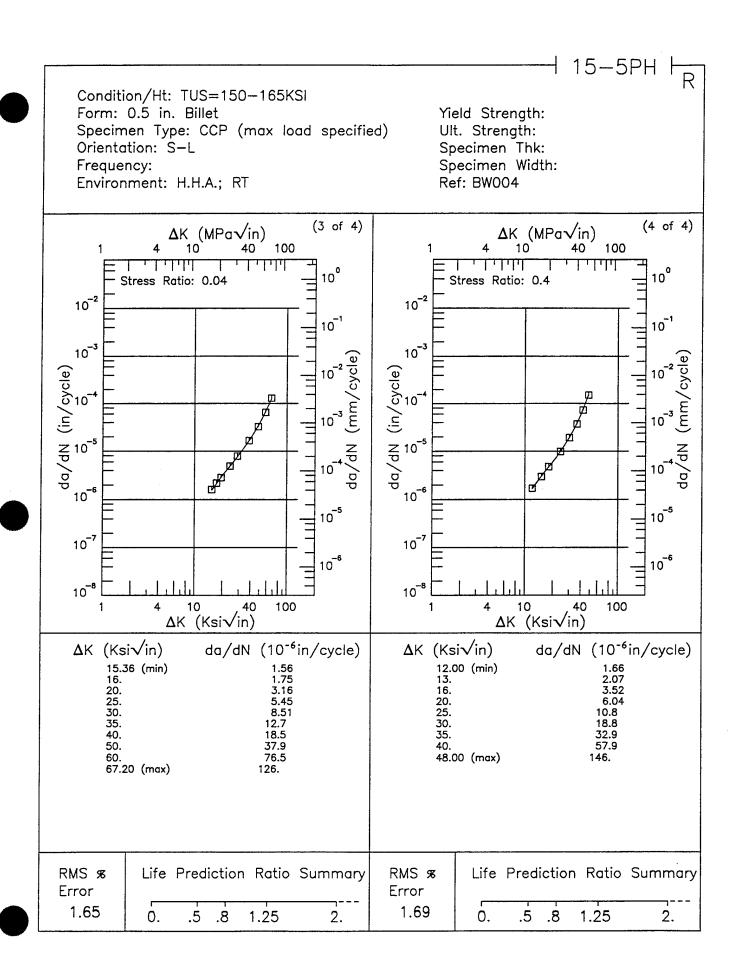


Figure 4.1.3.1.11 (Concluded)

TABLE 4.1.3.3

K_{Isco} SUMMARY FOR STAINLESS STEEL 15-5PH

	Reference	86688	88998	86688	86688	86688	88998
		8	8		å		80
	Test Date	1973	1973	1973	1973	1973	1973
Test	Time (min)		:	į	:		ŀ
ł	K _{la∞} (Ksi√in)	33	89	98	72+	<i>1</i> 2£	72+
ì	Kaivin)	71.8	71.8	71.8	75.7	75.7	7.27
,	(in)			ı			:
	Thk (in)	2.25	2.25	2.25	2.25	2.25	2.25
	Thick (in)	1	-	I	1	1	T
Specimen	Width (in)	8	2	8	2	2	2
92	Design	LO	CT	CT	CL	CT	CT
	Envir.	20% NaCl	Industrial Atm	Seacoast Atm	20% NaCl	Industrial Atm	Seacoast Atm
Yield	Str (Ksi)		171.2			93.1	
S. C.	Spec Or.		T-T			T-L	
Test	Temp Or. (Ksi)		R.T.			R.T.	
Dund	Form		В			ф	
Condition	Heat Treat		H900			H1150M	

* specimen thickness does not meet minimum requirements of $2.5~(rac{K_{loo}}{\sigma_{yy}})$

TABLE 4.2.3.3

K_{Isc} SUMMARY FOR STAINLESS STEEL 15-5PH(AM)

7.001410.00	Decid	Test	ğ	Yield		S	Specimen		Prod	,	;	ł	Test		
Heat Treat	Form	Temp (°F)	Or.	Str (Ksi)	Envir.	Design	Width Thick (in) (in)	Thick (in)	Thk (in)	Crack (in)	Crack Ko Keivin) (Keivin)	K _{laœ} (Ksi√in)	Time (min)	Test Date	Reference
H900	凡	F R.T.	i	175	3.5% NaCl	l CANT	1.5	0.48	£	1	96.8	+08	60009	1971	84333
H1000	F	F R.T.	ŀ	157.9	3.5% NaCl CANT	CANT	1.5	0.48	က	i	114	114*	60000 1971	1971	84333

* specimen thickness does not meet minimum requirements of 2.5 $(\frac{K_{box}}{\sigma_{yy}})$

TABLE 4.3.3.3

K_{Isce} SUMMARY FOR STAINLESS STEEL 15-5PH(VM)

7 374			7	Yield		S	Specimen		Prod	,	,	;	Test	i	
Condition/ Heat Treat	Form		Spec Or.	Temp Or. Str (°F) Or. (Ksi)	Envir.	Design	Width 7 (in)	Thick (in)	Thk (in)	Crack (in)	Crack No K _{leo} (in) (Ksivin) (Ksivin)	Ksi√in)	Time (min)	Test Date	Reference
006H	伍	R.T.	i	174.9	3.5% NaCl	1 CANT	1.5	0.48	4.5		74.5	55.8	48000	1971	84333
H1000	ᅜ	R.T.	i	157.6	157.6 3.5% NaCl CANT	CANT	1.5	1.5 0.48 4.5	4.5	I	120	120+	60000 1971	1971	84333

 $^{+}$ specimen thickness does not meet minimum requirements of 2.5 $(\frac{K_{Loc}}{\sigma_{\mathcal{P}}})^{2}$

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 17-4PH AT ROOM TEMPERATURE

0.001 60.0 53.01 PCGR (10 4 in/cycle) A.K. Level (Kek/in) 9.08 3.41 **ENVIRONMENT: Lab Air** 10.0 0.31 **9**.0 10° FREQ (Hz) 8 0.08 × PRODUCT FORM PLATE ORIENTATION: L-T HEAT TREATMENT CONDITION H 900

TABLE 4.4.1.2.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK 17-4PH AT ROOM TEMPERATURE

ORIENTATION: T-L	: T-L		Ð	ENVIRONMENT: Lab Air	NMEN	T: Lab	Air		
					FC	GR (10	FCGR (10 ⁻⁸ in/cycle)	le)	
CONDITION/ HEAT TREATMENT	PRODUCT	Ħ	FREQ. (Hz)		ΙΔ	Tevel 7	ΔK Level (Ksi\in)	(i	
				2.5	5.0	10.0	20.0	50.0	100.0
		0.1	30			90:0	2.04		
		0.1	30			90.0	2.01		
70001	are digitor	0.5	10				5.88		
ITIOZO	KOUND BAK	0.5	10				5.88		
		0.5	30		0.04	0.51			
		0.5	30		0.03	0.51			

TABLE 4.4.1.2.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 17-4PH AT ROOM TEMPERATURE

ORIENTATION: Unspecified

ENVIRONMENT: H.H.A.

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FCGR (10 ⁴ in/cycle)			
Ų	ΔK Level (Kst√in)	10.0 20.0	
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PI			
PI	HEAT TREATMENT FORM		
PI			

				92	STAINLESS STEEL	ESS STE		17-4PH K _{Io}	$\mathbf{K}_{\mathbf{Io}}$						
	PRODUCT	JCT.				8	SPECIMEN	7	CRACK			K _{Ie}			
CONDITION	FORM	THICK (ln.)	TEST TEMP ('F)	SPEC	YTELD STR (Kel)	WIDTH (In.)	THICK (In.) B	DRSIGN	LENGTH (in.) A	(K _{n,} /TYB) ³ (In.)	K. (Ket • (In.)	K. MEAN	STAN	DATE	REFER
Н 975	Rolled Bar	3.25	R.T.	LR	168.0	2.000	1.000	NB	1.000	0.63	84.60	i	ı	ı	84212
H1025	Round Bar	3.00	R.T.	T.L	175.3	1.990	0.503	CJ	0.837	0.45	74.50	ı	ı	1979	DA001

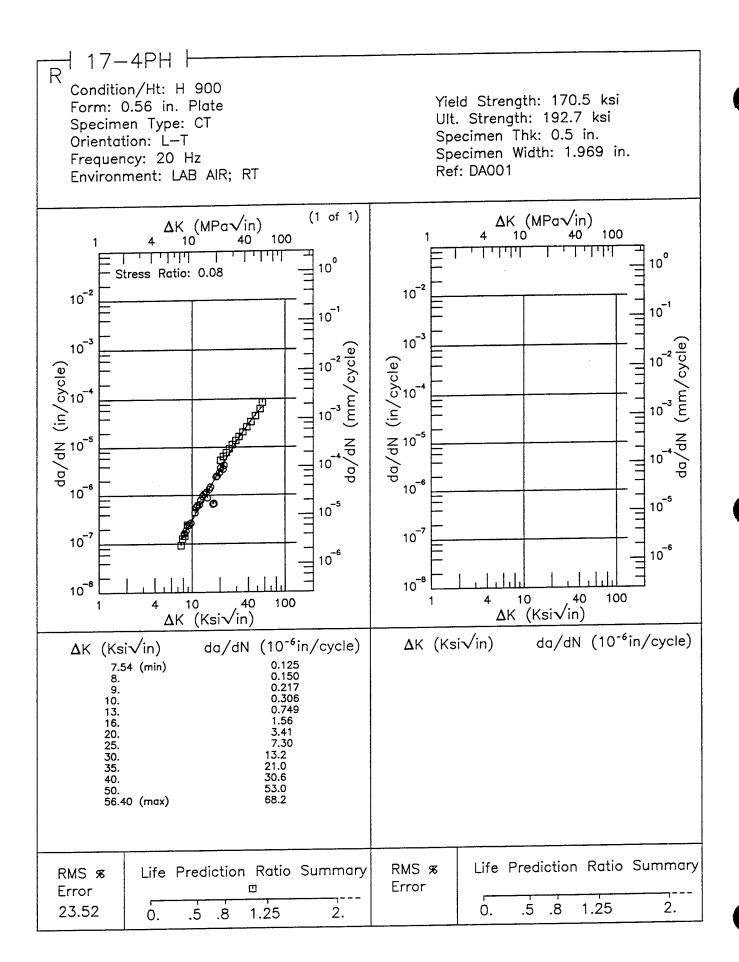


Figure 4.4.3.1.1

17-4PH R Condition/Ht: H1025 Yield Strength: 175.3 ksi Form: 3 in. Round Bar Ult. Strength: 179.8 ksi Specimen Type: CT Orientation: T-L Specimen Thk: 0.502 in. Specimen Width: 1.985 - 2.002 in Frequency: 10 Hz Environment: LAB AIR; RT Ref: DA001 (1 of 2)(2 of 2) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 10 40 100 10 40 100 1 1 1 1 1 1 1 1 لللللث 111111 1111 10[°] 10° Stress Ratio: 0.1 Stress Ratio: 0.5 10-2 10-2 10 10 1 10⁻³ 10-3 10-2 da/dN (in/cycle) da/dN (in/cycle) 10⁻³ 10⁻⁶ 10⁻⁶ 10⁻⁵ 10⁻⁵ 10⁻⁷ 10⁻⁷ 10⁻⁶ 10⁻⁶ 10 8 10⁻⁸ 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) **Δ**K (Ksi√in) $da/dN (10^{-6}in/cycle)$ ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) 20.54 (min) 25. 30. 35. 11.39 (min) 13. 16. 1.48 3.15 0.756 1.29 2.78 5.61 9.33 20. 5.88 49.82 (max) 54.3 28.37 (max) 43.2 RMS % Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary Error Error 4.80 3.01 0. .5 1.25 0. .5 .8 1.25 .8 2. 2.

Figure 4.4.3.1.2

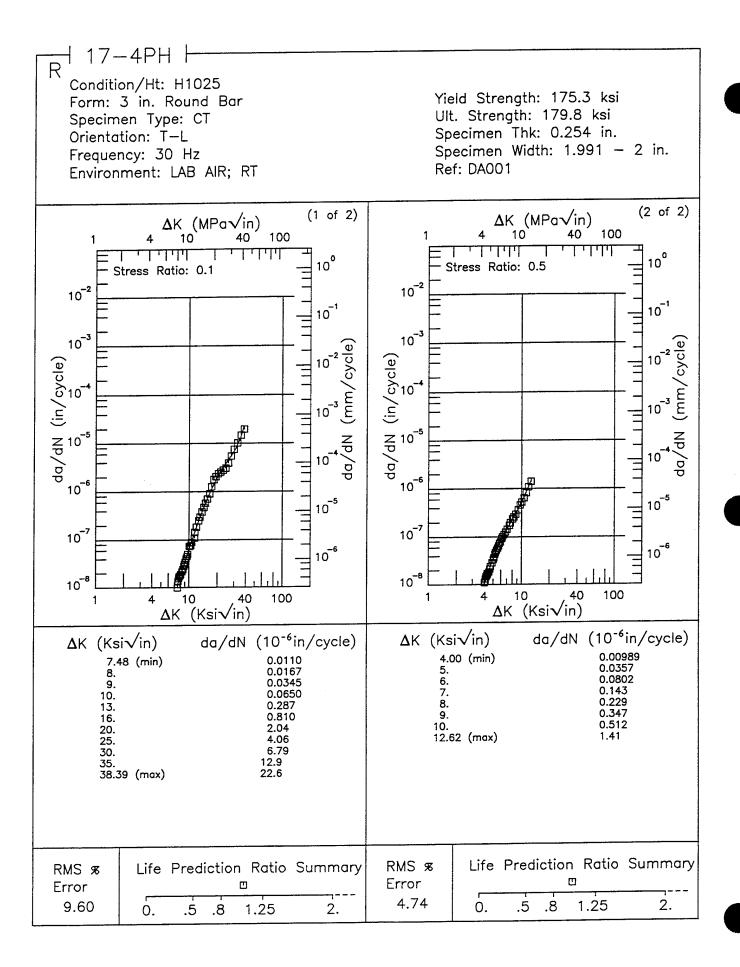


Figure 4.4.3.1.3

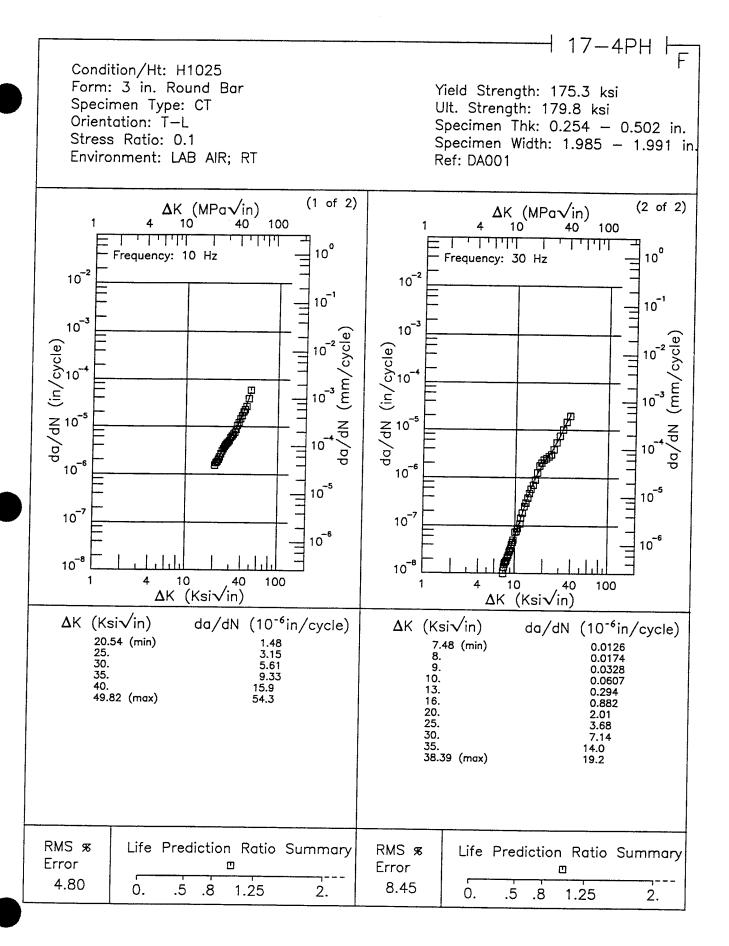


Figure 4.4.3.1.4

17-4PH Condition/Ht: H1025 Yield Strength: 175.3 ksi Form: 3 in. Round Bar Ult. Strength: 179.8 ksi Specimen Type: CT Specimen Thk: 0.254 - 0.502 in. Orientation: T-L Specimen Width: 2 - 2.002 in. Stress Ratio: 0.5 Ref: DA001 Environment: LAB AIR; RT (2 of 2) (1 of 2) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 100 10 40 10 40 100 الملتليك الللك 10⁰ 11111 11111 10⁰ Frequency: 30 Hz Frequency: 10 Hz 10⁻² 10-2 10⁻¹ 10-1 10⁻³ 10⁻³ 10-2 da/dN (in/cycle) da/dN (in/cycle) 10⁻³ 10⁻⁶ 10⁻⁶ 10 5 10⁻⁵ 10⁻⁷ 10⁻⁷ 10⁻⁶ 10 6 10⁻⁸ 10 40 100 4 40 100 4 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 4.00 (min) 5. 0.756 11.39 (min) 0.0344 1.29 2.78 13. 6. 7. 16. 20. 25. 5.88 8. 15.8 43.2 9. 28.37 (max) 10. 12.62 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error 2.92 2. .5 1.25 3.01 0. .8 .5 8. 1.25 2. 0.

Figure 4.4.3.1.5

17-4PH R Condition/Ht: H1025 Yield Strength: Form: Casting Specimen Type: CCP (max load specified) Ult. Strength: Specimen Thk: 0.103 - 0.113 in. Orientation: Specimen Width: 2.915 - 2.955 in Frequency: 1 Hz Ref: GD010 Environment: H.H.A.; RT (1 of 1) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 10 100 40 100 10 40 10° 10° Stress Ratio: 0.02 10-2 10 2 10⁻¹ 10 1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10 6 10⁻⁵ 10 -5 10⁻⁷ 10⁻⁷ 10⁻⁶ 10-6 10 -8 10 8 40 100 40 100 10 10 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 8.33 (min) 9. 10. 0.214 0.245 13. 16. 20.04 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Φ Error 1.25 18.73 .5 .8 2. 0. 0. .5 8. 1.25 2.

Figure 4.4.3.1.6

K_{Isce} SUMMARY FOR STAINLESS STEEL 17-4PH

7 - 7 - 7		Test	5	Yield		$\mathbf{S}_{\mathbf{I}}$	Specimen		Prod	,	;		Test		
Condition/ Heat Treat	Form	Temp (°F)	Spec Or.	Str (Ksi)	Envir.	Design	Width Thick (in)	Thick (in)	Thk (in)	(in)	Crack No K _{low} (in) (Ksivin)	K _{loo} (Ksi√in)	Time (min)	Test Date	Reference
H900	В	R.T.		176.5	3.5% NaCi	31 CANT	1.5	95-0	1.75	ı	51.5	51.5	60009	1971	84333
H1000	В	R.T.	;	157.9	3.5% NaCl CANT	CANT	1.5	1.5 0.48 1.75	1.75	:	119	119+	60000 1971	1971	84333

 $^{+}$ specimen thickness does not meet minimum requirements of 2.5 $(rac{K_{loo}}{\sigma_{ys}})^{2}$

TABLE 4.5.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR STAINLESS STEEL ALLOY 17-7PH AT ROOM TEMPERATURE

Product					$K_{L\!c}$	$K_{Ic}~(ksi\!\sqrt{in})$	<u> </u>			
Form	Condition/Heat Treatment			02	pecime	Specimen Orientation	itation	:		
			L-T			T-L			T-S	
		Mean K _{to}	Std Dev	u	Mean K _{Io}	Std Dev	n	Mean K _{ie}	Std Dev	и
Rolled Bar	RH1050	1		:	47.	7.0	3	ŀ	i	1

1 of 1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 17-7PH AT ROOM TEMPERATURE

ORIENTATION: 1

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ENVIRONMENT: Lab Air	
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PCGR (10 ⁻⁸ in/cycle)	Δ.K. Løvel (Ksk/in)	5.0	
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d	HEAT TREATMENT FORM		

TABLE 4.5.1.2.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 17-7PH AT ROOM TEMPERATURE

	196.0	
	(g) (g)	
	rc/e) (ii)	
Air	PCCR (10.6 in/cycle) ΔK Level (Ksi/in) α	4.59
ENVIRONMENT: Lab Air	ZR (10 ⁻⁸ K Lovel	0.38
Ä	CGR IR L	0.
ME	FC A.	0.02
IROI	2.5	
ENV.	Si	
	FREQ (Hz)	50
	E	
	R	0.1
	1.0	
	ROBUC	PLATE
Ţ	PRODUCI	Ľ.
T Z		
TIO	11.	
NTA	NEN VIEN	
ORIENTATION: T-L	FFIO	TH1050
	OND TRE	THI
	CONDITION/ HEAT TREATMENT	
	H	
- 1		

TABLE 4.5.2.1

				Ω	IAINLE	STAINLESS STEEL		I7-7FH K _{lo}	f _{Io}						
	PRODUCE	UCT				Sa	SPECIMEN	-	CRACK			K _{Ie}			
CONDITION	FORM	THICK (in.)	TEMP TEMP (°F)	SPEC OR	YIRLD STR (Kal)	WIDTH (in.) W	THICK (In.)	DESIGN	LENGTH (In.) A	(K, TY8)* (in.)	R., (Kai • √(π.)	K. MEAN	STAN DEV	DATE	REFER
		1.25			190.0	2.000	1.000	CT	1.026	0.15	47.10			1973	86688
RH1060	Rolled Bar	1.26	R.T.	T-L	190.0	2.000	1.000	Ę.	1.025	0.15	47.70	47.0	0.7	1973	86688
		1.25			190.0	2.000	1.000	t c	1.066	0.16	46.30			1973	86688

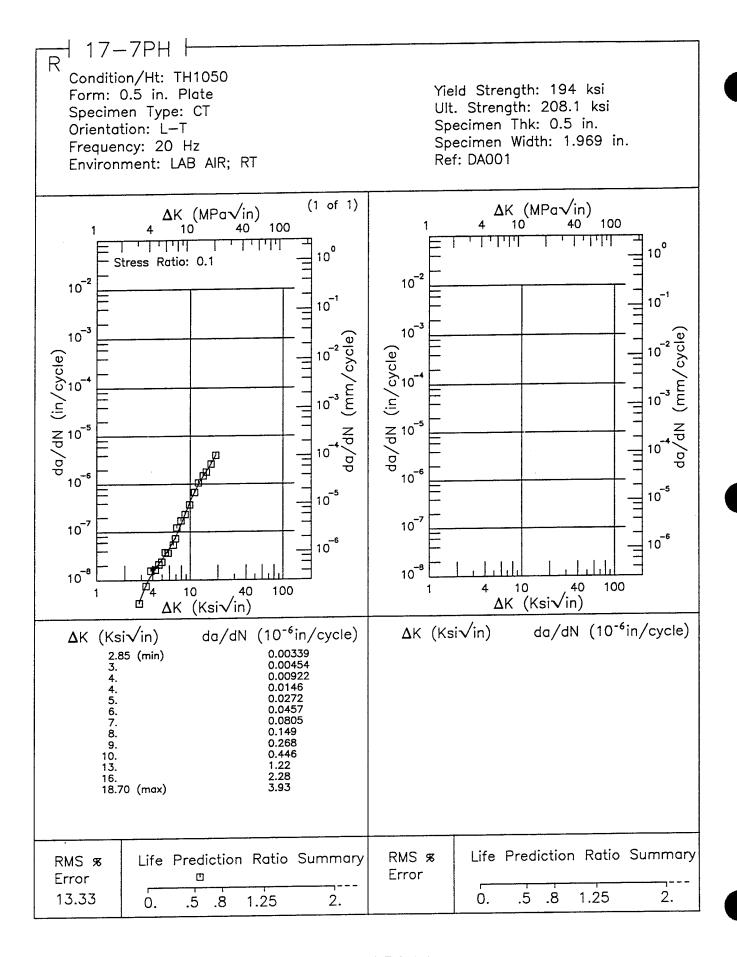


Figure 4.5.3.1.1

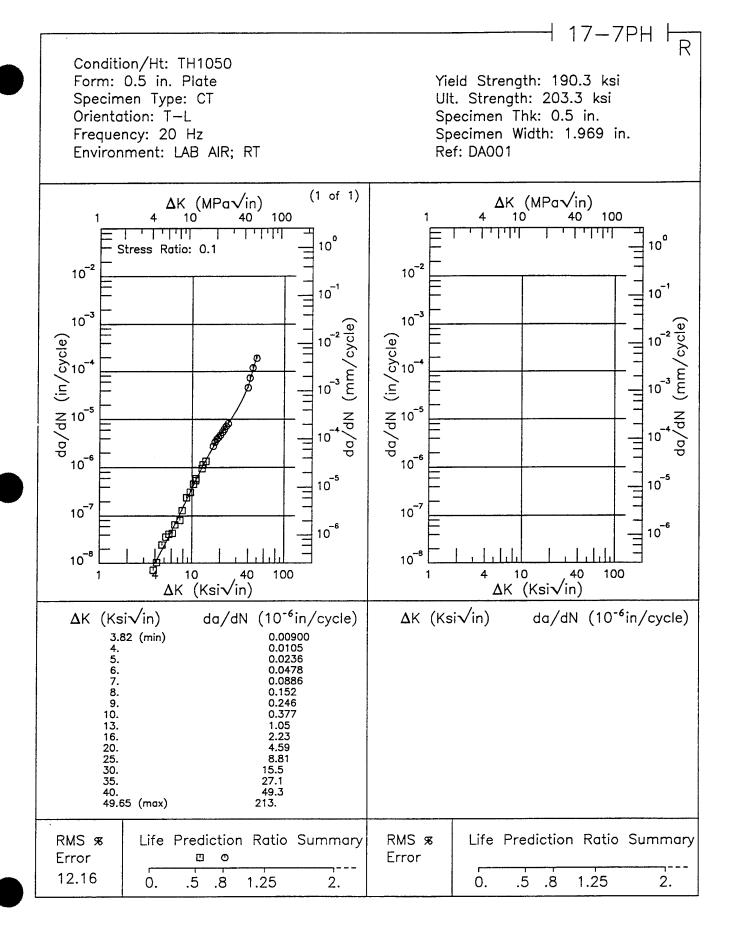


Figure 4.5.3.1.2

TABLE 4.5.3.3

Klscc SUMMARY FOR STAINLESS STEEL 17-7PH

Condition/	7	Test	Z	Yield		S	Specimen			,	,		Test		
Heat Treat	Form	Temp Or. Str (°F) (Ksi)	opec Or.	Str (Ksi)	Envir.	Design	Width Thick (in)	Thick (in)	Thk (in)	Crack (in)	Crack Ko K _{loo} (in) (Ksivin) (Ksivin	K _{la∞} (Ksi√in)	Time (min)	Test Date	Reference
RH950	В	R.T.		171.3	171.3 8.5% NaCi	CANT	1.5	0.48	1.75	ı	32.3	<19	42000	1971	84333
					20% NaCl	LO	7	1	1.25	i	47	10	:	1973	86688
RH1050	В	R.T.	T-L	T-L 190.5	Industrial Atm	£	2	1	1.25	ŀ	47	24	***	1973	86688
					Seacoast Atm	CI	7	-	1.25	1	47	12	:	1973	88998
TH1050	В	R.T.		-	3.5% NaCl	CANT	1.5	0.48	1.75	i	38.7	15.8	30000 1971	1971	84333

TABLE 4.6.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 21-6-9 NI40 AT ROOM TEMPERATURE

ORIENTATION: T-L

ENVIRONMENT: Lab Air

71.4	3.95	0.4			0.2		
78.59	3.56 7	0.56			0.1	SHEET	ANNEALED
57.29	2.35 5	0.34			0.01		
60.0 100.0	20.0	10.0	2.5 5.0	5			
	(Ksivin)	ΔK Level (Ksk/in)	7	(Hz)	4	FORM	HEAT TREATMENT
				FREG	;	PRODUCT	CONDITION
	PCGR (10 ⁻⁸ tr/cycle)	CGR (10 ⁻¹	H				

21-6-9 NI40 Condition/Ht: ANNEALED Yield Strength: 60 ksi Form: 0.03 in. Sheet Specimen Type: CCP (max load specified) Ult. Strength: 100 ksi Specimen Thk: 0.026 - 0.027 in. Orientation: T-L Specimen Width: 2.308 - 2.309 in Frequency: Ref: GD012 Environment: LAB AIR; RT (2 of 3)(1 of 3)ΔK (MPa√in) Δ K (MPa \sqrt{in}) 100 10 40 100 40 10 <u>, 1, 1, 1, 1, 1, 1</u> لللللت 10° 11111 TTITI 10° Stress Ratio: 0.1 Stress Ratio: 0.01 10⁻² 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) S N 10 6 10-6 10⁻⁵ 10 5 10⁻⁷ 10⁻⁷ 10 6 10 6 10 8 10⁻⁸ 100 10 40 10 40 100 4 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 6.73 (min) 7. 8. 0.145 0.154 6.80 (min) 7. 0.204 8. 9. 9. 10. 13. 16. 20. 25. 30. 35. 40. 50. 60. 70. 215. 73.97 (max) 369. 84.57 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Ø Error Error 0 29.10 24.49 .5 1.25 2. 2. 0. .8 1.25 0. .5 8.

Figure 4.6.3.1

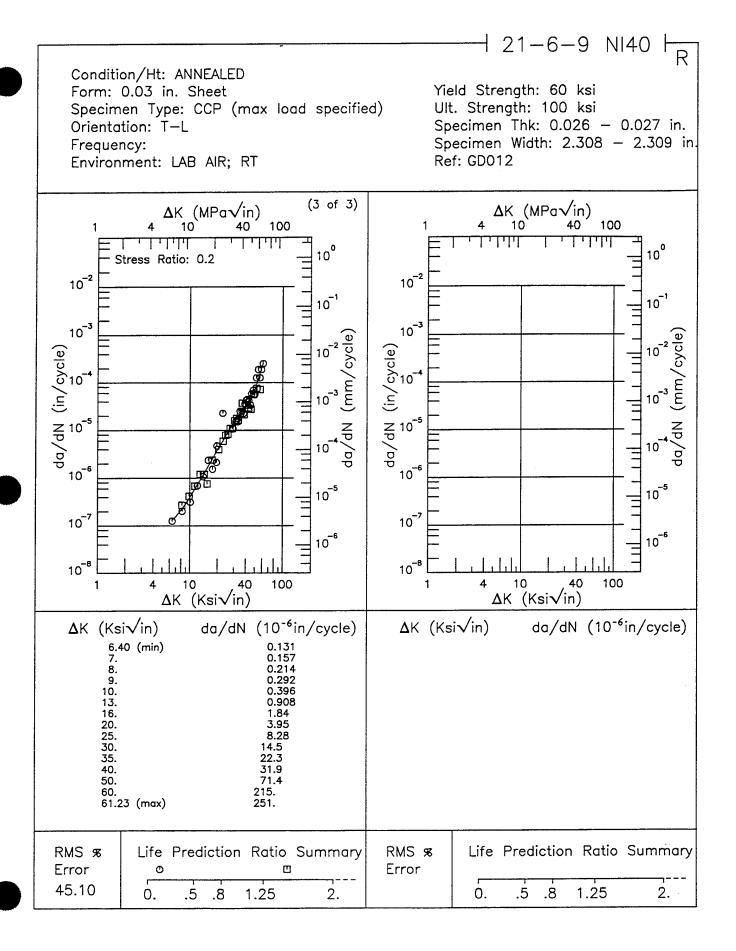


Figure 4.6.3.1 (Concluded)

TABLE 4.7.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK 304 AT ROOM TEMPERATURE

	100.00	6	6
	rde) in)	66.99	27.99
Air	ER (10 ⁻⁸ in/cyc Lovel (Ksi/ii 10.0 20.0		1.95
r: Lab	FCGR (10 ⁻⁶ in/cycle) ΔK Level (Ksi/in) 0 100 200 5		
ENVIRONMENT: Lab Air	PCC AR		
WIRO	23		
E	FREQ (HZ)	0.03	6.67
·	æ	0.	0.
:L-T	PRODUCT		PLATE
ORIENTATION: L-T	CONDITION/ HEAT TREATMENT		ANNEALED

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR △K 304 AT ROOM TEMPERATURE

	0.1	
	100.0	
	_	
	01	32.46
	(d)	32
	FCGR (10 ⁻⁶ in/cycle) ΔK Level (Kst/in) α 100 200 6	
ف	6 in/cycl (Kst/in	92
Ę	in 75 88	1.86
ENVIRONMENT: Lab Air	9 (
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	E .0.	
F	10 ×	
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X	0.0	
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TABLE 4.7.1.2.3

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK 304 AT ROOM TEMPERATURE

100.0 86.0 PCGR (10⁻⁸ in/cycle) ΔK Level (Keivin) 20.0 1.39 3.09 2.76 3.06 2.83 2.85 2.59 **ENVIRONMENT: Lab Air** 10.0 0.13 0.14 0.2 8.0 10 10 10 FREQ (Hz) 1.67-6 10-15 1.67 15 2 က 0.05 0.05 0.05 0.05 0.1 2 0.1 0.1 PRODUCT FORM SHEET PLATE **ORIENTATION: Unspecified** HEAT TREATMENT CONDITION ANNEALED & AGED ANNEALED

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304 H Condition/Ht: ANNEALED Yield Strength: Form: Sheet Specimen Type: CCP (max load specified) Ult. Strength: Specimen Thk: 0.01 - 0.018 in. Orientation: Specimen Width: 0.995 - 2 in. Frequency: 1.7 - 15 Hz Ref: HD009 Environment: LAB AIR; RT (2 of 2) (1 of 2)ΔK (MPa√in) Δ K (MPa \sqrt{in}) 100 10 40 100 10 40 11111 10° 1 1 1 1 1 1 1 10⁰ Stress Ratio: 0.1 Stress Ratio: 0.05 10-2 10 -2 10 1 10-1 10⁻³ 10⁻³ 10 2 10-2 da/dN (in/cycle) da/dN (in/cycle) اِتَ مَا 10 -3 10⁻⁶ 10⁻⁶ 10 -5 10 -5 10⁻⁷ 10⁻⁷ 10 6 10 6 10⁻⁸ 10-8 40 100 10 100 40 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) da/dN (10⁻⁶in/cycle) **Δ**K (Ksi√in) **Δ**K (Ksi√in) 0.154 0.112 0.144 0.416 10.85 (min) 9.16 (min) 13. 16. 20. 25. 0.299 10. 13. 0.877 16. 3.09 23.49 (max) 32.52 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error + ->03\100 Error 26.42 2. 24.35 0. .5 .8 1.25 2. .5 .8 1.25 0.

Figure 4.7.3.1.1

1 304 H Condition/Ht: ANNEALED Yield Strength: Form: Sheet Ult. Strength: Specimen Type: CCP (max load specified) Specimen Thk: 0.018 in. Orientation: Specimen Width: 0.995 - 1.998 in. Stress Ratio: 0.05 Environment: LAB AIR; RT Ref: HD009 (1 of 2) (2 of 2) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 10 100 100 40 10 40 Lilili 1 1 1 1 1 1 TTTTT10° 10° Frequency: 15 Hz Frequency: 10 Hz 10-2 10⁻² 10-1 10-1 10⁻³ 10⁻³ 10-2 da/dN (in/cycle) da/dN (in/cycle) 10⁻³ 10⁻⁶ 10⁻⁶ 10 -5 10 -5 10⁻⁷ 10⁻⁷ 10-6 10-6 10⁻⁸ 10 8 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) $da/dN (10^{-6}in/cycle)$ **Δ**K (Ksi√in) Δ K (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) 9.98 (min) 10. 0.200 0.200 9.16 (min) 10. 0.112 0.133 0.360 13. 0.454 13. 16. 1.36 16. 1.01 20. 2.83 3.06 20. 23.49 (max) 21.04 (max) 5.62 Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error ΔD Error □ +Δ ⊙ 15.52 28.53 1.25 0. .5 8. 0. .5 .8 1.25 2. 2.

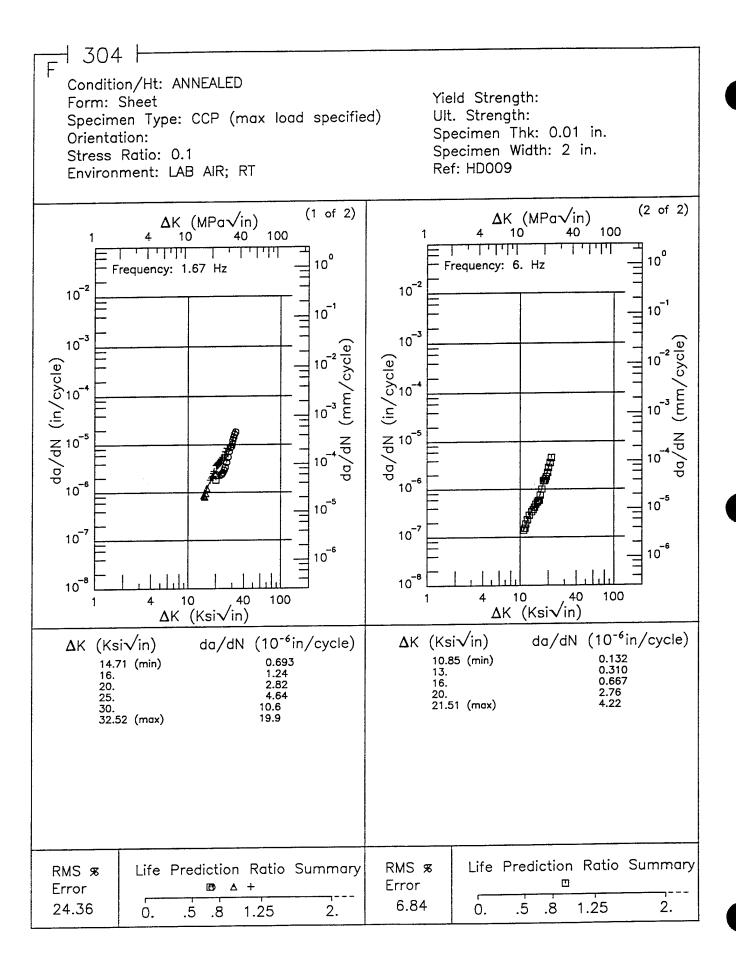
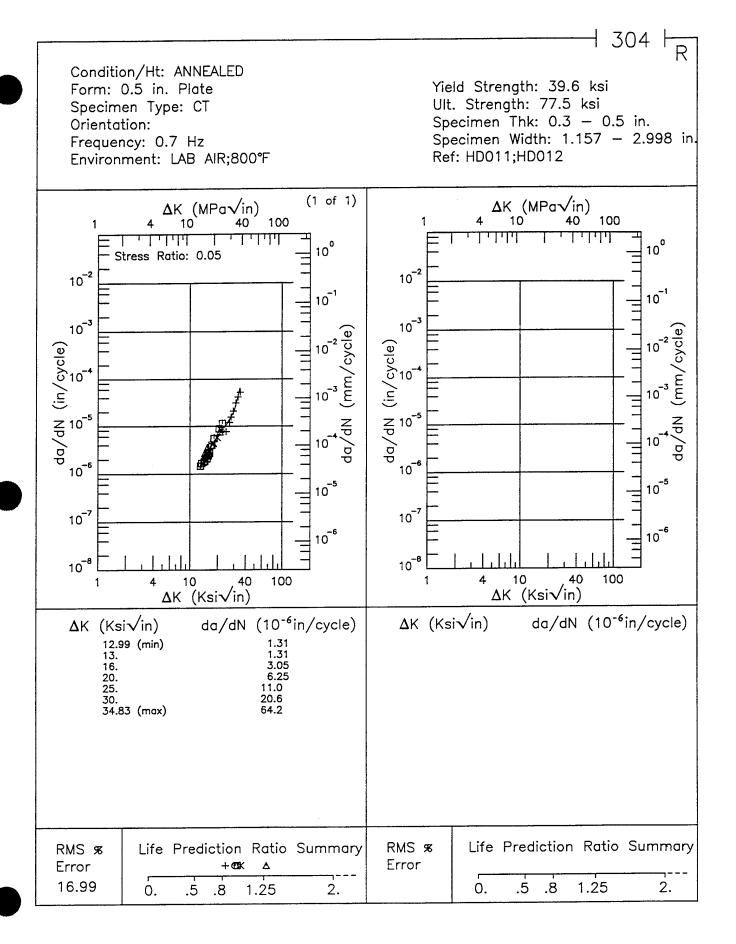


Figure 4.7.3.1.3



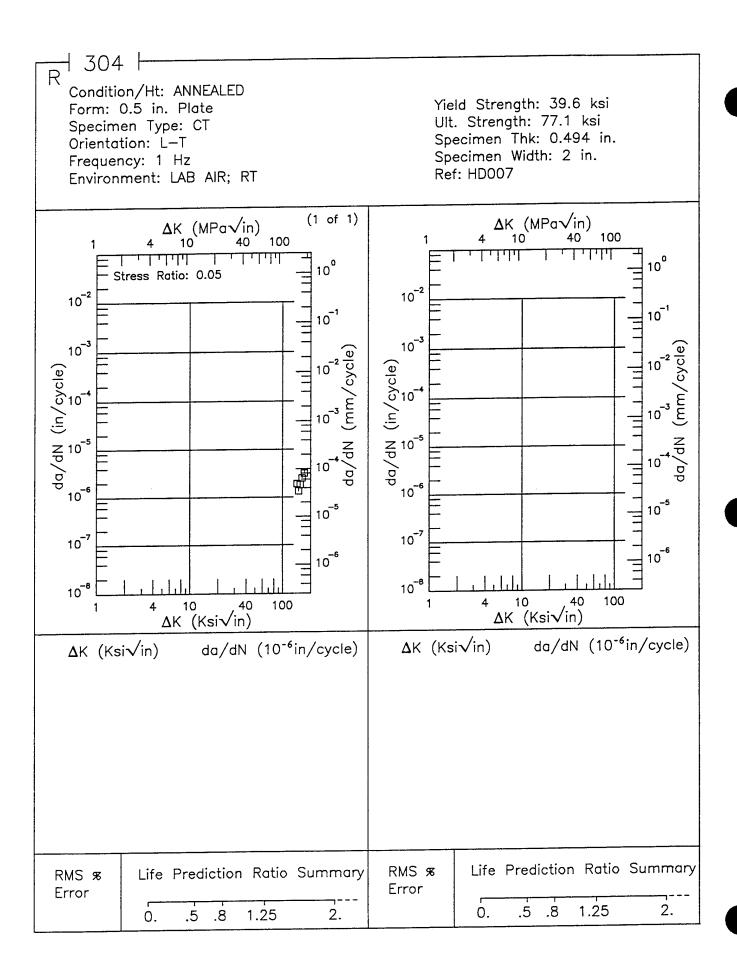
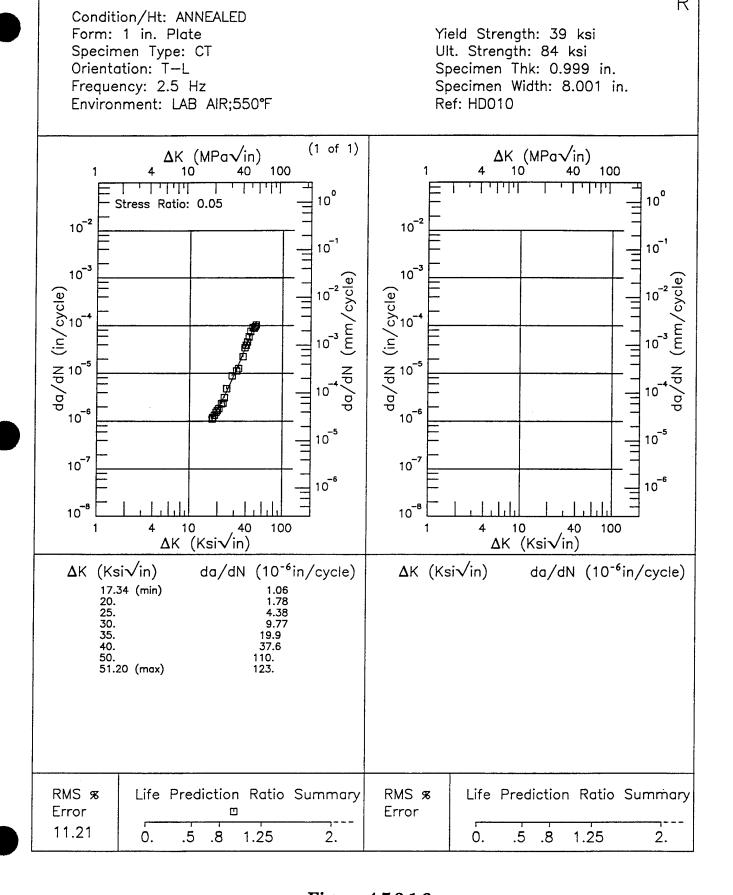


Figure 4.7.3.1.5



304 H

Figure 4.7.3.1.6

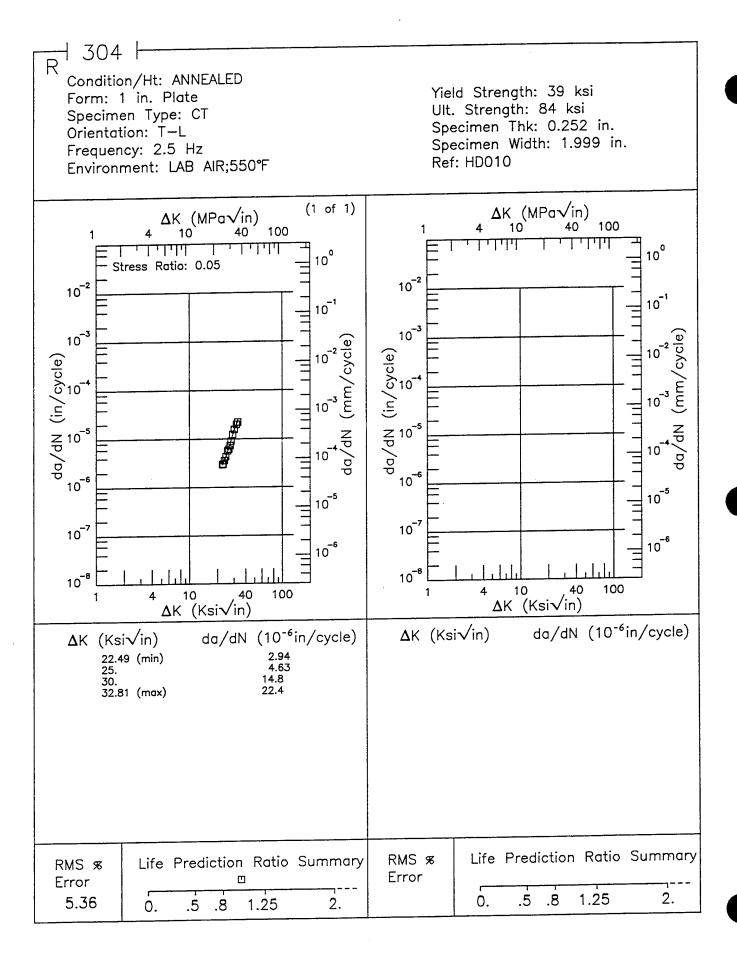


Figure 4.7.3.1.7

Condition/Ht: ANNEALED Yield Strength: 39.6 ksi Form: 0.5 in. Plate Ult. Strength: 77.1 ksi Specimen Type: SENT Specimen Thk: 0.491 in. Orientation: L-T Specimen Width: 4.91 - 4.95 in. Stress Ratio: 0. Ref: HD007 Environment: LAB AIR; RT (1 of 2)(2 of 2) $\Delta K (MPa\sqrt{in})$ Δ K (MPa \sqrt{in}) 100 100 10 40 40 111111 1.1111 10° 10° Frequency: 0.03 Hz Frequency: 6.67 Hz 10-2 10-2 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10 6 10-6 10⁻⁵ 10 -5 10⁻⁷ 10⁻⁷ 10⁻⁶ 10⁻⁶ 10-8 10⁻⁸ 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) **Δ**K (Ksi√in) da/dN (10⁻⁶in/cycle) 32.53 (min) 35. 40. 0.831 1.95 2.98 11.1 14.7 16.50 (min) 20. 25. 30. 35. 50. 60. 56.0 70. 80. 40. 50. 205. 217. 82.69 (max) 60. 68.22 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error 5.20 6.74 .5 1.25 0. .8 1.25 0. .8 2. .5 2.

1 304 H

Figure 4.7.3.1.8

304 Condition/Ht: ANNEALED Yield Strength: 39.6 ksi Form: 0.5 in. Plate Ult. Strength: 77.1 ksi Specimen Type: SENT Specimen Thk: 0.493 - 0.496 in. Orientation: T-L Specimen Width: 4.91 - 4.915 in. Stress Ratio: 0. Ref: HD007 Environment: LAB AIR; RT (2 of 2) (1 of 2) ΔK (MPa√in) ΔK (MPa√in) 100 10 40 100 10 40 10° 10° Frequency: 6.67 Hz Frequency: 3 Hz 10-2 10-2 10 1 10 -1 10⁻³ 10 da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10-6 10 5 10 5 10⁻⁷ 10⁻⁷ 10⁻⁶ 10⁻⁶ 10 8 10 8 40 100 10 40 100 1 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 1.09 1.86 16.13 (min) 20. 25. 30. 35. 40. 50. 60. 67.92 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error 5.77 .5 .8 1.25 2. 0. 1.25 2. .5 0. 8.

Figure 4.7.3.1.9

1 304 H Condition/Ht: ANNEALED & AGED Form: 0.5 in. Plate Yield Strength: 39.6 ksi Ult. Strength: 77.1 ksi Specimen Type: CT Specimen Thk: 0.496 in. Orientation: Specimen Width: 2.001 in. Frequency: 3 Hz Ref: HD008 Environment: LAB AIR; RT (1 of 1) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 10 40 100 10 100 40 11111 10° 10° Stress Ratio: 0.05 10-2 10-2 10 -1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10 10⁻⁶ 10-6 10 5 10⁻⁷ 10⁻⁷ 10 6 10⁻⁶ 10-8 10⁻⁸ 40 100 10 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 19.08 (min) 20. 25. 30. 11.4 27.5 30.0 35. 35.83 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error 2.45 .5 1.25 0. .5 .8 1.25 2. 0. .8 2.

Figure 4.7.3.1.10

1 of 1

TABLE 4.8.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK 316 AT ROOM TEMPERATURE

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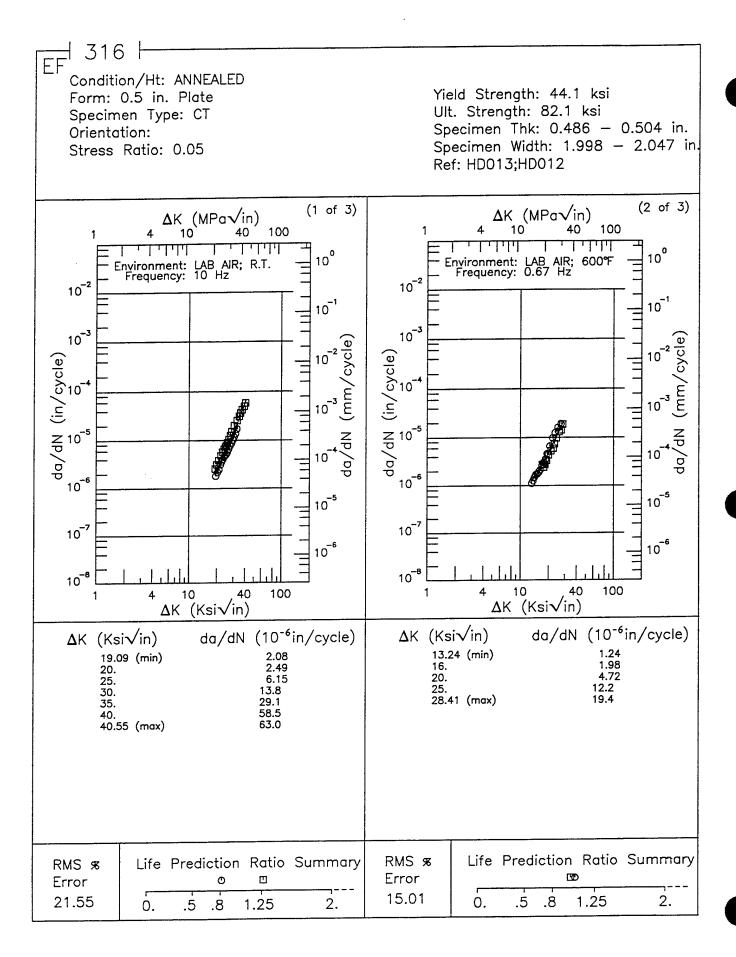


Figure 4.8.3.1.1

Yield Strength: 44.1 ksi Form: 0.5 in. Plate Specimen Type: CT Ult. Strength: 82.1 ksi Specimen Thk: 0.486 - 0.504 in. Orientation: Specimen Width: 1.998 - 2.047 in Stress Ratio: 0.05 Ref: HD013;HD012 (3 of 3) Δ K (MPa \sqrt{in}) ΔK (MPa√in) 100 10 100 4 10 $\frac{1}{1}$ 10° 10⁰ Environment: LAB AIR; 800°F Frequency: 0.67 Hz 10-2 10-2 10 10⁻³ 10⁻³ 10-2 da/dN (in/cycle) da/dN (in/cycle) 10 10 10⁻⁶ 10⁻⁶ 10⁻⁵ 10 -5 10⁻⁷ 10⁻⁷ 10 6 10⁻⁶ 10 8 10⁻⁸ 40 100 10 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) $da/dN (10^{-6}in/cycle)$ ΔK (Ksi√in) ΔK (Ksi√in) 16.21 (min) 20. 25. 30. 30.70 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS & Error Error 5.85 Ó. .5 1.25 0. .5 1.25 .8 2. .8 2.

Condition/Ht: ANNEALED

1 316 EF

Figure 4.8.3.1.1 (Concluded)

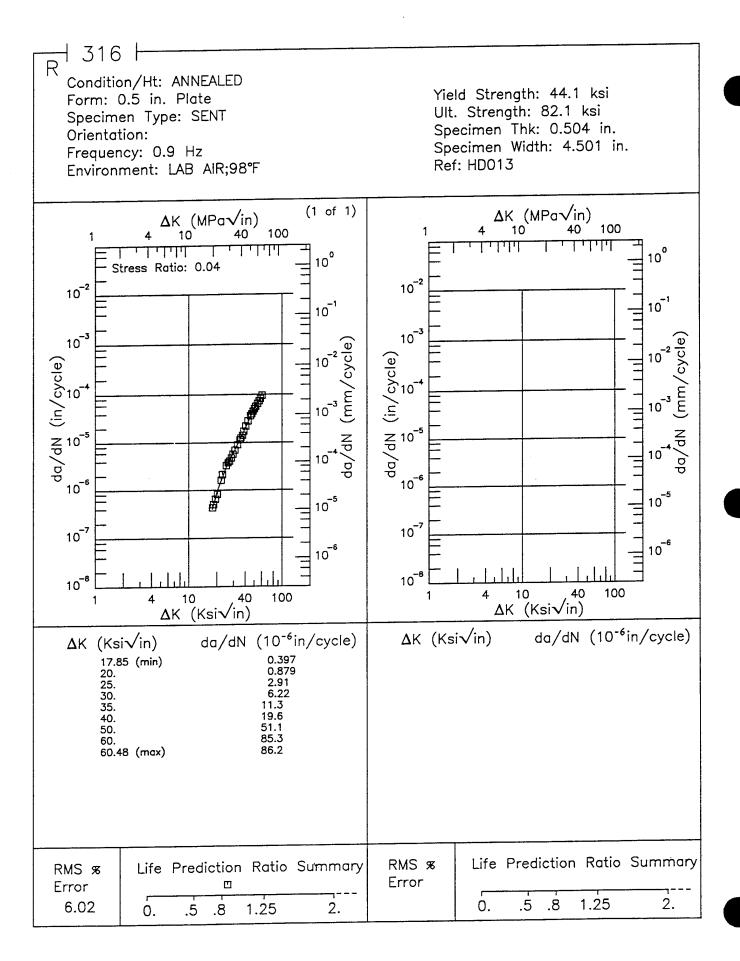


Figure 4.8.3.1.2

1 316 H Condition/Ht: ANNEALED AT 1950F 1HR WQ Form: 0.5 in. Plate Yield Strength: 43 ksi Specimen Type: CT Ult. Strength: 81.5 ksi Specimen Thk: 0.525 in. Orientation: Frequency: 5 Hz Specimen Width: 2.001 in. Ref: HD014 Environment: LAB AIR; RT (1 of 1) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 10 10 100 40 100 40 11111 1 1 1 1 1 1 1 لللبليا 10° 10° Stress Ratio: 0.05 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10-6 10⁻⁶ 10 -5 10 -5 10⁻⁷ 10⁻⁷ 10 6 10 6 10 8 10⁻⁸ 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) **Δ**K (Ksi√in) ΔK (Ksi√in) $da/dN (10^{-6}in/cycle)$ 21.20 (min) 25. 30. 2.84 5.45 11.6 22.8 42.4 46.5 35. 40.78 (max)

Figure 4.8.3.1.3

2.

RMS %

Error

Life Prediction Ratio Summary

1.25

2.

.5 .8

0.

Life Prediction Ratio Summary

1.25

RMS % Error

3.25

0.

.5 .8

TABLE 4.9.1.2

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK 347 AT ROOM TEMPERATURE

ORIENTATION: Unspecified

ENVIRONMENT: Lab Air

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Condition/Ht: .050 IN. FROM CENTERLINE Yield Strength: Form: Weldment Ult. Strength: Specimen Type: CT Specimen Thk: 1 in. Orientation: Specimen Width: 5 in. Frequency: 30 Hz Ref: AM001 Environment: LAB AIR; RT (1 of 1) ΔK (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 10 100 40 100 10 40 100 1 1 1 1 1 1 Stress Ratio: 0.1 10-2 10-2 10 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10 6 10-6 10⁻⁵ 10 -5 10⁻⁷ 10⁻⁷ 10⁻⁶ 10⁻⁶ 10⁻⁸ 10 8 100 10 40 100 10 40 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) Δ K (Ksi \sqrt{in}) da/dN (10⁻⁶in/cycle) 2.70 4.89 36.21 (min) 40. 50. 60. 70. 71.59 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error 2. .5 .8 1.25 0. 12.37 2. 1.25 0. .5 .8

Figure 4.9.3.1.1

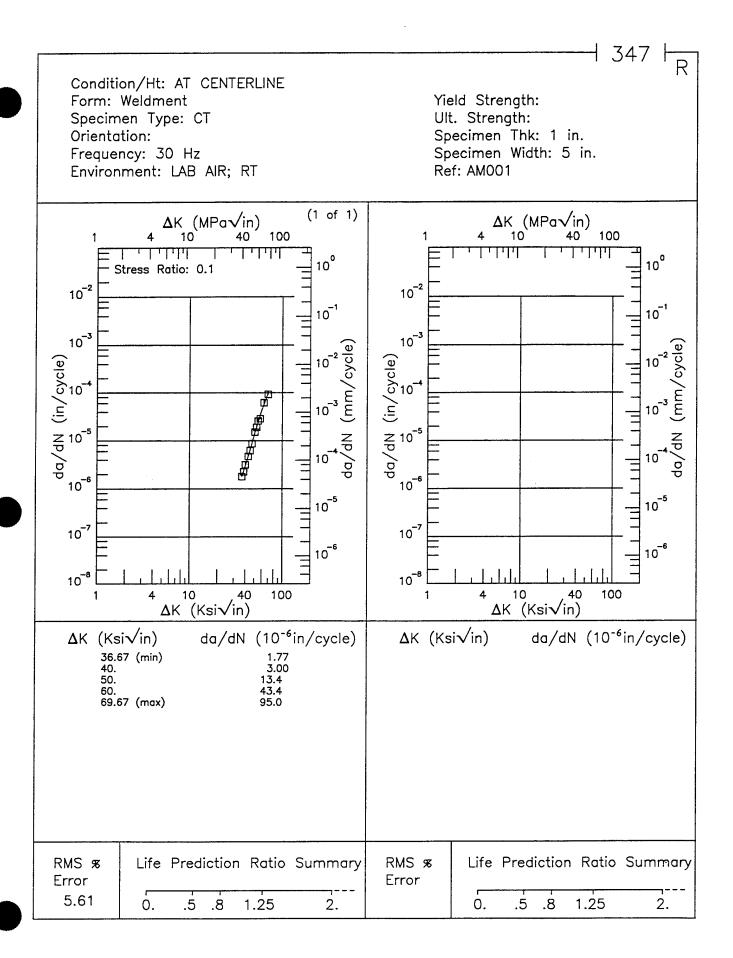


Figure 4.9.3.1.2

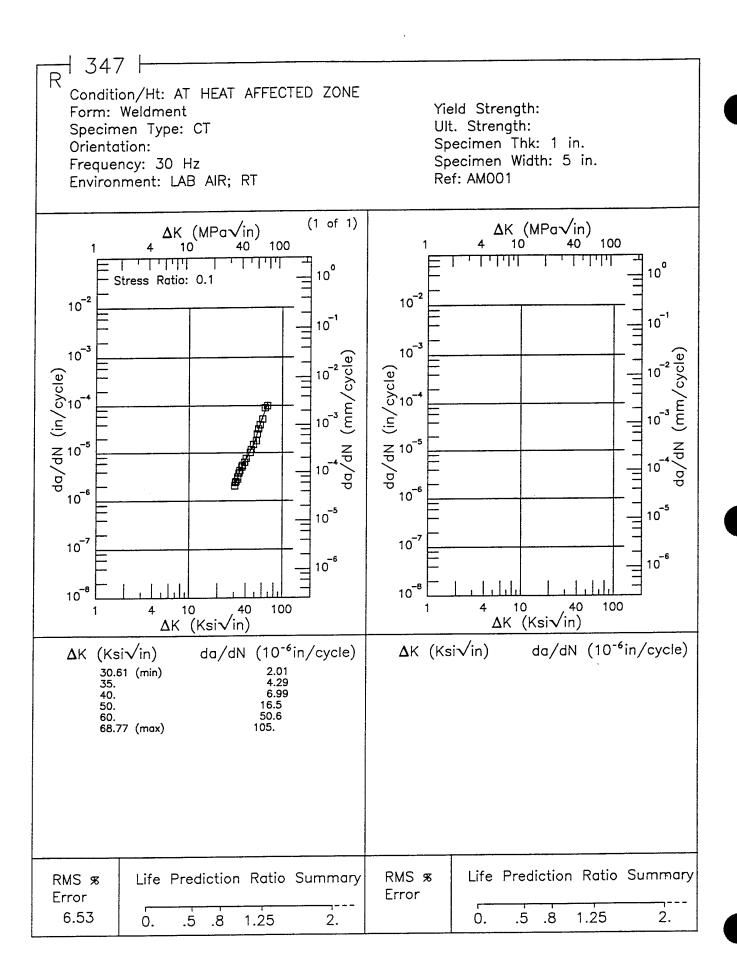


Figure 4.9.3.1.3

TABLE 4.10.3.3

K_{Isco} SUMMARY FOR STAINLESS STEEL AFC 260

7.5.41415.5.4	r.	Test	G. C.			Ŝ	Specimen			5	4	4	Test	·	
Condition Heat Treat	Form	Temp (°F)	Spec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)	Thk (in)	(in)	(Ksivin) (Ksivin)	^{N_{loo}} (Ksi√in)	Time (min)	Test Date	Reference
2200°F 1hr; 1900°F 1hr OQ; -100°F 1hr; -320°F 1hr; 800°F 2+2 hr	Ъ	R.T.	T-T	1	8.5% NaCi	CANT.	1.6	0.48	0.56	i	99	5993	1	1971	80685
2200°F 1hr; 1900°F 1hr OQ; -100°F 1hr; -320°F 1hr; 900°F 2+2 hr	Ъ	R.T.	T-L	196	3.5% NaCl	CANT.	1.5	0.48	0.56	l	47	40	i	1971	80685
2200°F 1hr; 1900°F 1hr OQ; -100°F 1hr; -320°F 1hr; 1000°F 2+2hr	Ъ	R.T.	T-T	206	3.6% NaCl	CANT"	1.5	0.48	99'0			45	i	1971	80685
2200°F 1hr; 1900°F 1hr OQ; -100°F 1hr; -320°F 1hr; 1050°F 2+2hr	ď	R.T.	T-L	185	3.5% NaCl	CANT.	1.5	0.48	0.56	I		37	-	1971	80685

 $^{\circ}$ specimen thickness does not meet minimum requirements of 2.5 $(rac{K_{loo}}{\sigma_{J^p}})^2$

^{*} asterisk in specimen design column indicates that specimens are side-grooved

TABLE 4.11.2.1

STAINLESS STEEL	STAINLESS	STAINLESS S	STAINLESS	TAINLESS S	SSS	E		AFC 77	K _{Io}						
1	PRODUCT	Cr				•	SPECIMEN	7	CRACK			$\mathbf{K}_{\mathbf{Io}}$			
	FORM	THICK (ln.)	TEMP TEMP (°F)	SPEC	YIELD STR (Kal)	WIDTH (In.)	THICK (in.) B	DEBICN	LENGTH (in.) A	(K., TY8)* (in.)	K. (K.ed • √(m.)	K. MRAN	BTAN	DATE	REFER
	Plate	0.56	R.T.	r.	232.0	1.500	0.500	NB	1	90.04	30.00	1		1969	74720 (1)
800F 1HR OQ -100F 0.5HR 700F 2+2HR (FINE GRAIN)	Plate	0.56	R.T.	LT	203.0	1.500	0.500	NB	1	0.15	49.00	1	ı	1969	74720 (1)
1800F 1HR OQ -100F 0.5HR 800F 2+2HR (FINE GRAIN)	Plate	0.66	R.T.	L-I	224.0	1.500	0.600	NB		90:0	31.00	ı	i	1969	74720 (1)
1800F 1HR OQ -100F 1HR 700F 2+2HR	Round Bar	3.00	R.T.	LR	185.0	1.500	0.480	NB	1	0.14	44.00	1	ı	1968	84302 (1)
1800F 1HR OQ -100F 1HR 800F 2+2HR	Round Bar	3.00	R.T.	L-R	213.0	1.500	0.480	SIN.	•	90.0	29.00		ı	1968	84302 (1)
1800F 1HROQ -100F 0.5HR 1000F 2+2HR (COARSE GRAIN)	Plate	0.56	R.T.	LT	173.0	1.500	0.500	NB	1	0.05	25.00	1	1	1969	74720 (1)
1800F 1HROQ -100F 0.5HR 700F 2+2HR (COARSE GRAIN)	Plate	0.56	R.T.	LT	183.0	1.500	0.500	NB	-	0.11	38.00	1	1	1969	74720 (1)
1800F 1HROQ -100F 0.5HR 800F 2+2HR (COARSE GRAIN)	Plate	0.56	R.T.	ГŢ	208.0	1.600	0.500	NB	1	0.06	28.00			1969	74720 (1)
1900F 1HR OQ -100F 1HR 800F 2+2HR	Round Bar	3.00	R.T.	LR	222.0	1.500	0.480	NB	1	0.28	74.00		1	8961	84302 (1)
2000F 1HR OQ ·100F 1HR 800F 2+2HR	Round Bar	3.00	R.T.	LR	207.0	1.500	0.480	NB	1	0.29	70.00	-	1	1969	76136 (1)
2000F 1HR OQ -100F 1HR 900F 2+2HR	Round Bar	3.00	99-	LR	:	1.500	0.480	NB		I	32.00	-	ı	1968	84302 (1)
2000F 1HR OQ -100F 1HR 900F 2+2HR	Round Bar	3.00	R.T.	LR	214.0	1.500	0.480	NB	ı	0.17	66.00	ı	ı	1969	76136 (1)

NOTES: (1) COMPOSITION (WT PERCENT) 0.16C, 0.18Mn; 0.015P, 0.021S, 0.13SI, 0.21Ni, 14.0Cr, 5.02Mo, 13.4Co, 0.23V, 0.04N THESE DATA ARE AVERAGE VALUES

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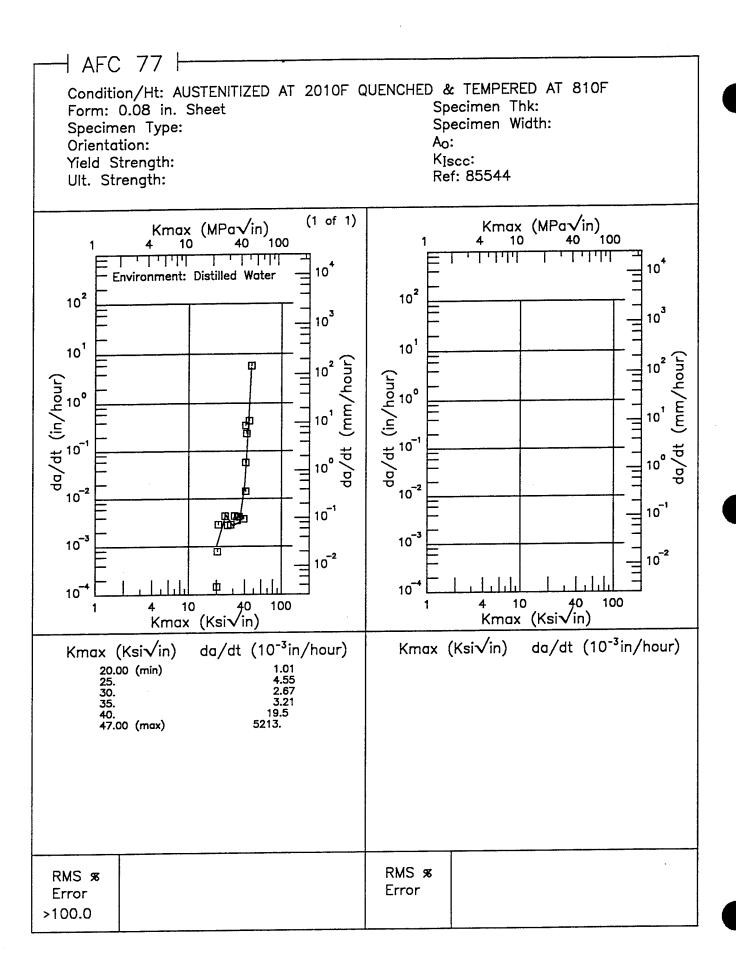


TABLE 4.11.3.3

Kisce SUMMARY FOR STAINLESS STEEL AFC 77

Or. (Ksi) Thick (in) (in) (in) (in) (in) (min) (min) (min) Date 154 3.5% NaCl CANT 1.5 0.48 0.56 119 82" 1569 156 3.5% NaCl CANT 1.5 0.48 0.56 111 97" 1569 173 3.5% NaCl CANT 1.5 0.48 0.56 255 115 1969 173 3.5% NaCl CANT 1.5 0.48 0.56 255 115 1969 169 3.5% NaCl CANT 1.5 0.48 3 200 106* 1969 277 3.5% NaCl CANT 1.5 0.48 3 106 90 1969 277 3.5% NaCl CANT	Prod	Test		Yield	Envir	Sp	Specimen		Prod	- 4	Ka	K _{Isoo}	Test	Test	
154 3.5% NaCl CANT 1.5 0.48 0.56 111 97* 1969 173 3.5% NaCl CANT 1.5 0.48 0.56 232 3.5% NaCl CANT 1.5 0.48 0.56 252 1.5	(°F)	1 E	Or.	(Ksi)		Design	Width (in)	Thick (in)	(in)	(in)	(Ksi√in)	(Ksi√in)	(min)	Date	Reierence
196 3.5% NaCl CANT 1.5 0.48 0.56 111 97* 1969 173 3.5% NaCl CANT 1.5 0.48 0.56 25 115 1969 232 3.5% NaCl CANT 1.5 0.48 3 80 30 1969 252 3.5% NaCl CANT 1.5 0.48 3 80 30 1969 277 3.5% NaCl CANT 1.5 0.48 3 80 30 1969 277 3.5% NaCl CANT 1.5 0.48 3 106 90 1969 277 3.5% NaCl CANT 1.5 0.48 3 106 90 1969 277 3.5% NaCl CANT 1.5 0.48 3 106 90 1969 277 3.5% NaCl CANT 1.5 0.48 3 106 90 1969	R.T.	ľ.	I	154	3.5% NaCl	CANT"	1.6	0.48	99'0		119	82*	i	1969	74720
173 3.5% NaCl CANT 1.5 0.48 0.56 25 15 1969 232 3.5% NaCl CANT 1.5 0.48 9.56 30 >20 1969 169 3.5% NaCl CANT 1.5 0.48 8 80 30 1969 277 3.5% NaCl CANT 1.5 0.48 8 106 90 1969 297 3.5% NaCl CANT 1.5 0.48 8 106 90 1969 297 3.5% NaCl CANT 1.5 0.48 8 106 90 1969	R.T.	ï		196	3.5% NaCl	CANT.	1.5	0.48	0.56	I	111	97+	I	1969	74720
232 3.5% NaCl CANT 1.5 0.48 0.56 30 >20 1969 169 3.5% NaCl CANT 1.5 0.48 3 80 30 1969 252 3.5% NaCl CANT 1.5 0.48 3 80 30 1969 277 3.5% NaCl CANT 1.5 0.48 3 106 90 1969 297 3.5% NaCl CANT 1.5 0.48 3 106 90 1969	R.T.	T.	l	173	3.5% NaCl	CANT	1.5	0.48	990	1	25	15	i	1969	74720
169 3.5% NaCl CANT 1.5 0.48 3 80 105 1969 277 3.5% NaCl CANT 1.5 0.48 3 80 30 1969 277 3.5% NaCl CANT 1.5 0.48 3 107 48 1969	R.	R.T.	!	232	3.5% NaCi	CANT.	1.5	0.48	0.56	ŀ	30	>20	i	1969	74720
	<u>~~</u>	R.T.	<u> </u>	169	3.6% NaCl	CANT.	1.5	0.48	83	i.	200	105*		1969	76136
297 3.5% NaCl CANT 1.5 0.48 3 107 48 1969	<u> </u>	E		252	3.5% NaCl	CANT.	1.5	0.48	အ	I	80	30	1	1969	76136
297 3.5% NaCl CANT 1.5 0.48 3 107 48 1969	ᅺ	i.	i	277	3.5% NaCl	CANT.	1.5	0.48	83		106	06		1969	76136
	<u> </u>	R.T.	i	297	3.5% NaCl	CANT.	1.5	0.48	က	<u> </u>	107	48	l	1969	76136

TABLE 4.11.3.3 (CONCLUDED)

K_{lsce} SUMMARY FOR STAINLESS STEEL AFC 77

	7	Test		Yield		S	Specimen		Prod			1	Test	E	
Condition Heat Treat	Form		opec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)		Crack (in)	Ro (Ksi√in)	^K ino (Ksi√in)	Time (min)	Test Date	Reference
2000°F 1hr OQ; -100°F 0.5Hr; 700°F 2+2 hr	В	R.T.	1	180	3.5% NaCl	CANT	1.5	0.48	3	į.	160	50	:	1969	76136
2000°F 1hr OQ; -100°F 0.5hr; 800°F 2+2 hr	В	R.T.		207	3.5% NaCl	CANT.	1.5	0.48	8	1	0.2	40	ı	1969	76136
2000°F 1hr OQ; -100°F 0.5hr; 900°F 2+2 hr	В	R.T.	••	214	3.5% NaCl	CANT	1.6	0.48	2		99	98	••	6961	76136
2000°F 1hr OQ; -100°F 0.5hr; 1100°F 2+2 hr	В	R.T.	•••	221	3.5% NaCl	CANT.	1.5	0.48	3	:	43	10	:	1969	76136
2000°F 1hr OQ; -100°F 0.5hr; 1400°F 2+2 hr	В	R.T.	1	150	3.5% NaCl	CANT.	1.5	0.48	3		116	801		6961	76136
2100°F 1hr FC to 1900°F hold 1hr OQ	C	Ę	L-T	165.8	3.5% NaCl	NB.	20	0.5	10	0.4	108	>10		1973	87360
-100°F 4hr 500°F 2+2 hr		1.1.	T-L	164.6	3.5% NaCl	NB*	15	0.5	10	0.4	110	>10	•••	1973	87360

* specimen thickness does not meet minimum requirements of 2.5 $(\frac{K_{loc}}{\sigma_{ys}})^2$

^{*} asterisk in specimen design column indicates that specimens are side-grooved

TABLE 4.12.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR STAINLESS STEEL ALLOY AFC 77 (VAR) AT ROOM TEMPERATURE

Product	_				K_{I_G}	$K_{Ic}~(ksi\!\sqrt{in})$	<u>a</u>)			
Form	Condition/Heat Treatment			<i>9</i> 2	Specimen Orientation	n Orie	ıtation			
			L-T			T-L			S-L	
		Mean K _{ic}	Std Dev	E	Mean K _{ie}	Std Dev	Ħ	Mean K _{ie}	Std Dev	u
£	1700F 1HR OQ 2100F 1HR MOVE TO FCE AT 1933F HELD 1HR OQ -100F 24HR 900	48.6	3.1	7	50.8	1.3	7	i	ŀ	:
rorging	2100F 1HR MOVED TO FCE AT 1900F HELD 1HR OQ -100F 4HR 500F 2+2HR	110.5	4.9	2	108	2.9	2	;	ı	i

TABLE 4.12.2.1

			-	STAI	NLESS	STAINLESS STEEL		AFC 77 (VAR)	ir) K _I o						
	PRODUCE					Sci	SPECIMEN	z	CRACK			K _{Io}			
CONDITION	PORM	THICK (in.)	TEST TEMP (°F)	SPEC	YTELD STR (Kel)	WIDTH (in.) W	THICK (in.) B	DESIGN	LENGTH (in.) A	2.6 * (K _{L,} TYS)* (in.)	K. (Kelvin.)	K, MEAN	STAN	DATE	REFER
1700F 1HR OQ 2100F 1HR MOVED TO FCE AT 1933F		6.00	į		210.0	1.002	0.501	NB	0.513	0.10	42.40			1973	87360 (1)
HELD 1HR OQ -100F 24HR 900F 2+2HR	Forging	6.00		L-T	210.0	1.002	0.501	NB	0.510	0.10	41.30	41.9	9.0	1973	87360 (1)
1700F 1HR OQ 2100F 1HR MOVED TO FCE AT 1933F		6.00	;	1	210.0	1.002	0.501	NB	0.523	0.11	43.30			1973	87360 (1)
HELD 1HR OQ · 100F 24HR 900F 2+2HR	Forging	6.00	8	T-L	210.0	1.002	0.501	NB	0.520	91.0	52.40	47.9	6.4	1973	87360 (1)
		6.00			192.0	1.002	0.500	NB	0.520	0.16	47.90			1973	87360 (1)
		90.9			192.0	1.002	0.500	NB	0.507	0.13	44.40			1973	87360 (1)
1700F 1HR OQ 2100F 1HR		6.00			192.0	1.002	0.501	NB	0.527	0.14	45.60			1973	87360 (1)
MOVED TO FCE AT 1933F HELD 1HR OQ -100F 24HR	Forging	9.00	R.T.	L.1	192.0	1.002	0.501	NB	0.523	0.19	53.40	48.6	3.1	1973	87360 (1)
900F 2+2HR		9.00			192.0	1.002	0.501	NB	0.505	0.18	60.80			1973	87360 (1)
		6.00			192.0	1.002	0.500	NB	0.533	0.16	48.80			1973	87360 (1)
		6.00			192.0	1.002	0.501	NB	0.510	0.17	49.60			1973	87360 (1)
		9.00			194.0	1.002	0.501	NB	0.525	0.17	49.90			1973	87360 (1)
		9.00			194.0	1.002	0.501	NB	0.520	0.18	62.60			1973	87360 (1)
1700F 1HR OQ 2100F 1HR		9.00			194.0	1.002	0.601	NB	0.513	0.16	48.80			1973	87360 (1)
MOVED TO FCE AT 1933F HELD 1HR OQ · 100F 24HR	Forging	9.00	R.T.	T-L	194.0	1.002	0.501	NB	0.513	0.18	62.00	£0.8	1.3	1973	87360 (1)
900F 2+2HR		6.00	· •		194.0	1.002	0.501	NB	0.510	0.17	60.70			1973	87360 (1)
		9.00			194.0	1.002	0.601	NB BB	0.515	0.17	50.40			1973	87360 (1)
		6.00			194.0	1.002	0.501	EN RB	0.500	0.17	61.00			1973	87360 (1)

NOTES: (1) COMPOSITION (WT PERCENT) 0.15C, 0.08Mn, 0.012P, 0.004S, 0.20Si, 1.17Ni, 13.7Cr, 5.02Mo, 13.5Co, 0.30V, 0.18Cb, 0.020N

TABLE 4.12.2.1 (CONCLUDED)

				STAI	NLESS	STAINLESS STEEL		AFC 77 (VAR)	IR) K _{Ie}						
	PRO	PRODUCT				oc.	SPECIMEN	z	CRACK			K			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (in.)	THICK (in.) B	DESIGN	LENGTH (in.) A	2.5 • (K _w ,TYS)* (in.)	K. (Kelvin.)		STAN	DATE	REFER
2100F 1HR MOVED TO FCE AT 1900F HELD 1HR OQ -100P 4HR 500P 2+2HR	Forging	6.00	99-	LT	180.0	0.995	0.495	NB	0.477	0.46	77.70	1	!	1973	87360
2100F 1HR MOVED TO FCE AT	i i	6.00	30	Ē	180.0	0.995	0.497	NB NB	0.490	0.35	67.10			1973	87360
-100F 4HR 500F 2+2HR	Forking	6.00	ê	7.	180.0	0.994	0.497	NB	0.533	0.42	73.90	70.5	8.	1973	87360
2100F 1HR MOVED TO FCE AT	Powering	6.00	£	E	165.0	4.000	2.007	CT	2.090	1.19	114.00			1973	87360
-100F 4HR 500F 2+2HR	Surgin 8	9.00		3	165.0	4.000	2.006	CT	2.110	1.05	107.00	110.6	4.9	1973	87360
2100F 1HR MOVED TO FCE AT	Porming	9.00	Đ	Ē	166.0	4.000	2.006	CT	2.070	0.98	104.00			1973	87360
.100F 4HR 500F 2+2HR	99	6.00	:	1-1	166.0	4.000	2.007	cr	2.110	1.14	112.00	108.0	6.7	1973	87360

TABLE 4.13.3.3

Kiece SUMMARY FOR STAINLESS STEEL AM 355

	r G	Test				S	Specimen		Prod				Test		
Condition Heat Treat	Form	Temp (°F)	Spec Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)		Crack (in)	Roi√in)	K _{le∞} (Ksi√in)	Time (min)	Test Date	Refer
MOD SCT1000	В	R.T.	1	163.2	3.5% NaCl	CANT	1.5	840	2.25		117	117*	30000	1971	84333
					20% NaCl	CT	. 2	1	1.13	•	48	8	***	1973	88998
	д	R.T.	T-L	152.5	Industrial Atm	CL	8	1	1.13	•	48	4.5	•••	1973	88888
					Seacoast Atm	\mathbf{CT}	2	1	1.13	;	48	24		1973	88998
SCT 850			i	180	3.5% NaCl	CANT	1.5	0.48	2.25	***	269	92.5	30000	1261	84333
	۶	É			20% NaCl	LO	2	1	2		36.6	9	:	1973	86688
	η	F. I.	T-L	190.3	Industrial Atm	L)	2	1	2	ł	36.6	18	1	1973	88998
-					Seacoast Atm	\mathbf{cr}	2	1	2	•	36.6	18	ł	1973	88998
					20% NaCl	ţ	2	1	1.13		104.7	9.7		1973	86688
	ч	R.T.	T·L	169.7	Industrial Atm	CT	2	1	1.13	-	104.7	99	i	1973	86688
a	,				Sencoust Atm	5	2	-	1.18		104.7	52	1	1973	86688
SCT1000			i	171.2	3.5% NaCl	CANT	1.5	0.48	2.25		88.4	88.4+	30000	1971	84333
	Ļ	£			20% NaCl	CI	2	-	2		70	28	-	1973	86688
	۹	F. I.	T-T	172.4	Industrial Atm	CT	2	1	2	-	70	99	1	1973	86688
					Seacoast Atm	GJ.	2	1	2	1	70	35	-	1973	86688

* specimen thickness does not meet minimum requirements of $2.5~(rac{K_{Loo}}{\sigma_{yr}})^2$

TABLE 4.14.3.3

K_{lscc} SUMMARY FOR STAINLESS STEEL AM 362

Condition/	Dag	Test		Yield		S	Specimen		Prod		;		Tout		
Heat Treat	Form	Temp (°F)	Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)	Thk (in)	Crack (in)	Crack Ko (in) (Ksivin)	K _{lac} (Ksi√in)	Time (min)	Test Date	Reference
H900	В	R.T.	-	200.5	3.5% NaCi	CANT	1.5	0.48	2.25	1	30.2	12.5	42000	1971	84333
H1000	В	R.T.	i	178.9	3.5% NaCl	CANT	1.5	0.48	2.25		40.1	31	36000	1971	84333

K_{lscc} SUMMARY FOR STAINLESS STEEL AM 364

	Refer	84333	84333
E	Test Date	1971	1971
	Time (min)	90009	00009
ŀ	N _{loo} (Ksi√in)	-86	128+
÷	ne Ksi√in	131	128
Č		-	!
Prod	Thk (in)	g	က
1	Thick (in)	0.48	0.48
Specimen	Width (in)	1.5	1.5
3 2	Design	CANT	CANT
	Envir.	3.5% NaCl	3.5% NaCl CANT
Yield	Str (Ksi)	183.3	186.7
ō	Or.	T-L	R.T. T-L 186.7
Test	Temp (°F)	R.T. T-L 183.3	
F	Form	ম	ᄕᅭ
	Condition/ Heat Treat	H850	H950

 $^{+}$ specimen thickness does not meet minimum requirements of $2.5~(rac{K_{Loc}}{\sigma_{yy}})$

1 of 1

TABLE 4.16.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR STAINLESS STEEL ALLOY CUSTOM 455 AT ROOM TEMPERATURE

Product					K_{Ic}	$K_{Ic}~(ksi\sqrt{in})$	<u>1</u>			
Form	Condition/Heat Treatment			S2	pecime	Specimen Orientation	ıtation			
			L-T			T-T			S-L	
		Mean K _{le}	Std Dev	E	Mean K _{le}	Std Dev	п	Mean K _{lo}	Std Dev	5
	1500F 1HR OQ 900F 4HR AC	46.2	3.3	3	:	:	:	i	:	:
rorging	1500F 1HR OQ 950F 4HR AC	72.1	7.8	2	••	;	÷	i	:	:

TABLE 4.16.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK CUSTOM 455 AT ROOM TEMPERATURE

			٥		
			100.0		
	(0)	9	60.0		
Air	FCGR (10 ^d in/cyclo)	ΔK Level (Ksi/in)	20.0 50.0	2.76	3.72
r: Lab	ZR (10	Loval	10.0		
NMEN	FCC	Δĥ	5.0		-
ENVIRONMENT: Lab Air			2.5		
A		FREQ.		10-30	20-30
		R		0.1	0.3
: L-T		PRODUCT		Sitte	FORGING
ORIENTATION: L-T		CONDITION/ HEAT TREATMENT			H1000

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK **CUSTOM 455 AT ROOM TEMPERATURE**

CONDITION/ HEAT TREATMENT	T-L PRODUCT FORM	Ħ	ER FREQ (Hz)	ENVIRONMENT: Lab Air FCGR (10 ⁻⁸ in/c	ENT: Lab Air FCGR (10 ⁻⁶ in/cycle)	d in/cyc	(e)	
H1000	FORGING	0.1	10 20 20-30	6.0	10.0 20.0 11 3.11 2.52	2.62 (M.S.)	26	1 00.00

TABLE 4.16.2.1

				STAIL	STAINLESS STEEL	STEEL	- 1	STOM 4	CUSTOM 455 K _{Ic}						
	PRODUCT					5 2	SPECIMEN	z	CRACK			K _{Io}			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Kal)	WIDTH (in.)	THICK (in.)	DEBIGN	LENGTH (in.) A	2.6 • (K _{to,} TYS)* (in.)	K. (Ksivin.)	K. MEAN	STAN DEV	DATE	REFER
		4.00		_	255.0	1.500	0.480	NB	0.310	60'0	47.70				77934
1500F 1HR OQ 900F 4HR AC	Forging	4.00	R.T.	T-71	265.0	1.500	0.480	NB	0.330	0.09	48.40	46.2	3.3		77934
		4.00			255.0	1.500	0.480	NB	0.320	0.07	42.40			ı	77934
2000		4.00	E	E	246.0	1.500	0.480	NB	0.310	0.25	77.60			i	77934
1500F THK OQ 850F 4HK AC	Forging	4.00	н. Н	<u> </u>	246.0	1.500	0.480	NB NB	0.310	0.18	09'99	72.1	7.8	:	77934

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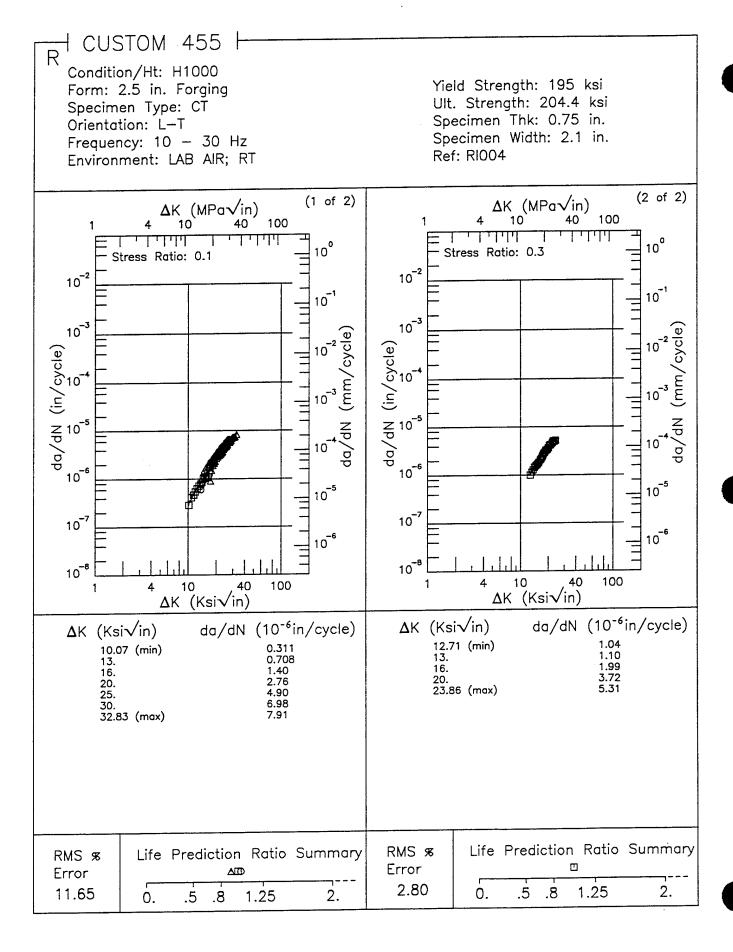


Figure 4.16.3.1.1

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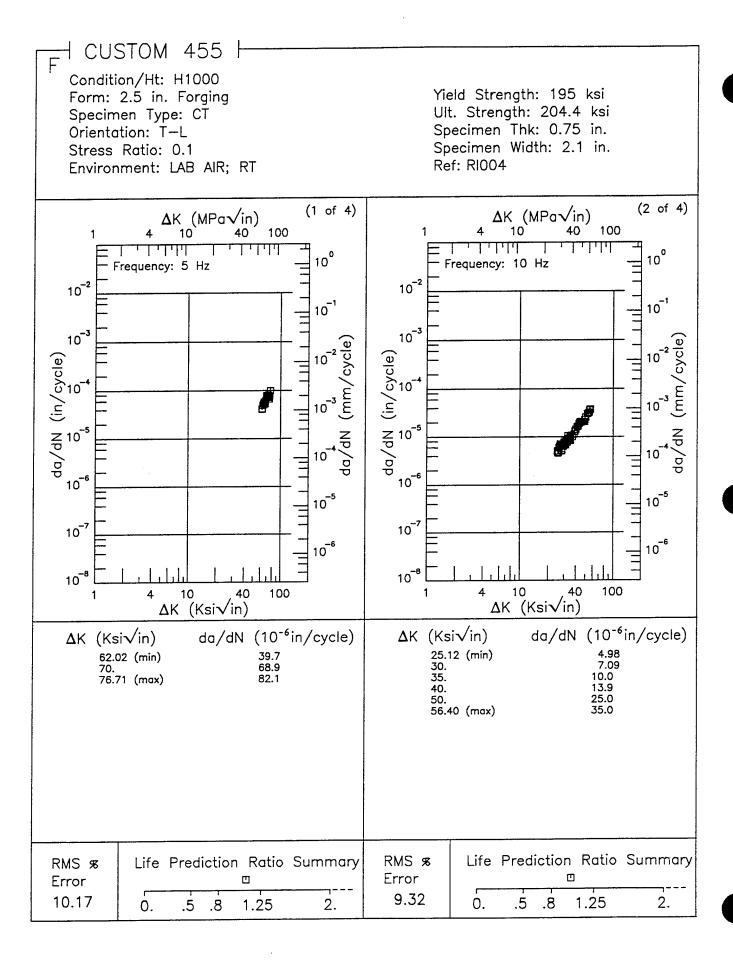


Figure 4.16.3.1.2

Condition/Ht: H1000 Yield Strength: 195 ksi Form: 2.5 in. Forging Ult. Strength: 204.4 ksi Specimen Type: CT Specimen Thk: 0.75 in. Orientation: T-L Specimen Width: 2.1 in. Stress Ratio: 0.1 Environment: LAB AIR; RT Ref: RI004 (4 of 4)(3 of 4) Δ K (MPa \sqrt{in}) **Δ**K (MPa√in) 100 10 100 10 40 40 77777 1 1 1 1 1 1 10⁰ 10° Frequency: 30 Hz Frequency: 20 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ 10 -2 da/dN (in/cycle) da/dN (in/cycle) 10 10⁻⁶ 10-6 10 -5 10 -5 10⁻⁷ 10⁻⁷ 10-6 10 6 10⁻⁸ 10⁻⁸ 40 100 10 10 40 100 ΔK (Ksi√in) ∆K (Ksi√in) da/dN (10⁻⁶in/cycle) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) ΔK (Ksi√in) 0.911 0.772 0.290 12.70 (min) 10.09 (min) 13. 16. 13. 1.03 16. 20. 25. 27.10 (max) 20. 3.11 25. 25.96 (max) 3.80 3.95 Life Prediction Ratio Summary RMS % RMS % Life Prediction Ratio Summary 0 🛚 Error Error 14.13 21.66 0. 1.25 2. 1.25 .5 .8 0. .5 .8 2.

H CUSTOM 455 F

Figure 4.16.3.1.2 (Concluded)

TABLE 4.16.3.3

K_{lsc} SUMMARY FOR STAINLESS STEEL CUSTOM 455

Condition/	Duck	Test	ğ	Yield		S	Specimen		Prod	,	;		Test		
Heat Treat	Form	Temp Or.	Or.	Str (Ksi)	Envir.	Design	Width Thick (in)	Thick (in)	Thk (in)	(in)	Crack Kq K _{lew} (in) (Ksivin) (Ksivin)	K _{less} (Ksivin)	Time (min)	Test Date	Reference
006Н	F	F R.T.		255	35% NaCl	1 CANT	1.5	0.5	4	1	62	- 69	00009	1969	77934
H950	দ	F R.T.	ı	246 3.	3.5% NaCl CANT	CANT	1.5	0.48	4		72.1	72.1	60000	1761	84333

FOR STAINLESS STEEL ALLOY PH13-8Mo AT ROOM TEMPERATURE MEAN PLANE STRAIN FRACTURE TOUGHNESS

					K_{Ic}	$K_{Ic}~(ksi\sqrt{in})$	<u> </u>			
Product										
Form	Condition/Heat Treatment			S	Specimen Orientation	n Orier	ntation			
			L-T			T-T			S-L	
		Mean K _I	Std Dev	Ħ	Mean K _{le}	Std Dev	ď	Mean K _{lo}	Std Dev	ď
3	H950	58.4	6.5	2	69.4	16.1	4	i	:	
Sneet	H1000	105.6	4.8	9	96.2	5.2	4	i	;	;
Plate	H1000	94.7	3.6	3	i		***	:	:	i
	ANNEALED	114.1	15.7	5	9.66	22.4	9	:	;	**
	H960	70.3	16.	9	:	i	•••		:	***
rorging	H1000	101.6	11.	12	88.1	17.1	7	:		***
	H1050	143.3	9.2	3	122.	2.2	2	•••	***	•••
Extrusion	H1000	68.5	5.5	8	66.2	2.1	9	:	1	i
Forged Bar	AUSTENITE COND AND TRANSFORMED AT 38F AGED 1016F	103.	19.4	2	89.6	1.8	2	i		ŀ
	H1000	114.2	0.9	2	122.7	3.	3	•••	•••	•••
	H950	66.9	2.9	3	63.5	1.7	9	74.1	2.1	8
Rolled Bar	H1000	96	7.1	2	75	4.2	2	ı		•••
	H1050	103.1	4.6	3	94.9	7.8	9	92.2	4.2	2

TABLE 4.17.1.2.1

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK PHI3-8Mo AT ROOM TEMPERATURE

ORIENTATION: L-T	L-T		ENVE	SONM	ENT: I	istille	ENVIRONMENT: Distilled Water	¥	
							¥		
					HC	0D <i>H</i>	PCCH (10" incode)	(9)	
CONDITION	PRODUCT	â	FREQ						
HEAT TREATMENT	FORM	4	(Hz)		ΔJ	C Lovel	AK Lovel (Ksk/in)	æ	
			1						
				8.8	0.0	10.0	20.0	99.0	100.0
1080	CATOGOS	0.1	1			0.41	11.67	159.49	
	FONGING	9.0			90.0	1.38	14.47		

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK PH13-8Mo AT ROOM TEMPERATURE

ORIENTATION: L-'	4: L-T		9	ENVIRONMENT: Dry Air	NT: Dry	, Air		
CONDITION/	PRODUCT	î	CHEC	FY	FCGR (10° ⁶ in/cycle)	⁶ II/Cyc	(e)	
HEAT TREATMENT	FORM	K	(HZ)	ν	ΔΚ Level (Ksk/in)	ľ (Kak/ii	(ii	
				2.5 5.0	10.0	20.0	50.0	100.0
		0.08	9			5.82		
		0.08	9			5.82		
	-	0.1	9		0.24	3.08	29.91	
	-	0.1	9		0.24	3.08	29.91	
	C C C C C C C C C C C C C C C C C C C	0.3	9			4.63		
	FORGED BAR	0.3	9		0.58	4.17		
		0.3	9		0.43	4.46		
		0.5	9		0.71	4.93		
OOOTH		0.5	9		0.49	4.36		
200111		0.5	9		0.63	4.52		
	BILLET	90:0	9		0.36	3.97		
		90.0	9		0.38	3.86	34.13	
	EXTRUDED BAR	90.0	9		0.38	3.86	34.13	
		0.5	9		0.84	5.58		
		90.0	1-6		0.3	3.41		
	444 444 1704	90'0	1-6		0.3	3.41		
	ROLLED BAK	0.3	9		0.62	4.39		
		0.5	9		9.0	4.93		
		0.08	9			2.22	20.81	
Unspecified	EXTRUDED BAR	90.0	9			2.22	20.81	
		0.3	9			2.98		

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK PH13-8Mo AT ROOM TEMPERATURE

ENVIRONMENT: H.H.A.

ORIENTATION: L-T

						· ·	,	
CONDITION	PRODICE		Cada	M	FCGR (10° increle)	in/cyc	le)	
HEAT TREATMENT	FORM	æ	(HZ)	7	AK Lovel (Ksi/in)	(Ksk/i	(0	
				2.5 5.0	10.0	20.0	50.0	100.0
		0.1	1		0.36	8.11	102.77	
		0.1	1		0.36	8.11	102.77	
COCKETE	מיים ממטמטמ	0.3	1		0.82	11.3	129.3	
HIGGO	FORGED BAR	0.3	1		0.8	10.77	123.85	
		0.5	1		0.93	13.34		
		0.5	1		0.91	12.96		

TABLE 4.17.1.2.4

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK PH13-8Mo AT ROOM TEMPERATURE

ORIENTATION: L-T

ORIENTATION: L-1	V: L-T		H	NVIR) NIME	ENVIRONMENT: Lab Air	Air		
CONDITION	PRODITOT		Odda		FC	CR (10	FCGR (10 ⁴ in/cycle)	le)	
HEAT TREATMENT	FORM	Ħ	(HZ)		A.	K Love	AK Level (Kst/in)	(1)	
				8.8	8.0	10.0	20.0	50.0	100
HIOOD	FORGING	0.1	6-10				5.7	30.78	127.33
000	BAR	0.02	10					31.58	
		-1	ŭ			0.31	3.31	26.63	
		0.1	ъ			0.36	3.64	28.08	
		0.1	20				3.5	24.45	183.59
H1050	FORGING	4.0	10		90'0	0.56	4.82		
		0.4	20		0.05	0.53	4.28	31.08	
		9.4	6-20		0.06	0.53	4.55	32.68	
		9.0	15-30		0.1	68'0	5.33	,	

TABLE 4.17.1.2.5

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK PH13-8Mo AT ROOM TEMPERATURE

	6 in/cycle) (Ksi/in) 20.0 100.0	60.89
.S.	FCGR (10 ⁻⁶ in/cycle) AK Level (Ksk/in)	5.26
ENVIRONMENT: S.C.S.	(GR (10)	
ONME	FC A.	
ENVIR	2.5	
-	FREQ (Hz)	T
	R	90.0
: L-T	PRODUCT	ROLLED BAR
ORIENTATION: L-	CONDITION/ HEAT TREATMENT	H1000

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK PHIS-8Mo AT ROOM TEMPERATURE

100.0 60.0 65.46 PCGR (10 fin/cycle) ΔK Level (Ksiγin) 9.08 9.07 ENVIRONMENT: S.S.W. 10.0 9 90 61 FREQ (Hz) 1.10 × 0.1 PRODUCT FORM FORGING ORIENTATION: L-T HEAT TREATMENT CONDIMON H1000

TABLE 4.17.1.2.7

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK PH13-8Mo AT ROOM TEMPERATURE

ORIENTATION: L-T

ENVIRONMENT: S.T.W.

					Ç	שמש	(*)***********************************	40	
MONTHUMO	DDAMEGE		Cada		7.5	741 (10		Đ	
HEAT TREATMENT	FORM	R	(Hz)		Δ.	I Lovel	AK Lovel (Ksi/in)		
				2.3	6.0	001	20.0	60.0	100.0
	EXTRUDED BAR	0.08	1			0.64	7.11		
		0.08	0.1				6.44		
H1000	1	0.08	1				4.2		
	ROLLED BAR	0.08	1				4.08		
		0.3	1			0.58	11.86		
Unspecified	EXTRUDED BAR	0.08	1				2.69		

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK PHIS-8Mo AT ROOM TEMPERATURE

ORIENTATION: T-L

ENVIRONMENT: Distilled Water

		100.0			
(op	E	50.0	136.09	136.09	
d in/cyt	(Ksh/i	20.0	19.74	19.74	13.82
FCGR (10 ⁻⁸ in/cycle)	AK Lavel (Ksk/in)	10.0	9.0	0.8	1.26
FC	V	0'9	90.0	90.0	90.0
		2.5			
	FREQ (Hz)		1	1	-
	Ħ		0.1	0.1	9.0
	PRODUCT FORM			FORGING	
	CONDITION/ HEAT TREATMENT			H1050	

TABLE 4.17.1.2.9

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK PHIS-8Mo AT ROOM TEMPERATURE

ORIENTATION: T-L	: T-L		3	ENVIRONMENT: Dry Air	MENT	: Dry	Air		
NOLLIGNOD	PRODUCT	1	FRED		FCG	R (10°	FCGR (10 ⁻⁸ in/cycle)	(9)	
HEAT TREATMENT	FORM	¥	(Hz)		ΔK	Lovei	ΔK Lovel (KstVin)	1)	
				2.5	5.0	0.01	20.0	50.0	100.0
		0.1	9			0.24	3.12	24.51	
		0.1	8			0.24	3.12	24.51	
	ROBCED BAB	0.3	9			0.45	4.07	36.4	
	FORGED DAN	0.3	9			0.45	4.05	36.63	
H1000		0.5	9			0.51	4.56		
		0.5	8			0.51	4.56		
	BILLET	0.08	8			0.37	3.66	30.7	
	n va tan ba	0.08	8				4.05		
	NOLLED BAR	0.08	9				4.05		

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK PH13-8Mo AT ROOM TEMPERATURE

ORIENTATION: T.L

ENVIRONMENT: H.H.A.

		100.0						
(0))	66.0	109.06	109.06	215.14	215.14	578.58	568.44
FCGR (10 ⁻⁸ in/cycle)	ΔK Level (Ksk/in)	20.0	6.49	6.49	9.62	8.62	11.52	12.45
<i>GR</i> (10	K Lovel	10.0			0.63	0.63	1.15	1.08
J.	Δ.	5.0						
		2.5						
FREG	(Hz)		1	1	1	1	1	1
1	#		0.1	0.1	0.3	0.3	0.5	0.5
PRODUCT	FORM				a va dayada	FONGED BAN		
CONDITION/	HEAT TREATMENT				n 1990	00011		

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK PHIS-8Mo AT ROOM TEMPERATURE

ORIENTATION: T-L

ENVIRONMENT: Lab Air

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR AK PH13-8Mo AT ROOM TEMPERATURE

ENVIRONMENT: S.S.W.

ORIENTATION: T-L

100.0 385.3 98 67.86 FCGR (10 tin/cycle) ΔK Lovel (Ksivin) 20.0 8.51 10.0 9 9 80 84 FREQ (Hz) 1-10 × 0.1 PRODUCT FORM FORGING HEAT TREATMENT CONDITION H1000

TABLE 4.17.1.2.13

FATIGUE CRACK GROWTH RATE AT DEFINED LEVELS OF STRESS INTENSITY FACTOR ΔK PH13-8Mo AT ROOM TEMPERATURE

ENVIRONMENT: S.T.W.	FCGR (10 ⁻⁸ in/cycle) AK Lavel (Kst/in) AK Lavel (Kst/in) 25.0 55.0	19.2	0.3
ENA	R FREQ	0.08	0.08
. T-L	PRODUCT	FORGED BAR	ROLLED BAR
ORIENTATION: T-L	CONDITION/ HEAT TREATMENT	COOLE	000111

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				S	STAINLESS STEEL	SS STE		PH13-8MO	K _{Io}						
	PRODUCT	JCT					SPECIMEN	7	CRACK			K _I °			
CONDITION	FORM	THICK (in.)	TEMP (°F)	SPRC OR	YIELD STR (Kel)	WIDTH (in.)	THICK (in.)	DESIGN	LENGTH (in.) A	E.D. (K.,TYS)* (In.)	R. (Ked • √in.)	K. MEAN	STAN DRV	DATE	REFER
		3.00	-		200.7	4.000	2.003	cr	2.043	0.62	92.12			1976	NC001
		3.00			200.7	3.998	2.003	CT	2.073	99.0	103.80			1976	NC001
ANNEALED	Forging	3.00	R.T.	1.7	200.7	3.997	1.996	СT	2.058	1.02	128.41	114.1	16.7	1976	NC001
		3.00			206.0	2.000	1.007	СТ	1.026	0.94	126.90			1976	NC001
		3.00			206.0	4.000	1.999	CT	2.057	0.83	119.40			9/61	NC001
		3.00		············	202.0	3.999	1.996	СТ	2.060	0.43	83.91			9261	NC001
		3.00			202.0	3.999	1.998	cr	2.061	0.73	109.27			9/61	NC001
		3.00	E		202.0	4.000	2.003	CT	2.035	1.08	132.91			1976	NC001
ANNEALED	Forging	3.00	H H		205.0	2.000	1.007	CT	1.025	0.76	113.50	9.66	22.4	9261	1002N
		3.00			207.0	3.938	2.002	cr	2.008	0.36	79.44			1976	100DN
		3.00			214.0	2.000	1.004	CT	1.005	0.33	78.36			1976	NC001
AUSTENITE COND		2.20			212.0	2.999	1.635	cT	1.677	0.78	116.70			1973	98838
AND IKANSPORMED AT 38F AGED 1015F	Forged Bar	2.20	K.T.	1.51	212.0	3.001	1.626	CT	1.597	0.44	89.20	103.0	19.4	1973	85836
AUSTENITE COND	:	2.20	į		212.0	3.001	1.628	CT	1.604	0.46	90.80			1973	85836
AT 38F AGED 1016F	Forged Bar	2.20	K.T.	7.	212.0	3.001	1.634	CT	1.587	0.43	88.30	89.6	1.8	1973	96838
	ī	1.50	Ę		210.0	2.000	1.000	CT	1.000	0.22	63.00			1972	84365
11 apo	Sheet	1.50	K.T.	17.	210.0	2.000	1.000	CT	1.000	0.16	53.80	58.4	6.5	1972	84365
		1.00			210.0	i	1	NB	1	0.38	81.60			1972	84365
1	į	2.25	i i	į	210.0	ì	!	NB	1	0.41	85.00			1972	84365
096 H	Sheet	1.50	K.T.		210.0	2.000	1.000	CT	1.000	0.18	66.70	69.4	16.1	1972	84365
		1.60			210.0	2.000	1.000	CT	1.000	0.17	64.30			1972	84365

TABLE 4.17.2.1 (CONTINUED)

					STAINLESS STEEL	SS STE		PH13-8MO	K _{Io}						
	PRODUCT	JCT				9	SPECIMEN	,	CRACK			⊼ ₁			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F.)	SPEC OR	YIELD STR (Kel)	WIDTH (In.)	THICK (la.) B	DESIGN	LENGTH (in.) A	(K.,TYS)*	K K K	K. MBAN	BTAN DEV	DATE	REFER
		4.00			210.0		1	NB	1	0.39	83.60			1972	84365
		8.00			210.0	2.000	1.000	Ţ	1.000	0.13	47.00			1972	84365
****		8.00			210.0	2.000	1.000	CT	1.000	0.19	67.80			1972	84365
		4.00		1	210.0	1	1	NB	1	0.18	55.90			1972	84365
Н 950	Forging	8.00	R.T.	7	210.0	2.000	1.000	cr	1.000	0.19	58.20	70.3	16.0	1972	84365
		4.00			210.0	'	i	NB	***	0.40	84.50	!		1972	84365
		4.00		_	210.0	ı	ı	NB		0.40	83.90			1972	84365
		4.00			210.0	I	i	NB	-	82:0	70.50			1972	84365
		4.00			210.0	2.000	1.000	CT	1.000	25'0	91.30			1972	84365
		2.25			202.0	2.000	1.000	CT	1.069	06:0	70.00			1973	86688
Н 950	Rolled Bar	2.25	R.T.	7.	202.0	2.000	1.000	C.	1.040	0.27	66.40	699	2.9	1973	86688
		2.25			202.0	2.000	1.000	cT	1.077	0.25	64.20			1973	86688
		2.26			197.0	2.000	1.000	СŢ	1.060	0.24	06'09			1973	86688
		2.25		•	197.0	2.000	1.000	CT	1.030	0.26	00'19			1973	86688
99	Dollad Box	2.25	£	Ē	197.0	4.000	2.000	сT	2.028	92.0	02.99			1973	86688
	IBCT POLICE	2.25	į		197.0	4.000	2.000	CT	2.071	0.28	09'69	63.5	1.7	1973	88998
		2.26			197.0	2.000	1.000	CT	1.049	0.25	08.29			1973	88998
		2.25			197.0	4.000	2.000	CT	1.996	0.28	63.40	,		1973	88998
		2.25			203.0	1.500	0.750	CT	0.797	0.32	72.20			1973	88998
H 960	Rolled Bar	2.25	R.T.	3.1	203.0	1.500	0.750	CT	0.780	0.33	73.80	74.1	2.1	1973	86688
		2.25			203.0	1.500	0.750	CT	0.738	96:0	78.40		.	1973	88998

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				SO	FAINLE	STAINLESS STEEL		PH13-8MO	K _{lo}						
	PRODUCT	JCT				Ø2	SPECIMEN	7	CRACK			K _{Io}			
CONDITION	FORM	THICK (in.)	TEBT TEMP (°F)	SPEC	YIELD STR (Kel)	WIDTH (in.) W	THICK (in.) B	DEBIGN	LENGTH (in.) A	(K, TY8)* (in.)	K. (Kei *	K. MEAN	STAN DEV	DATE	REFER
		1.50		1	205.0	2.000	1.000	CT	1.000	0.58	98.50			1972	84365
		1.50		1	205.0	2.000	1.000	ţ	1.000	0.71	109.00			1972	84365
	į	2.25	ē	I	211.0	ı	·	NB	1	0.59	103.00			2261	84365
Maria	198010	2.26	1	I	211.0	ı	ī	NB	1	0.68	110.00	105.6	4.8	2261	84365
		2.25			211.0	2.000	1.000	CT	1.000	09:0	103.00			1972	84365
		1.75			219.0	I	i	CT	1	0.63	110.00			1972	84365
		1.50			205.0	2.000	1.000	CT	1.000	0.59	99.70			1972	84365
90011	ā	1.50	E		205.0	2.000	1.000	cr	1.000	0.61	101.00			1972	84365
O COLOR	198uc	2.25		1 1	213.0	2.000	1.000	cr	1.000	0.49	94.30	86.2	6.2	2261	84365
		2.25			214.0	2.000	1.000	CT	1.000	0.44	89.60			1972	84365
		4.00		1	201.0	3.501	0.978	cr	1.768	0.55	94.90			ï	84306
H1000	Plate	4.00	R.T.	5	201.0	3.501	0.990	CT	1.761	0.69	98.10	94.7	3.6	:	84306
		4.00			201.0	3.501	0.994	cr	1.782	0.51	91.00				84306
H1000	Plate	4.00	R.T.	T-L	198.0	3.500	0.990	cr	1.796	0.54	93.40	i	1		84306
VVV I	ß	4.00	ě	E	185.0	3.994	1.381	CT	1.941	0.21	63.80			1973	85836
MOM	Lorging	5.00	3	5	195.0	2.000	1.000	CT	1.030	0.14	46.90	50.4	4.9	1973	96838
	f	2.25	į	Ė	215.0	3.000	1.630	CT	i	0.15	63.00			1974	11008
nion	Surfing	4.00	ş	3	215.0	3.000	1.630	CT	i	0.17	56.00	64.5	2.1	1974	11006
		8.00		1	205.0	2.493	1.261	CT	1.188	0.58	98.60			1974	88136
		8.00		1	205.0	1.000	2.000	CT	1.000	99'0	97.30			1973	86034
H1000	Forging	8.00	R.T.		205.0	2.495	1.258	CT	1.232	0.65	104.60	101.6	11.0	1974	88136
	,	4.00			205.0	1.000	2.000	82	1.000	0.69	108.00			1972	84365
		8.00			205.0	2.497	1.259	ದ	1.226	0.59	99.50			1974	88136

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	1	æ					Π																
		REFER	85034	84365	86034	85034	86836	85836	85836	85857	85857	85857	86857	85034	86034	85034	86836	90011	90011	90011	90011	90011	90011
		DATE	1973	1972	1973	1973	1973	1973	1973	1973	1973	1973	1973	1973	1973	1973	1973	1974	1974	1974	1974	1974	1974
		BTAN DEV				Cont'd							17.1				1		2.0			1.2	
	K _{Ie}	K. MEAN				Cont'd							88.1				i		200			48.7	
		K. (Kei * \in)	85.10	131.00	100.00	99.40	99.80	104.00	91.70	73.00	79.50	78.20	75.60	98.50	90.70	121.00	86.40	60.00	62.00	48.00	50.00	48.00	48.00
		(KTY8)* (in.)	0.43	1.00	0.67	99.0	99.0	09.0	0.47	0.34	0.43	0.39	0.37	0.61	0.51	0.87	0.46	0.13	0.15	0.12	0.13	0.12	0.12
K _{to}	CRACK	LENGTH (in.) A	1.000	1.000	0.986	0.988	1.000	1.000	1.000	0.890	1.008	1.002	1.013	986.0	0.982	1.000	1.499	ı	1	1	1	1	1
PH13-8MO	7	DESIGN	CT	NB	لا	CT	CI	CT	CT	CT	cT	CT	CT	CT	CT	CT	СT	СТ	CT	cr	СŢ	cr	CT
	SPECIMEN	THICK (in.) B	2.000	2.000	0.763	0.751	2.000	2.000	2.000	0.751	0.752	0.750	0.750	0.752	0.752	2.000	1.368	1.000	1.000	1.000	1.000	1.000	1.000
STAINLESS STEEL	· 62	WIDTH (fn.)	1.000	1.000	1.998	1.997	1.000	1.000	1.000	2.003	2.002	2.003	2.004	2.001	1.999	1.000	3.002	3.000	3.000	3.000	3.000	3.000	3.000
FAINLE		YIELD STR (Kel)	205.0	205.0	209.0	210.0	211.0	212.0	212.0	196.0	196.0	196.0	196.0	199.0	201.0	205.0	202.0	215.0	215.0	215.0	215.0	215.0	215.0
Σά		SPEC OR	1	1		Cont'd	1						12				8-T		7.			. II.	
		TEST TEMP (°P)				R.T. Cont'd							R.T.				R.T.		3 9			ş	
	Į.	THICK (in.)	8.00	4.00	6.00	6.00	4.00	4.00	4.00	2.76	2.75	2.75	2.75	6.00	6.00	8.00	4.00	1.50	1.50	1.50	1.60	1.50	1.50
	PRODUCT	FORM	I			Forging Cont'd	L						Forging	_	· · · ·		Forging		Extrusion			Extrusion	
		CONDITION				H1000 Cont'd							H1000				H1000		H1000			H1000	

TABLE 4.17.2.1 (CONTINUED)

				Ω	STAINLESS	SS STEEL		PH13-8MO	K _{Io}						
	PRODUCT	JCT				9	SPECIMEN	7	CRACK			K _I °			
CONDITION	FORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIELD STR (Ket)	WIDTH (In.)	THICK (in.) B	DESIGN	LENGTH (in.) A	(K _{to} /TYS) ² (in.)	K. (Kei •	K. MEAN	BTAN	DATE	REFER
		1.50		I	208.0	3.000	1.000	СŢ	1	0.29	71.00			1974	11006
		1.50		!	208.0	3.999	1.417	cr	2.018	0.34	76.70			1973	85836
		1.50			208.0	3.000	1.000	cr	ï	0.28	70.00			1974	11006
500	F	1.50	Ę	1	208.0	3.000	1.000	cr		0.25	66.00			1974	11006
00010	Lextrusion	1.50	 :	<u> </u>	208.0	3.999	1.413	cr	1.973	0.30	72.20	68.5	19.	1973	85836
		1.50			208.0	3.000	1.000	cr	:	0.21	61.00			1974	11006
		1.50			208.0	3.000	1.000	CT	:	0.21	61.00			1974	90011
		1.50			208.0	3.000	1.000	ст	i	0.28	70.00			1974	90011
		1.60			208.0	3.000	1.000	СТ	1	0.22	62.00			1974	11006
		1.50			208.0	3.000	1.000	CT	:	0.26	67.00			1974	90011
		1.50	į.		208.0	3.000	1.000	cr	1	0.26	67.00			1974	90011
H1000	Extrusion	1.50	H.H.		208.0	3.000	1.000	CT	1	0.26	67.00	66.2	2.	1974	90011
		1.50			208.0	3.000	1.000	СТ	1	0.25	66.00			1974	11006
		1.50			208.0	3.000	1.000	CT	1	0.27	68.00			1974	90011
H1000	Forged Bar	4.00	88	LT	210.0	2.006	0.998	CT	1.028	0.14	48.90	I	ı	1973	85836
		1.00	ļ		215.0	2.006	1.000	CT	1.062	0.69	113.50			8261	600GD
H1000	Forged Bar	1.00	K.T.	3	215.0	2.004	1.000	CT	1.051	0.71	114.80	114.2	6.0	1978	GD009
		1.00			216.0	2.005	1.001	CT	1.058	0.82	124.00			1978	GD009
H1000	Forged Bar	1.00	R.T.	T:L	216.0	2.003	1.001	CT	1.034	0.83	124.80	122.7	3.0	1978	GD009
		1.00			216.0	2.004	1.005	СŢ	1.048	0.76	119.30			1978	GD009
	:	1.50	É		205.0	3.000	1.000	ÇĪ	Ī	0.43	85.00			1974	90011
H1000	Rolled Bar	1.60	K.T.	1.1	205.0	3.000	1.000	CT	:	0.54	95.00	90.0	7.1	1974	90011

TABLE 4.17.2.1 (CONTINUED)

				Š	STAINLESS	SS STEEL		PH13-8MO	K,						
	PRODUCT	JCT				8	SPECIMEN	-	CRACK			K			
CONDITION	FORM	THICK (in.)	TEST TEMP (°P)	SPEC	YIELD STR (Kel)	WIDTH (in.)	THICK (in.) B	DESIGN	LENGTH (in.) A	(K, TYB)* (in.)	K. (Kel •	K. MEAN	FTAN	DATE	REFER
With	יים דיונים	1.50	E	l	205.0	3.000	1.000	CT	1	0.31	72.00			1974	90011
OWIH	Kolled Bar	1.60			205.0	3.000	1.000	CT	-	96'0	78.00	75.0	4.2	1974	90011
H1025	Sheet	5.00	R.T.	L-T	200.0	1	i	NB	ı	0.44	84.30	i	ï	1972	84365
		1.50		1	194.7	3.008	1.503	CT	1.537	0.44	81.80			1987	DA006
H1050	Forging	1.50	99	5	194.7	3.009	1.504	CT	1.540	0.42	80.20	78.3	8.	1987	DA006
		3.00			206.9	2.000	0.998	cT	1.021	0.31	72.80			1987	DA007
		1.60		1	193.6	3.006	1.500	cr	1.550	0.38	75.40			1987	DA006
H1050	Forging	1.50	99	<u>-</u>	193.6	3.009	1.503	CT	1.663	0.39	76.50	72.4	6.1	1987	DA006
		3.00			206.8	2.000	0.998	CT	1.024	0.25	65.40			1987	DA007
		2.00			185.4	4.006	1.997	CT	2.100	1.70	152.90			1987	DA006
H1050	Forging	3.00	R.T.	7	196.6	4.009	2.000	CT	2.241	1.31	142.30	143.3	9.5	1987	DA007
		3.00			196.5	4.008	2.001	CT	2.221	1.17	134.60			1987	DA007
	į.	3.00	E		196.9	4.005	2.001	CT	2.198	0.83	120.40			1987	DA007
MUDDO	rorging	3.00	.i	7.	196.9	4.007	2.001	cr	2.246	0.98	123.50	122.0	2.2	1987	DA007
		2.26		1	172.0	2.000	1.000	CT	1.034	0.97	107.30			1973	86688
H1050	Rolled Bar	2.26	R.T.	፤	172.0	2.000	1.000	CT	1.018	0.81	98.20	103.1	9.4	1973	86688
		2.25			172.0	2.000	1.000	CT	1.019	0.91	103.90			1973	86998
		2.25			178.0	4.000	2.000	cr	2.091	0.81	101.40			1973	86688
		2.25			178.0	2.000	1.000	CT	1.032	0.59	86.30			1973	86688
South	of Letter	2.25	E	Ē	178.0	2.000	1.000	CT	1.030	0.61	88.10			1973	86688
	TROT BOILON	2.26	į		178.0	4.000	2.000	CT	2.104	0.82	102.10	94.9	7.8	1973	86688
		2.26			178.0	4.000	2.000	CT	2.105	0.82	102.30			1973	88998
		2.25			178.0	2.000	1.000	СT	1.028	0.62	98.90			1973	88998

				52	TAINLE	STAINLESS STEEL		PH13-8MO	K _{lo}						
	PRODUCT	ıcr					SPECIMEN	״	CRACK			K			
CONDITION	FORM	THICK (la.)	TEMP TEMP (°F)	SPEC	YTRLD STR (Kal)	WIDTH (in.) W	THICK (ia.) B	DESIGN	LENGTH (in.)	(fn.)	% K (a) • (a)	K. MRAN	BTAN	DATE	REFER
Cach	1100	2.25	E	,	176.0	1.500	0.750	СТ	0.762	0.64	89.20			1973	86688
000111	rolled Dar	2.25	R. I.	7.F	176.0	1.500	0.750	CT	0.781	0.73	95.20	82.2	4.2	1973	86688
MILL 1700F LAB 1060F 4HR	Forging	5.00	-66	LT	195.0	2.996	1.500	CT	1.546	0.41	78.80	1	ı	1973	85836
MILL 1700F LAB 1600F 1000F 4 HR	Forging	6.00	-66	LT	195.0	2.008	1.000	CT	1.060	0:30	67.60	ı	ı	1973	85836
MILL 1700F LAB 1500F 1000F 4 HR	Forging	5.00	-65	LT	195.0	2.006	0.999	CT	1.062	16:0	72.50	1	;	1973	85836
		1.50			210.0	1.000	0.500	CT		0.18	67.00			1974	90011
ozo ma	2000	1.60	E	F	210.0	1.000	0.500	CT	1	0.20	69.00			1974	90011
	Teorina Date	1.60	į	<u> </u>	210.0	1.000	0.500	CT	1	0.21	61.00	6.63	2.2	1974	11006
		1.50			210.0	1.000	0.600	CT	1	0.22	62.00			1974	11006
		1.60			207.0	1.000	0.500	CT	ì	0.25	90.99			1974	90011
RH 976	Rolled Bar	1.60	R.T.	r.	207.0	1.000	0.600	Ç	ï	0.34	76.00	70.0	65	1974	11006
		1.50			207.0	1.000	0.500	CT	i	06'0	68.00			1974	90011
RH1000	Rolled Bar	1.50	R.T.	LR	205.0	1.000	0.500	cr	:	0.64	95.00	ı	1	1974	90011

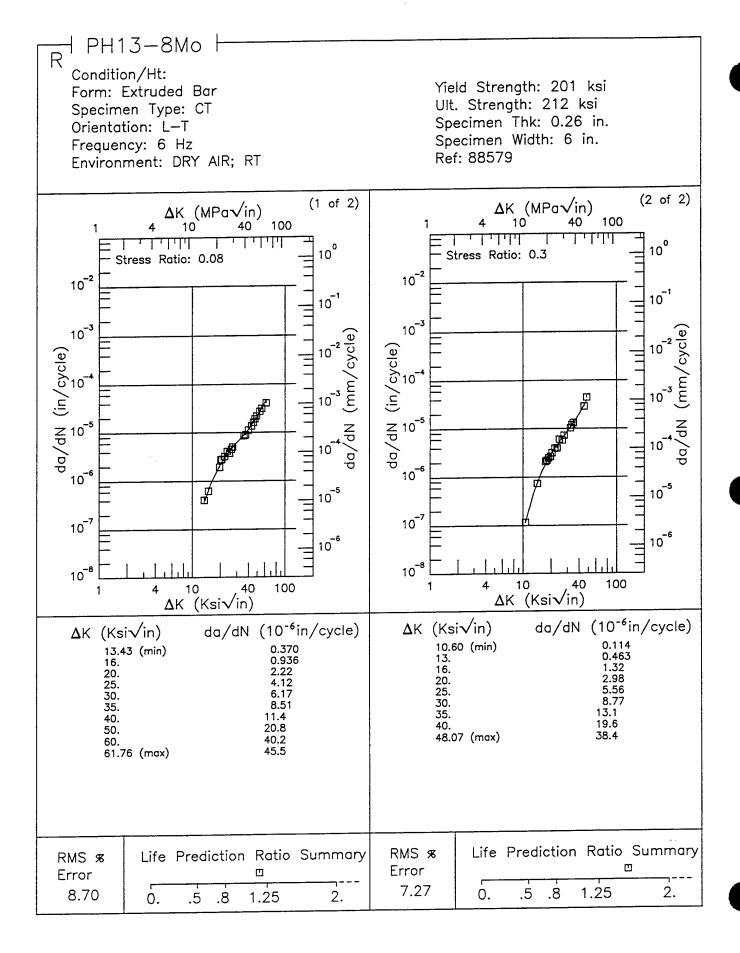


Figure 4.17.3.1.1

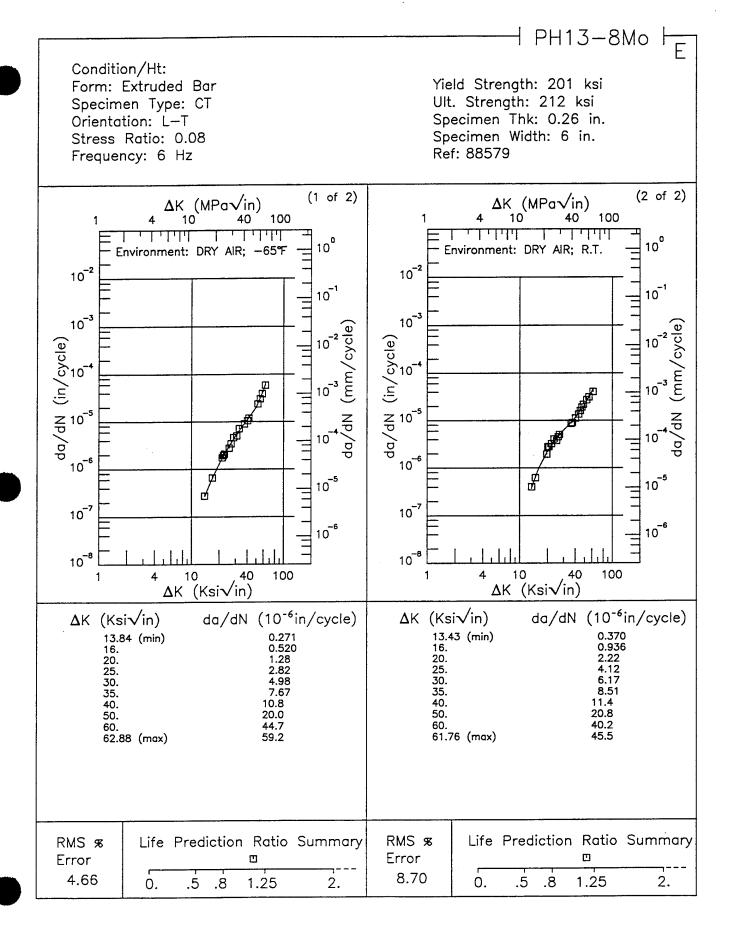


Figure 4.17.3.1.2

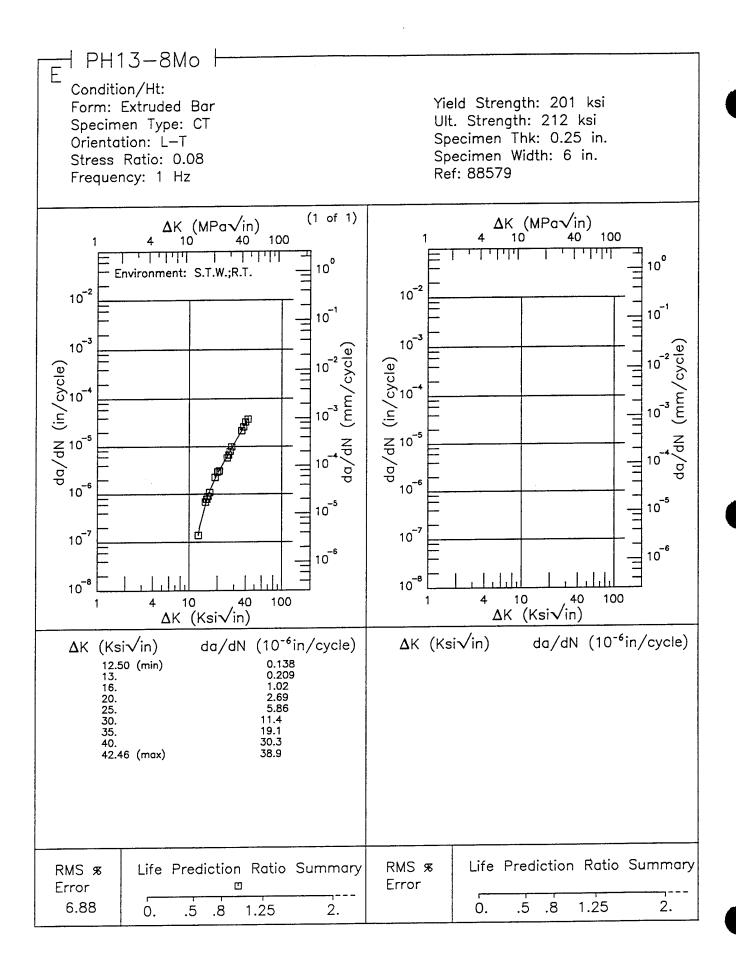


Figure 4.17.3.1.3

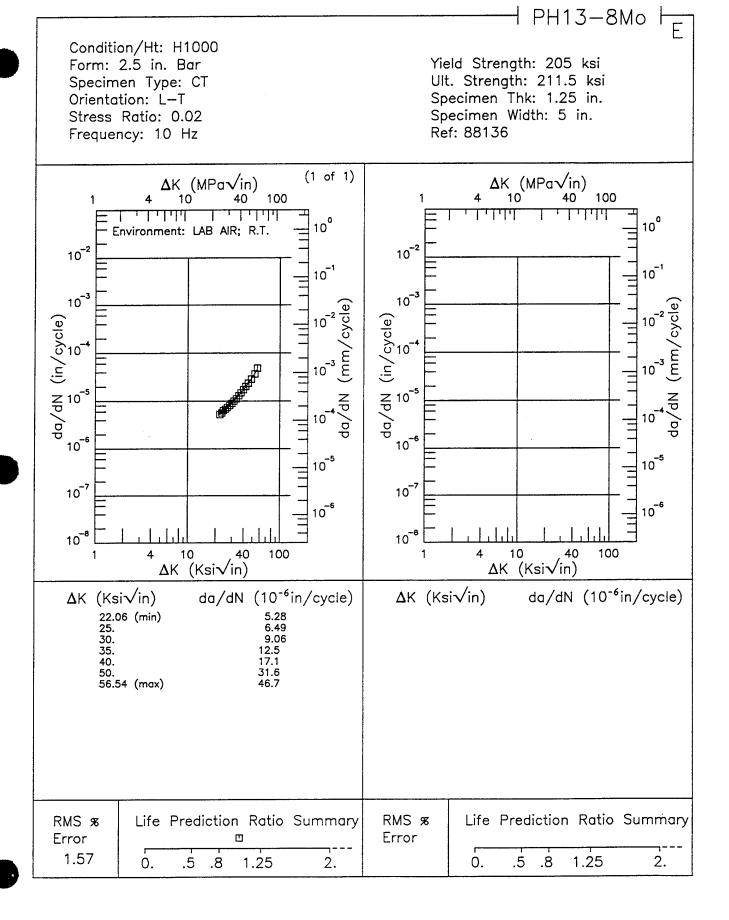


Figure 4.17.3.1.4

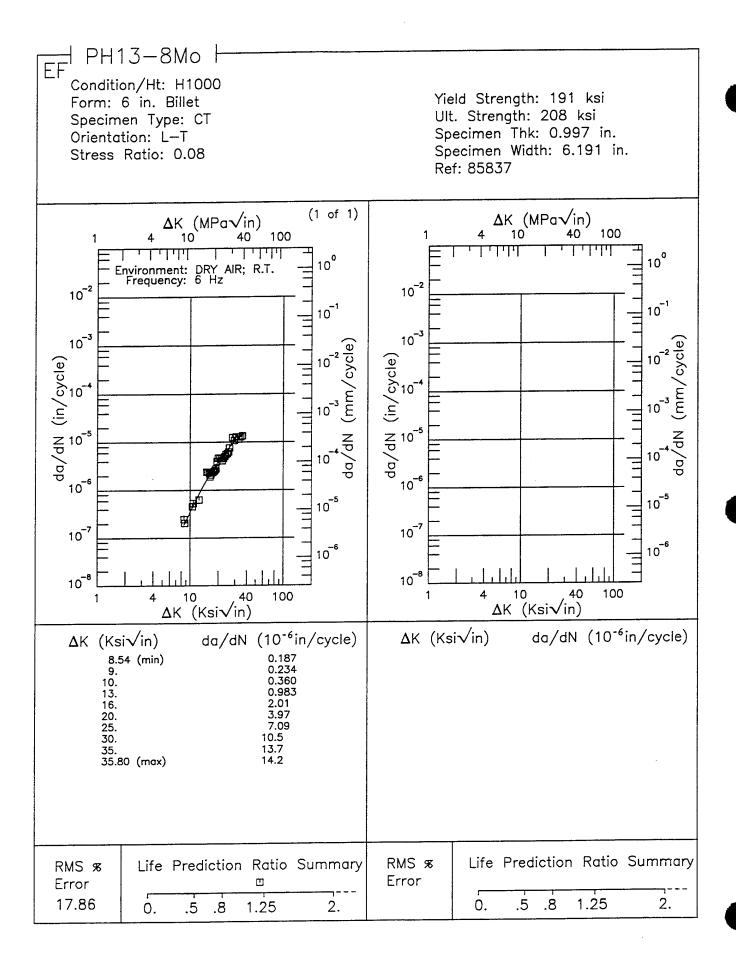


Figure 4.17.3.1.5

H PH13-8Mo EF Condition/Ht: H1000 Yield Strength: 190 ksi Form: 22 in. Billet Ult. Strength: 207 ksi Specimen Type: CT Specimen Thk: 1 in. Orientation: T-L Specimen Width: 4.94 in. Stress Ratio: 0.08 Ref: 88579 (1 of 1) $\Delta K (MPa\sqrt{in})$ Δ K (MPa \sqrt{in}) 100 10 40 10 40 100 1 1 1 1 1 10⁰ 10° Environment: DRY AIR; R.T. Frequency: 6 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ 10 -2 da/dN (in/cycle) da/dN (in/cycle) 10⁻³ 10⁻⁶ 10⁻⁶ 10 5 10 -5 10⁻⁷ 10⁻⁷ 10 -6 10⁻⁶ 10⁻⁸ 10⁻⁸ 4 10 40 100 40 100 10 ΔK (Ksi√in) **Δ**K (Ksi√in) da/dN ($10^{-6}in/cycle$) ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) 8.63 (min) 9. 0.370 13. 1.95 16. 20. 25. 30. 35. 8.06 11.5 16.2 30.7 55.15 (max) Life Prediction Ratio Summary RMS % RMS % Life Prediction Ratio Summary Error ⍗ Error 6.32 .5 1.25 2. 2. 0. .8 1.25 0. .5 8.

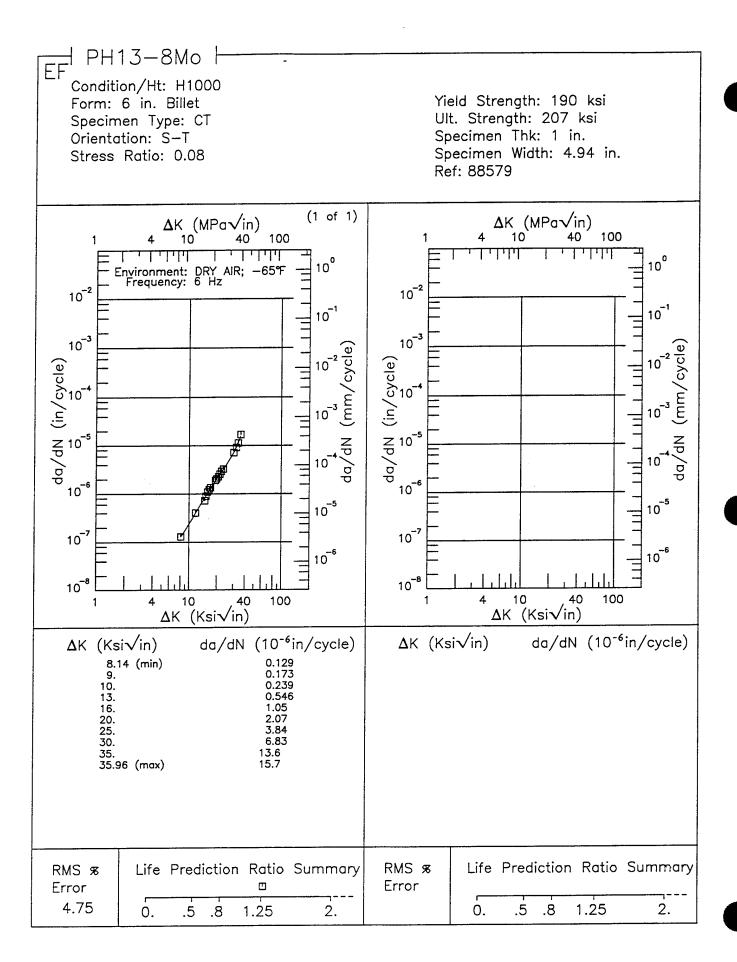


Figure 4.17.3.1.7

H PH13−8Mo HR Condition/Ht: H1000 Yield Strength: 214 ksi Form: 1.5 in. Extruded Bar Ult. Strength: 221 ksi Specimen Type: CT Specimen Thk: 1 in. Orientation: L-T Specimen Width: 6.17 - 6.18 in. Frequency: 6 Hz Ref: 88579 Environment: DRY AIR; RT (2 of 2) (1 of 2) ΔK (MPa√in) ΔK (MPa√in) 10 40 100 100 1 1 1 1 1 11111 10° 10° Stress Ratio: 0.5 Stress Ratio: 0.08 10-2 10 -2 10⁻¹ 10-1 10⁻³ 10⁻³ 10⁻²(0) da/dN (in/cycle) da/dN (in/cycle) 10 -3 10⁻⁶ 10 6 10⁻⁵ 10 5 10⁻⁷ 10⁻⁷ 10 6 10 6 10⁻⁸ 10-8 100 10 100 10 40 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) $da/dN (10^{-6}in/cycle)$ ΔK (Ksi√in) ΔK (Ksi√in) 7.25 (min) 8. 0.254 7.96 (min) 8. 9. 10. 13. 0.381 10. 13. 16. 20. 25. 30. 33.12 (max) 20.3 59.52 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error Φ 11.09 21.06 0. .5 .8 1.25 2. 0. .5 1.25 2. .8

Figure 4.17.3.1.8

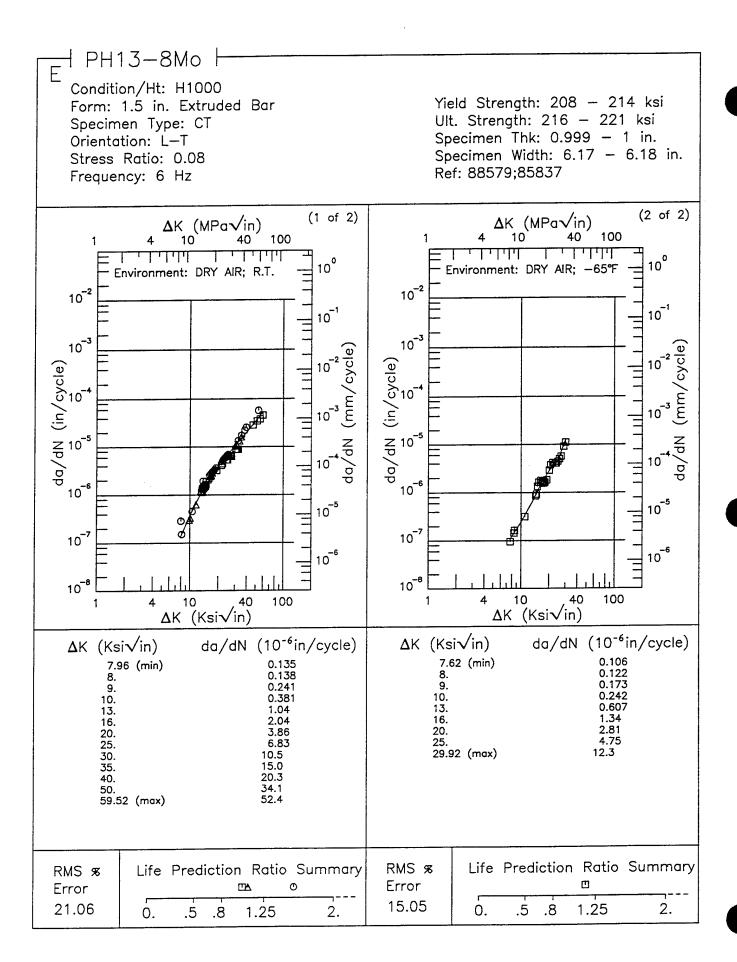


Figure 4.17.3.1.9

Yield Strength: 214 ksi Form: 1.5 in. Extruded Bar Ult. Strength: 221 ksi Specimen Type: CT Orientation: L-T Specimen Thk: 1 in. Specimen Width: 6.18 in. Stress Ratio: 0.08 Ref: 88579 Frequency: 1 Hz (1 of 1) ΔK (MPa√in) Δ K (MPa \sqrt{in}) 100 10 40 100 10 11111 10⁰ 10⁰ Environment: S.T.W. 10-2 10⁻² 10-1 10 -1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10 -3 10⁻⁶ 10⁻⁶ 10⁻⁵ 10 5 10-7 10⁻⁷ 10⁻⁶ 10 6 10⁻⁸ 10 8 10 100 10 40 100 40 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) da/dN (10⁻⁶in/cycle) Δ K (Ksi \sqrt{in}) 8.27 (min) 0.388 10. 13. 16. 20. 25. 34.43 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error. Error 7.75 0. .5 .8 1.25 2. 0. .5 .8 1.25 2.

Condition/Ht: H1000

HPH13-8Mo F

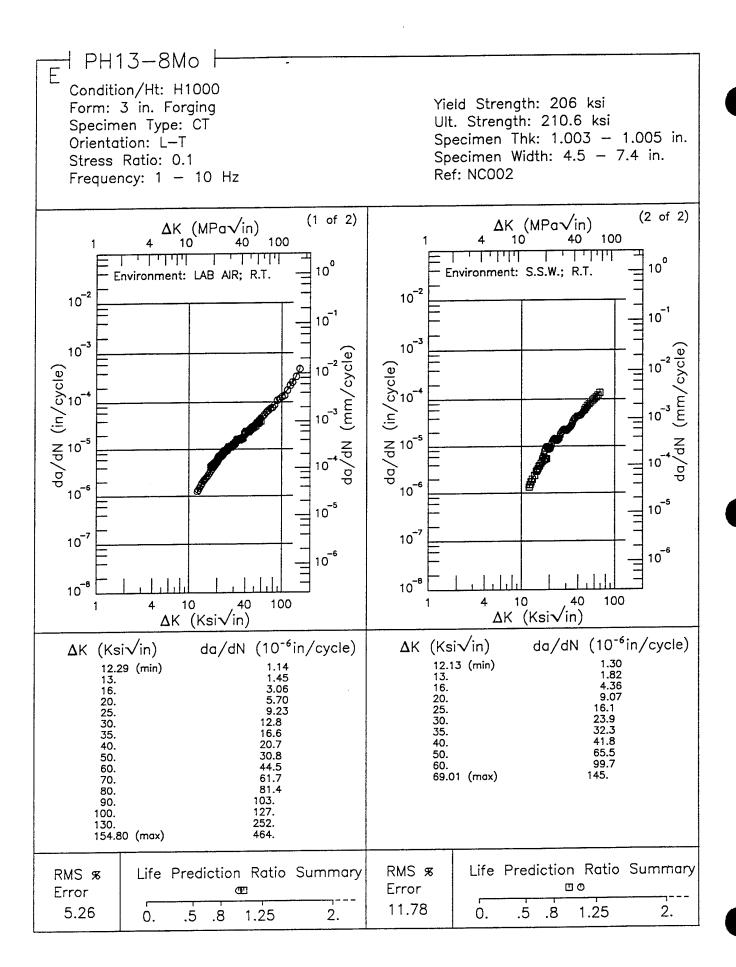


Figure 4.17.3.1.11

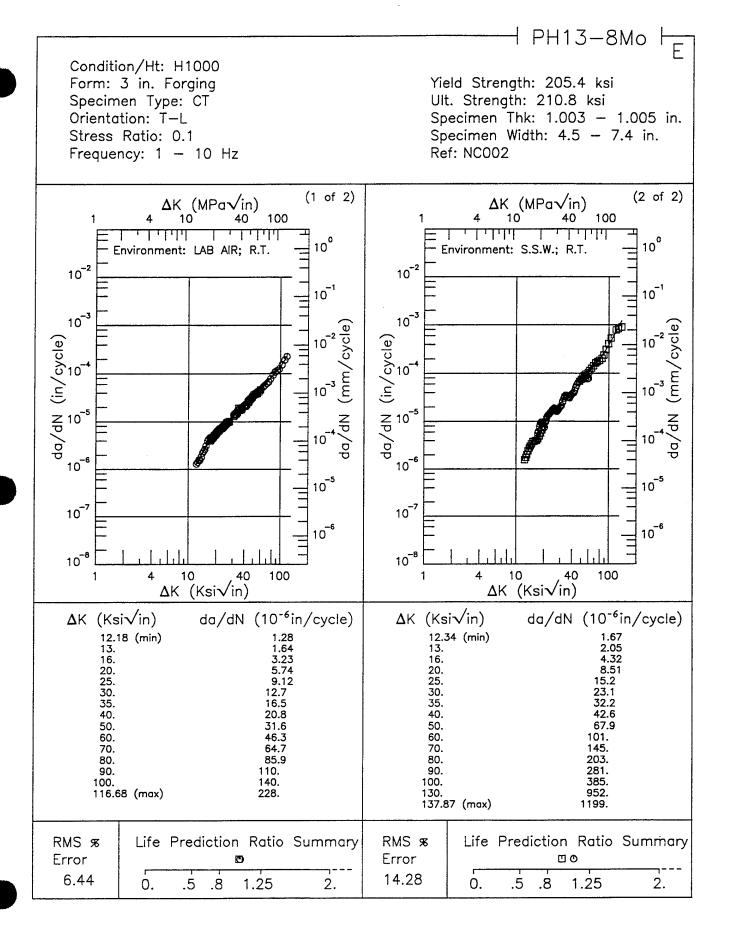


Figure 4.17.3.1.12

1 PH13-8Mo 1 Condition/Ht: H1000 Yield Strength: 201 ksi Form: 4 in. Forged Bar Ult. Strength: 212 ksi Specimen Type: CT Specimen Thk: 0.99 - 0.998 in. Orientation: L-T Specimen Width: 6 in. Frequency: 6 Hz Ref: 85837;88579 Environment: DRY AIR; RT (2 of 3) (1 of 3) $\Delta K (MPa\sqrt{in})$ Δ K (MPa \sqrt{in}) 10 100 40 10 40 100 البليانا ليليلي 10° الليليك 71111 10° Stress Ratio: 0.3 Stress Ratio: 0.08 10-2 10 2 10⁻¹ 10⁻¹ 10⁻³ 10⁻³ 10-2 da/dN (in/cycle) da/dN (in/cycle) 10 -6 10⁻⁶ 10⁻⁵ 10⁻⁵ 10⁻⁷ 10⁻⁷ 10⁻⁶ 10⁻⁶ 10 8 40 100 4 10 40 100 1 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) 0.567 1.33 10.25 (min) 10.78 (min) 13. 16. 1.52 13. 16. 20. 25. 3.49 20. 5.82 25. 13.4 20.0 30. 30. 34.71 (max) 34.32 (max) 19.9 Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error 17.38 1.25 2. .5 .8 0. 10.41 2. .5 1.25 0. 8.

Figure 4.17.3.1.13

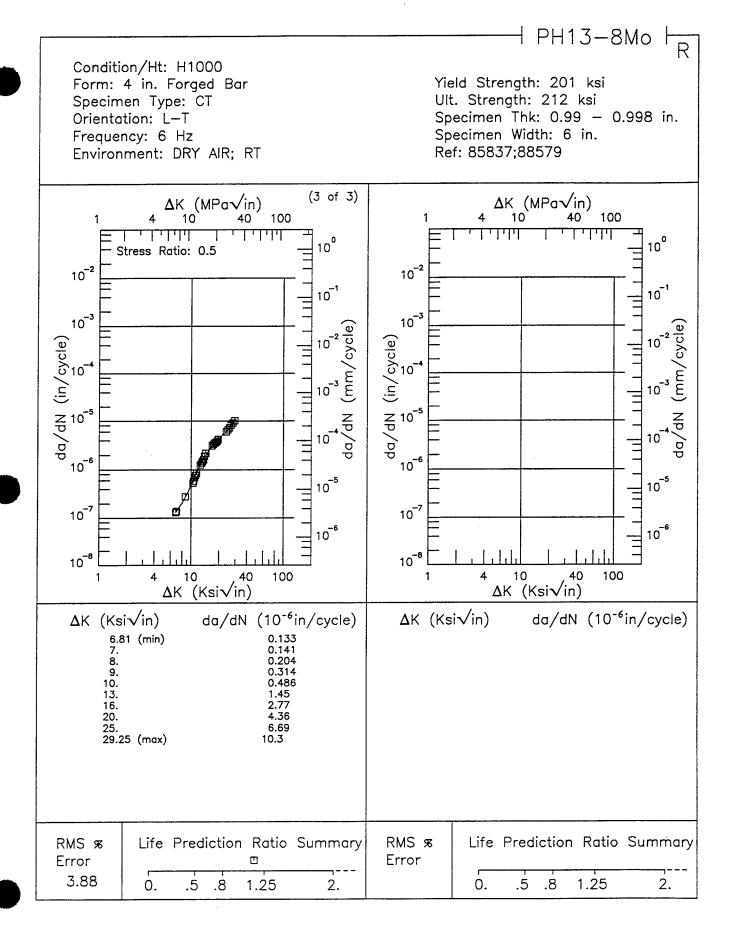


Figure 4.17.3.1.13 (Concluded)

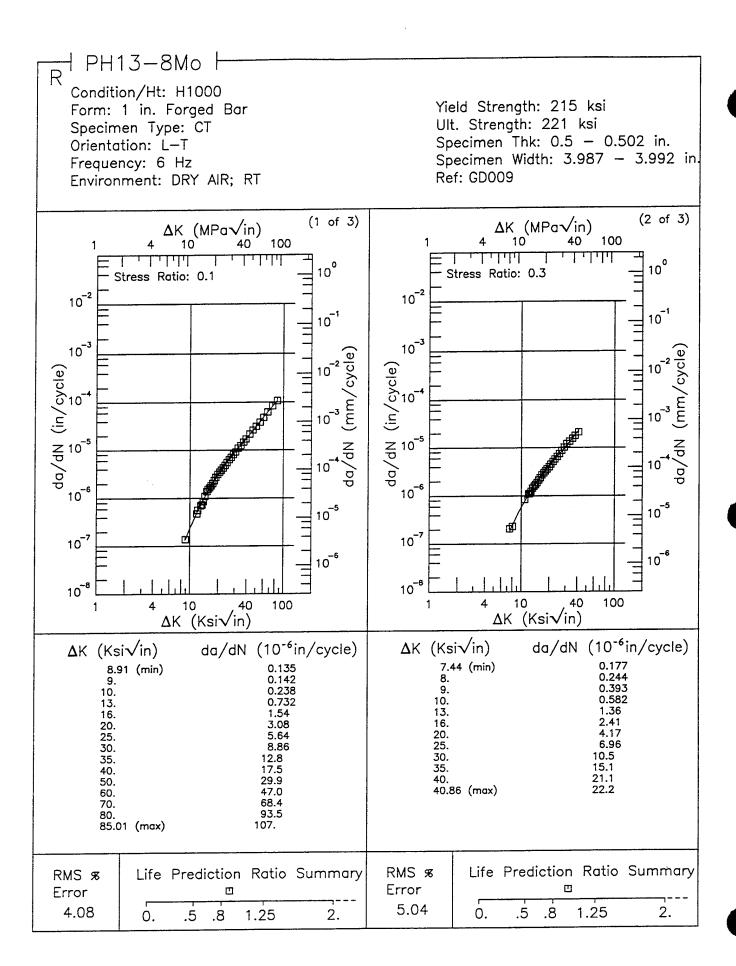


Figure 4.17.3.1.14

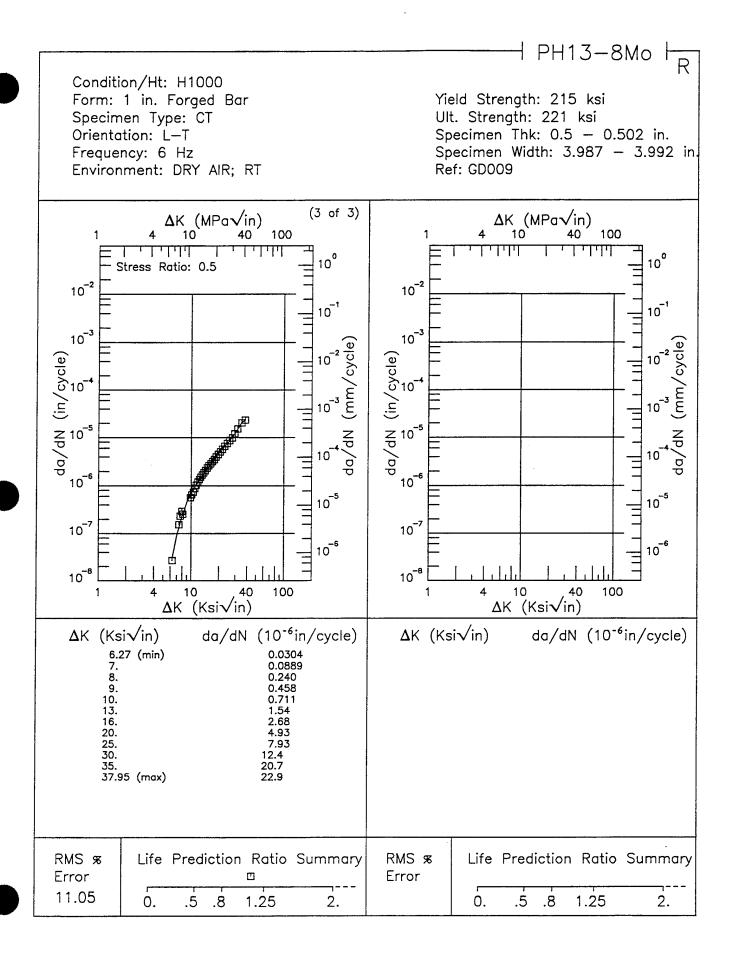


Figure 4.17.3.1.14 (Concluded)

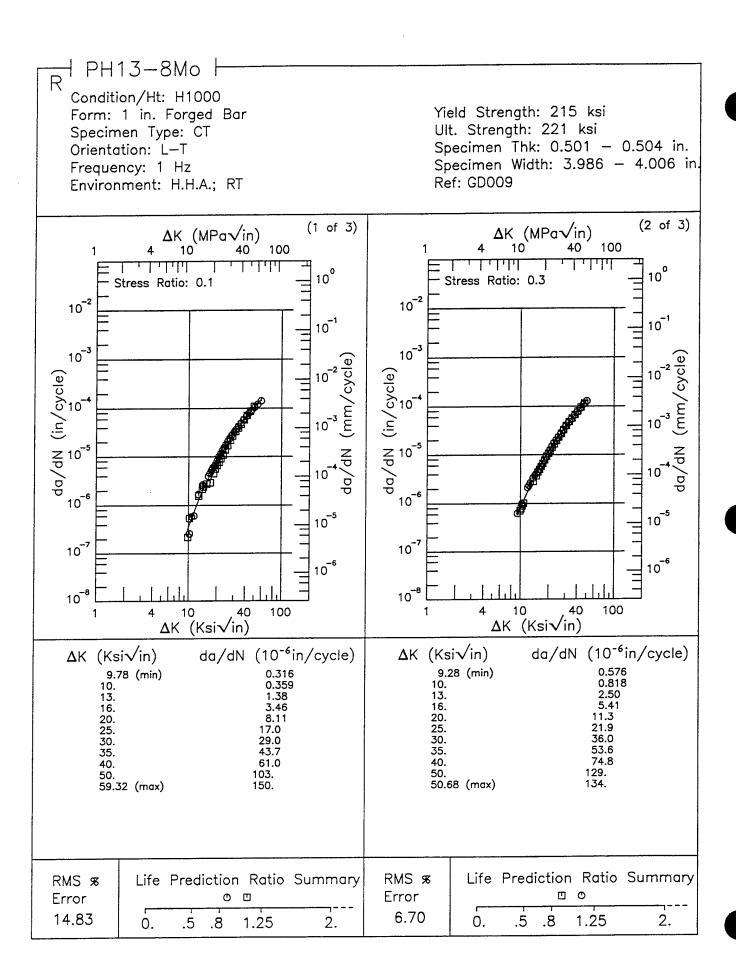


Figure 4.17.3.1.15

1 PH13-8Mo | R Condition/Ht: H1000 Yield Strength: 215 ksi Form: 1 in. Forged Bar Ult. Strength: 221 ksi Specimen Type: CT Specimen Thk: 0.501 - 0.504 in. Orientation: L-T Specimen Width: 3.986 - 4.006 in Frequency: 1 Hz Ref: GD009 Environment: H.H.A.; RT (3 of 3) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 10 100 100 10 40 10⁰ 10° Stress Ratio: 0.5 10⁻² 10-2 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻³ 10-6 10⁻⁶ 10⁻⁵ 10⁻⁵ 10⁻⁷ 10⁻⁷ 10 6 10⁻⁶ 10⁻⁸ 10 8 100 10 40 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) $da/dN (10^{-6}in/cycle)$ 6.78 (min) 7. 8. 0.265 0.283 0.403 10. 13. 16. 25. 30. 35. 47.33 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error 四〇 Error 13.20 0. .5 .8 1.25 2. .5 .8 1.25 2. 0.

Figure 4.17.3.1.15 (Concluded)

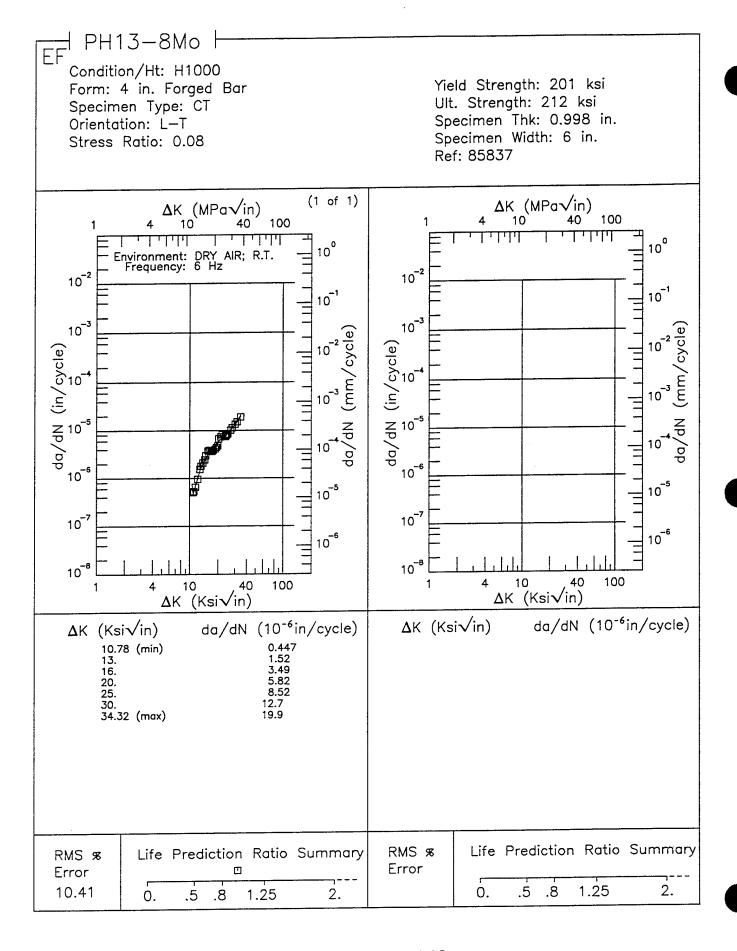


Figure 4.17.3.1.16

1 PH13-8Mo EF

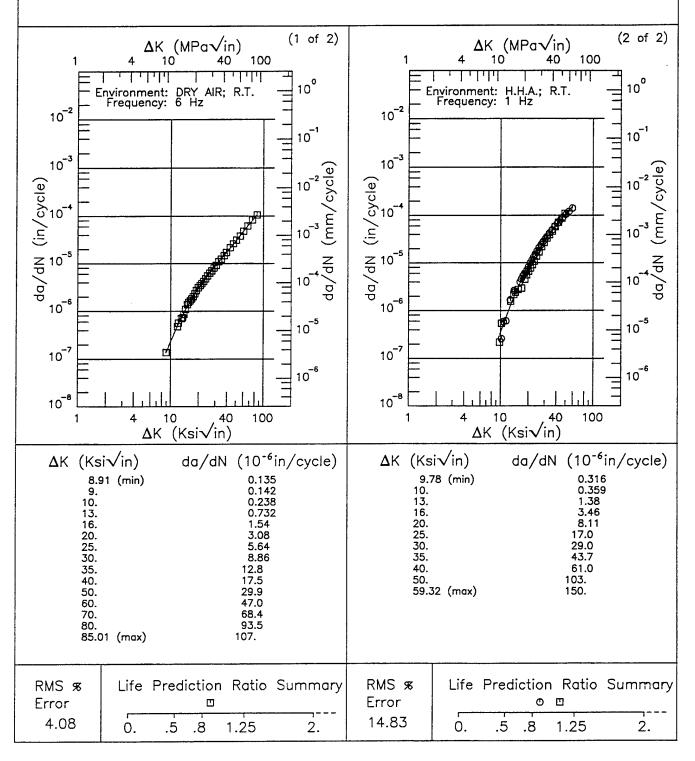
Condition/Ht: H1000 Form: 1 in. Forged Bar

Specimen Type: CT Orientation: L-T Stress Ratio: 0.1

Yield Strength: 215 ksi Ult. Strength: 221 ksi

Specimen Thk: 0.501 - 0.504 in. Specimen Width: 3.986 - 3.99 in.

Ref: GD009



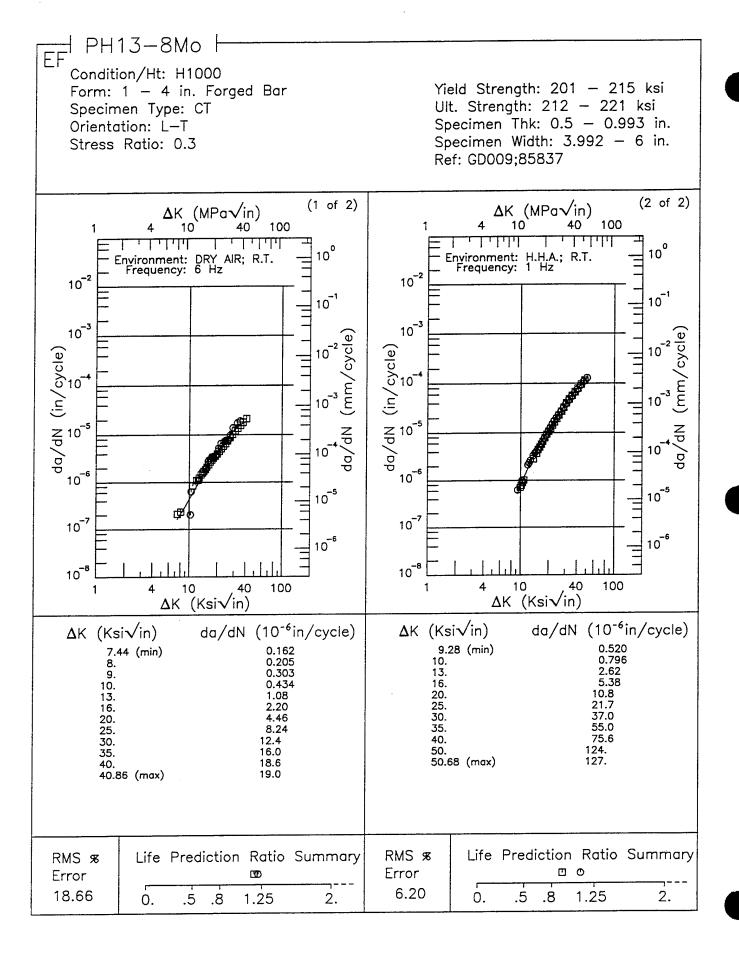


Figure 4.17.3.1.18

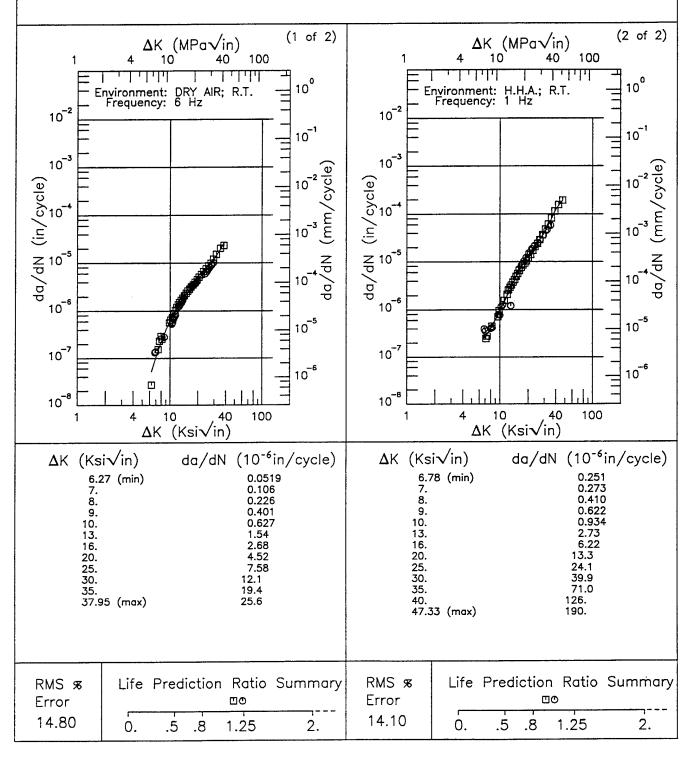
→ PH13-8Mo FF

Condition/Ht: H1000

Form: 1 - 4 in. Forged Bar

Specimen Type: CT Orientation: L—T Stress Ratio: 0.5 Yield Strength: 201 — 215 ksi Ult. Strength: 212 — 221 ksi Specimen Thk: 0.501 — 0.99 in. Specimen Width: 3.987 — 6 in.

Ref: GD009;88579



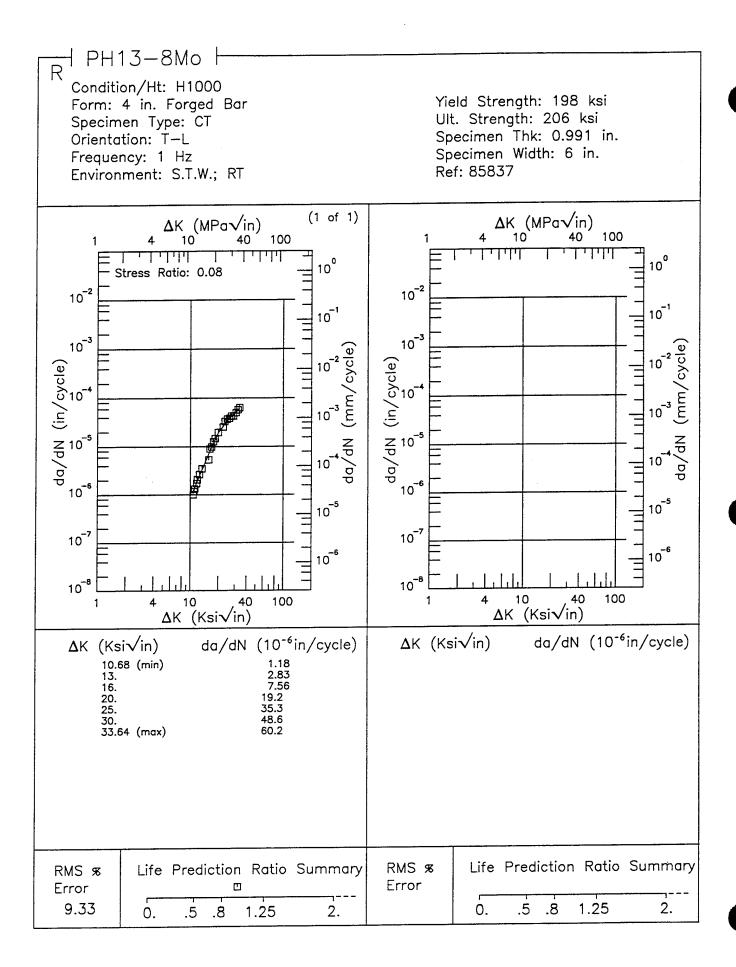


Figure 4.17.3.1.20

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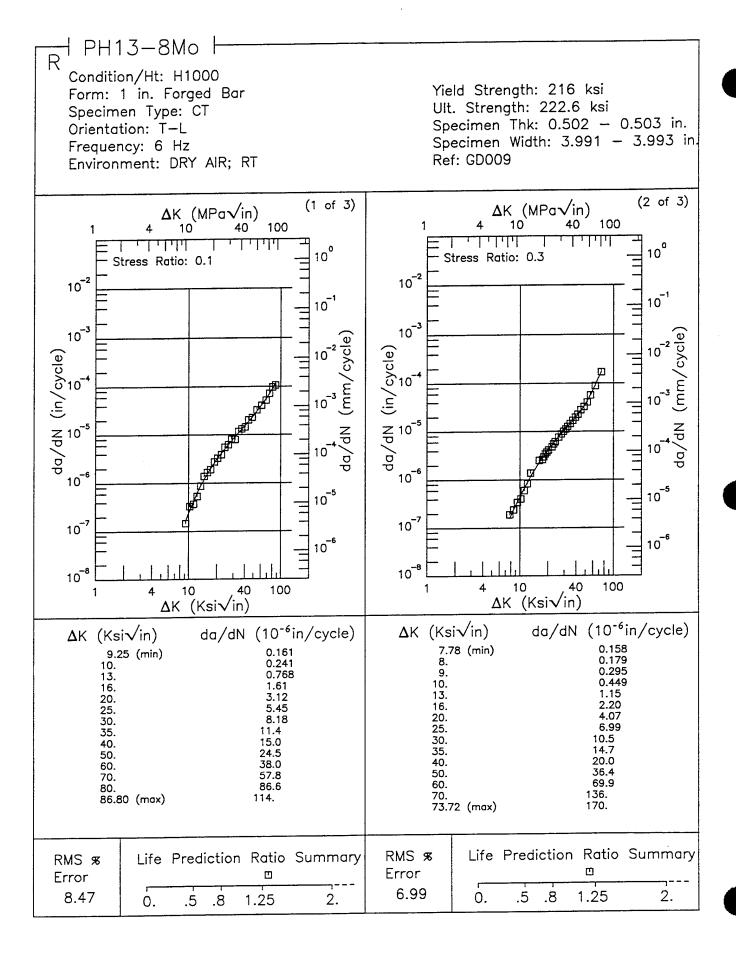


Figure 4.17.3.1.21

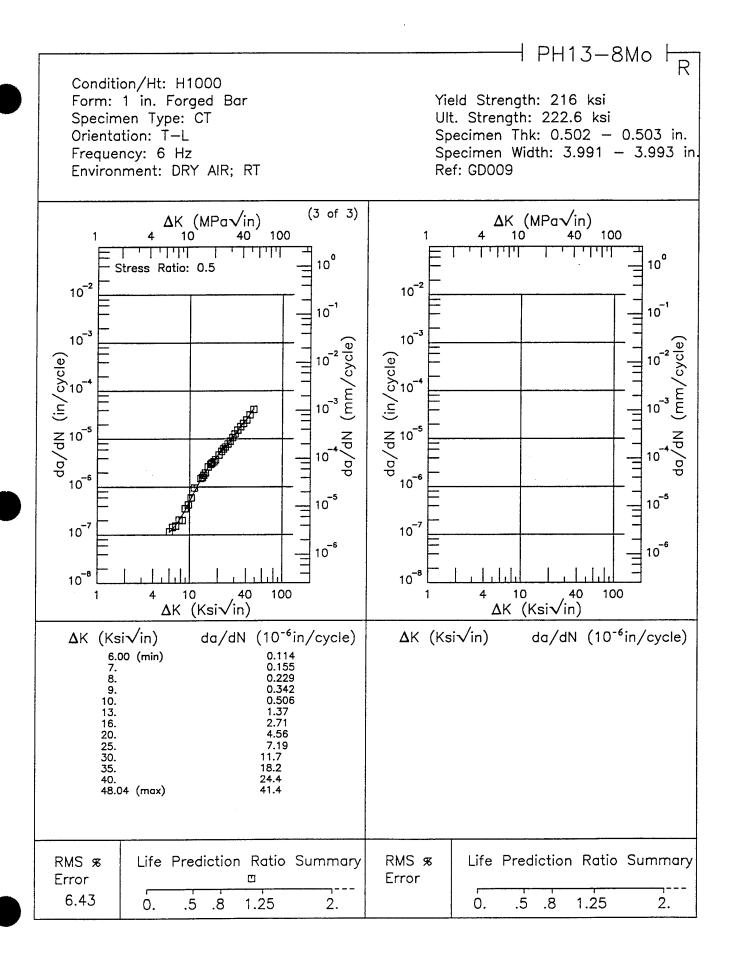


Figure 4.17.3.1.21 (Concluded)

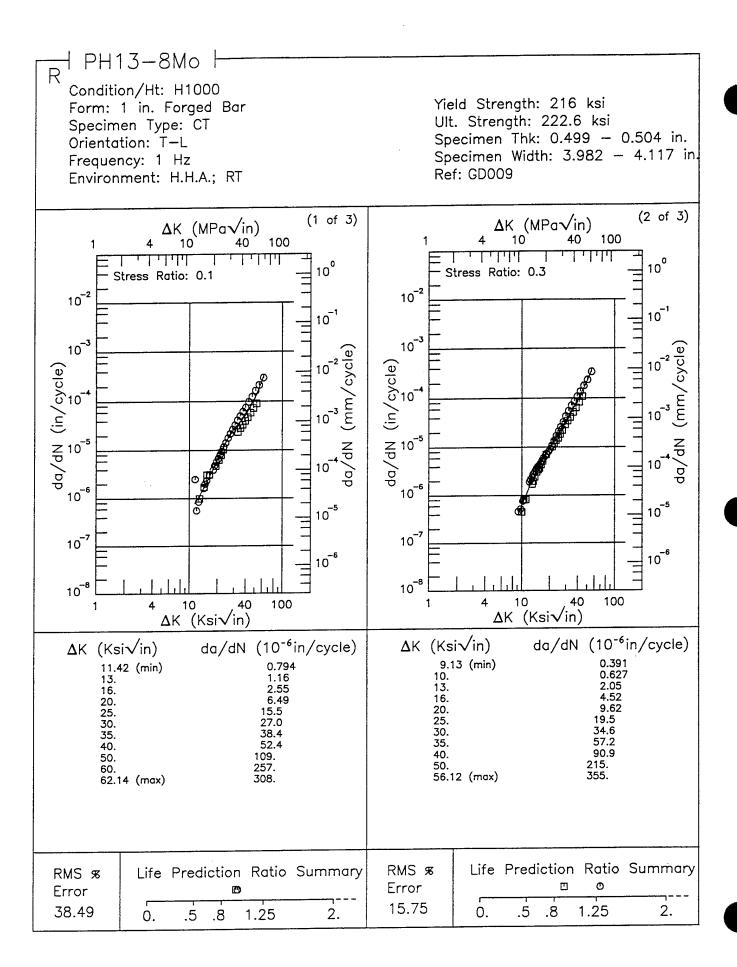


Figure 4.17.3.1.22

H PH13−8Mo HR Condition/Ht: H1000 Yield Strength: 216 ksi Form: 1 in. Forged Bar Ult. Strength: 222.6 ksi Specimen Type: CT Specimen Thk: 0.499 - 0.504 in. Orientation: T-L Specimen Width: 3.982 - 4.117 in Frequency: 1 Hz Ref: GD009 Environment: H.H.A.; RT (3 of 3) $\Delta K_{10} (MPa\sqrt{in})$ Δ K (MPa \sqrt{in}) 100 100 10 40 البابالي 10° 10° Stress Ratio: 0.5 10-2 10-2 10⁻¹ 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10 -3 10⁻⁶ 10-6 10⁻⁵ 10 -5 10⁻⁷ 10⁻⁷ 10 6 10⁻⁶ 10⁻⁸ 10 8 100 4 10 40 100 10 40 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) 6.87 (min) 0.242 7. 8. 0.264 9. 10. 13. 16. 40. 176. 50.46 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error 14.72 .5 1.25 2. 0. .8 .5 .8 1.25 2. 0.

Figure 4.17.3.1.22 (Concluded)

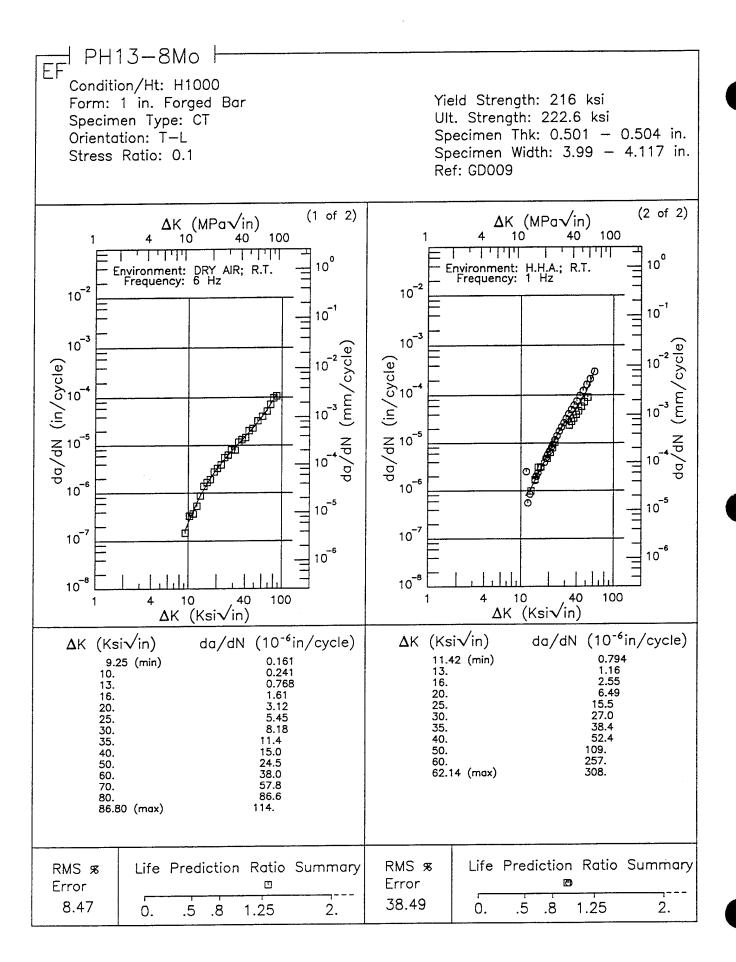


Figure 4.17.3.1.23

↑ PH13-8Mo EF Condition/Ht: H1000 Yield Strength: 216 ksi Form: 1 in. Forged Bar Ult. Strength: 222.6 ksi Specimen Type: CT Specimen Thk: 0.501 - 0.502 in. Orientation: T-L Specimen Width: 3.988 - 3.992 in Stress Ratio: 0.3 Ref: GD009 (2 of 2) (1 of 2) Δ K (MPa \sqrt{in}) ΔK (MPa√in) 100 10 40 10 40 100 1 1 1 1 1 1 1 بابابانا 10° 10° Environment: DRY AIR; R.T. Frequency: 6 Hz Environment: H.H.A; R.T. Frequency: 1 Hz 10-2 10-2 10 1 10-1 10⁻³ 10⁻³ 10-2 da/dN (in/cycle) da/dN (in/cycle) 10⁻³ 10 6 10⁻⁶ 10⁻⁵ 10⁻⁵ 10⁻⁷ 10-7 10⁻⁶ 10 6 10 8 10⁻⁸ 4 10 40 100 4 10 40 100 1 ∆K (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) $da/dN (10^{-6}in/cycle)$ ΔK (Ksi√in) 9.13 (min) 0.391 7.78 (min) 0.157 10. 13. 16. 0.178 8. 9. 4.52 0.450 10. 20. 25. 13. 16. 20. 30. 35. 90.9 215. 355. 40. 50. 56.12 (max) 20.0 50. 36.6 69.8 60. 70. 73.72 (max) 134. 170. RMS % Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % Ø Error Error 15.75 7.10 0. .5 .8 1.25 2. 2. .5 8. 1.25 0.

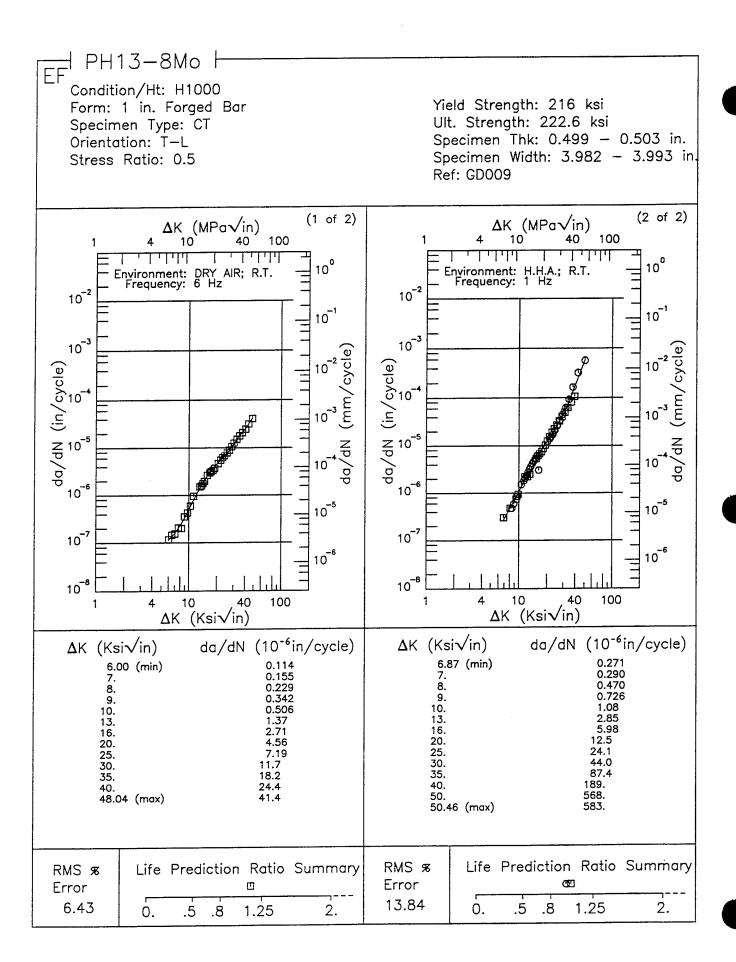


Figure 4.17.3.1.25

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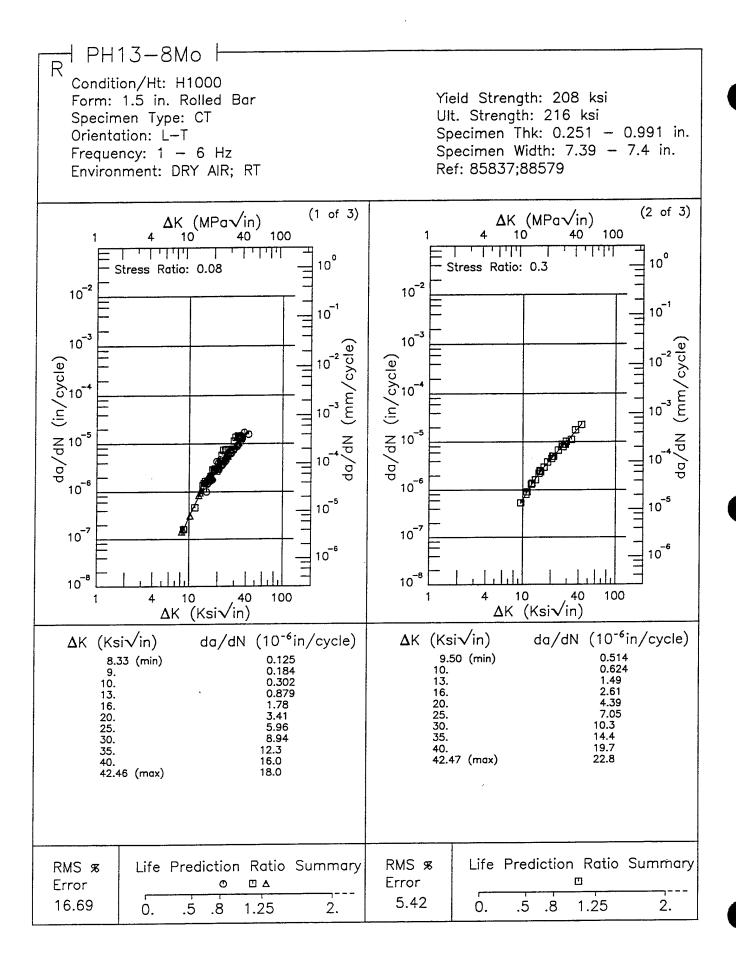


Figure 4.17.3.1.26

1 PH13—8Mo H Condition/Ht: H1000 Yield Strength: 208 ksi Form: 1.5 in. Rolled Bar Specimen Type: CT Ult. Strength: 216 ksi Specimen Thk: 0.251 - 0.991 in. Orientation: L-T Specimen Width: 7.39 - 7.4 in. Frequency: 1 - 6 Hz Ref: 85837;88579 Environment: DRY AIR; RT (3 of 3) Δ K (MPa \sqrt{in}) ΔK (MPa√in) 100 10 100 10 40 40 1 1 1 1 1 1 ليليليل 10° 10° Stress Ratio: 0.5 10⁻² 10-2 10-1 10-1 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10 6 10⁻⁶ 10 5 10 5 10⁻⁷ 10⁻⁷ 10 6 10⁻⁶ 10 8 10 8 10 40 100 10 40 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) **Δ**K (Ksi√in) ΔK (Ksi√in) da/dN (10⁻⁶in/cycle) 9.52 (min) 10. 13. 16. 20. 25. 30. 35. 41.04 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error ⊞ Error 6.68 .5 .8 1.25 0. .5 .8 1.25 2. 0. 2.

Figure 4.17.3.1.26 (Concluded)

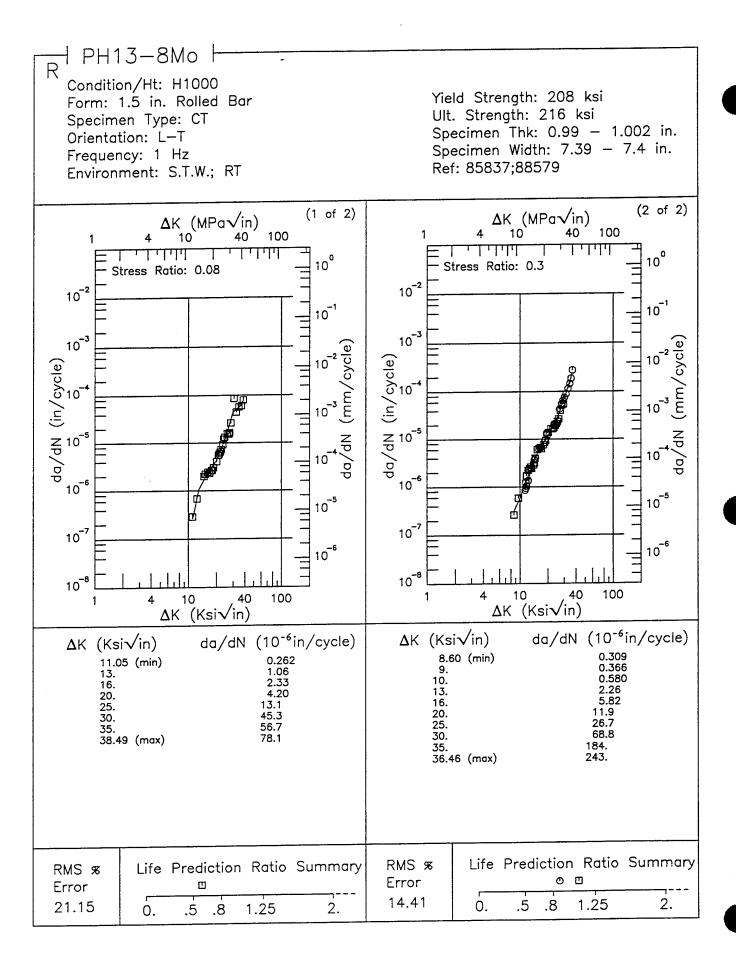


Figure 4.17.3.1.27

⊢ PH13-8Mo ⊢ Condition/Ht: H1000 Form: 1.5 in. Rolled Bar Yield Strength: 208 ksi Specimen Type: CT Ult. Strength: 216 ksi Orientation: L-T Specimen Thk: 0.251 - 0.993 in. Stress Ratio: 0.08 Specimen Width: 7.39 - 7.4 in. Frequency: 1 - 6 Hz Ref: 85837;88579 (1 of 2)(2 of 2) ΔK (MPa√in) ΔK (MPa√in) 100 10 10 100 40 40 لللللك للبليات 7 11 111 11111 10° 10° Environment: DRY AIR; R.T. Environment: DRY AIR; -65°F 10-2 10⁻² 10-1 10 10⁻³ 10⁻³ da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10⁻⁶ 10 -5 10 5 10⁻⁷ 10 7 10 6 10⁻⁶ 10 8 10⁻⁸ 100 10 40 10 40 100 4 ΔK (Ksi√in) ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) **Δ**K (Ksi√in) da/dN (10⁻⁶in/cycle) 8.33 (min) 15.07 (min) 0.404 16. 0.594 10. 20. 1.67 13. 16. 20. 25. 25. 29.64 (max) 3.68 7.95 35. 42.46 (max) RMS % Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary Error ◫◬ Error ╝ 16.69 13.42 0. .5 8. .5 1.25 1.25 2. 0. .8 2.

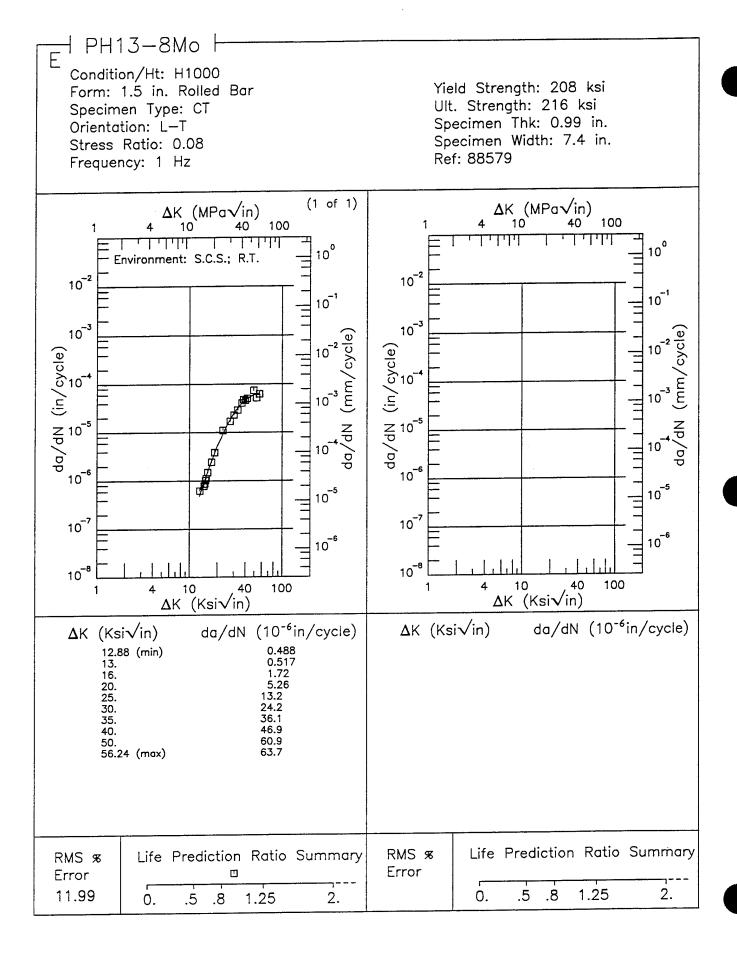


Figure 4.17.3.1.29

H PH13−8Mo F Condition/Ht: H1000 Yield Strength: 208 ksi Form: 1.5 in. Rolled Bar Ult. Strength: 216 ksi Specimen Type: CT Orientation: L-T Specimen Thk: 0.99 - 1.002 in. Specimen Width: 7.4 in. Stress Ratio: 0.08 Environment: S.T.W.; RT Ref: 88579;85837 (1 of 2)(2 of 2) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 10 10 100 40 100 40 11111 ليليليان 10° 10° Frequency: 1 Hz Frequency: 0.1 Hz 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ 10-2 da/dN (in/cycle) 10 10⁻⁶ 10-6 10⁻⁵ 10⁻⁵ 10⁻⁷ 10⁻⁷ 10 6 10⁻⁶ 10 8 10 -8 40 10 40 10 100 100 ΔK (Ksi√in) ΔK (Ksi√in) $da/dN (10^{-6}in/cycle)$ da/dN (10⁻⁶in/cycle) **Δ**K (Ksi√in) ΔK (Ksi√in) 14.76 (min) 2.15 2.95 11.05 (min) 0.256 16. 13. 16. 1.08 20. 25. 2.30 20. 4.08 25. 30. 31.99 (max) 26.7 35. 38.49 (max) RMS % Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary Error Error 2.62 23.86 .5

Figure 4.17.3.1.30

2.

0.

.5

.8

1.25

0.

1.25

2.

.8

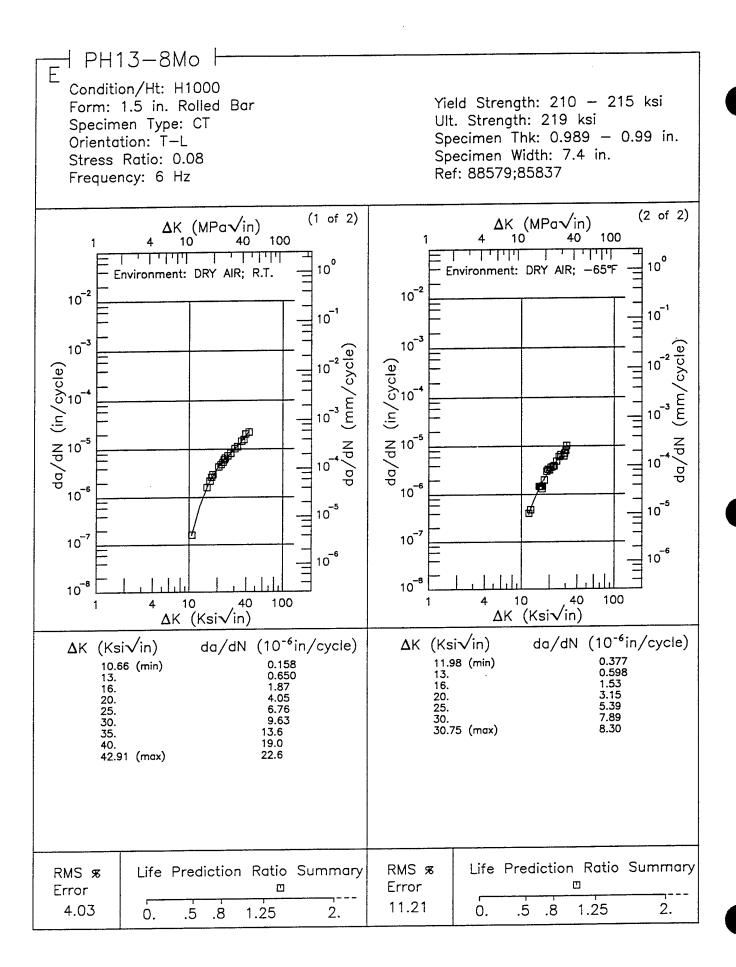


Figure 4.17.3.1.31

H PH13−8Mo FF

Condition/Ht: H1000 Form: 1.5 in. Rolled Bar

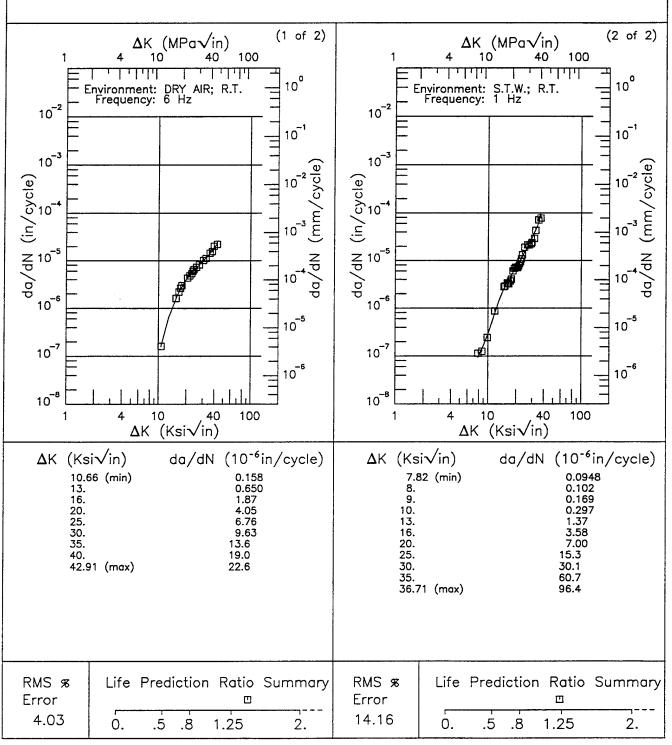
Specimen Type: CT Orientation: T-L Stress Ratio: 0.08 Yield Strength: 210 - 215 ksi

Ult. Strength: 219 ksi

Specimen Thk: 0.99 - 0.993 in.

Specimen Width: 7.4 in.

Ref: 88579



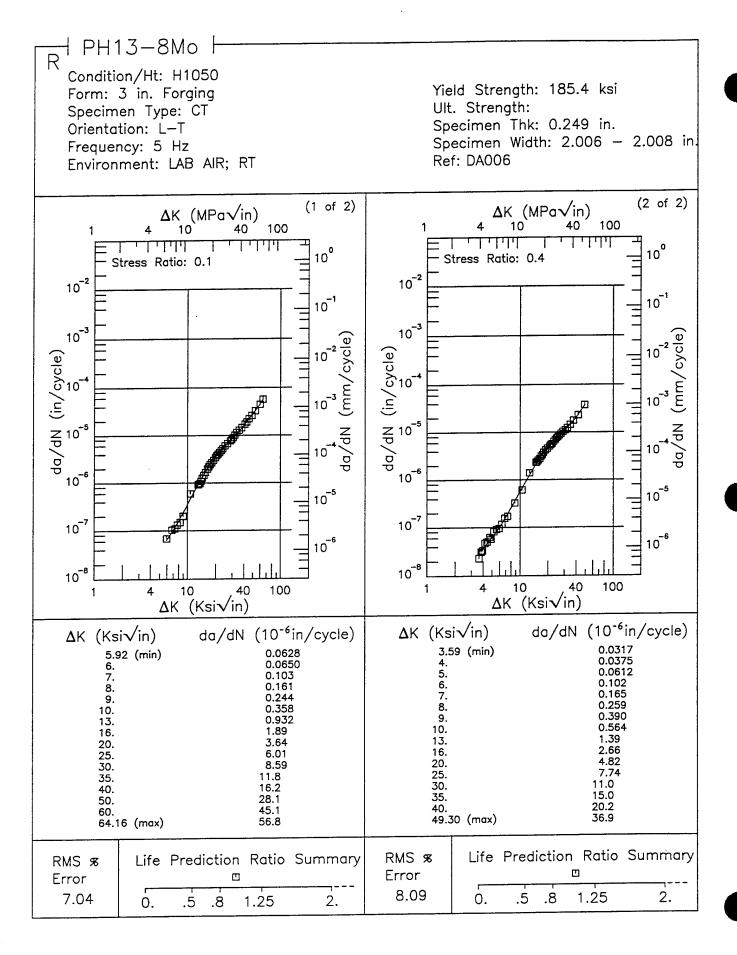


Figure 4.17.3.1.33

Condition/Ht: H1050 Yield Strength: 196.5 ksi Form: 3 in. Forging Specimen Type: CT Ult. Strength: Specimen Thk: 0.249 - 0.25 in. Orientation: L-T Specimen Width: 1.996 - 2 in. Frequency: 20 Hz Ref: DA007 Environment: LAB AIR; RT (2 of 2)(1 of 2) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 100 10 40 100 10 1 1 1 1 1 1 1 11111 10° 10° Stress Ratio: 0.4 Stress Ratio: 0.1 10-2 10-2 10 1 10 1 10⁻³ 10-3 da/dN (in/cycle) da/dN (in/cycle) 10⁻⁶ 10-6 10⁻⁵ 10 -5 10⁻⁷ 10⁻⁷ 10 6 10 -6 10⁻⁸ 10 8 40 100 4 O 10 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) da/dN (10⁻⁶in/cycle) **Δ**K (Ksi√in) ΔK (Ksi√in) 0.0155 0.0160 3.46 (min) 5.08 (min) 0.0180 3.5 0.0360 6. 7. 4. 5. 6. 7. 8. 9. 0.0240 0.0682 8. 0.118 0.188 9. 10. 16. 1.55 20. 10. 30. 8.64 16. 40. 4.28 20. 60. 10.3 30. 80. 90.7 18.3 184. 100. 58.45 (max) 48.8 100.97 (max) Life Prediction Ratio Summary Life Prediction Ratio Summary RMS % RMS % Error Error 13.07 14.16 0. .5 8. 1.25 2. .5 8. 1.25 2. ٥.

1 PH13-8Mo F

Figure 4.17.3.1.34

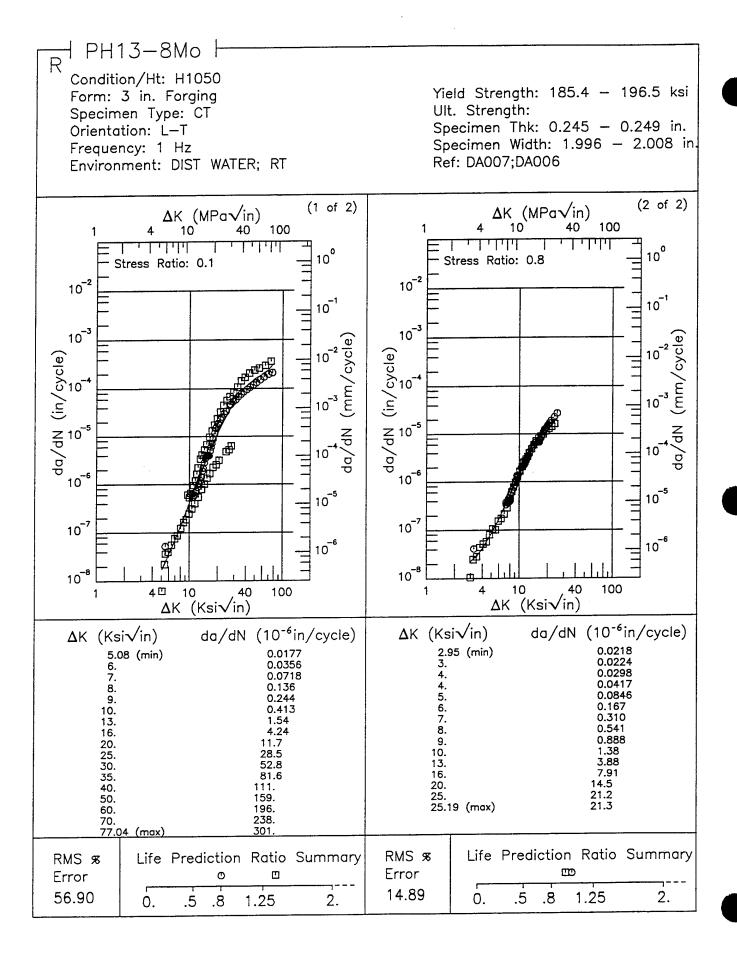


Figure 4.17.3.1.35

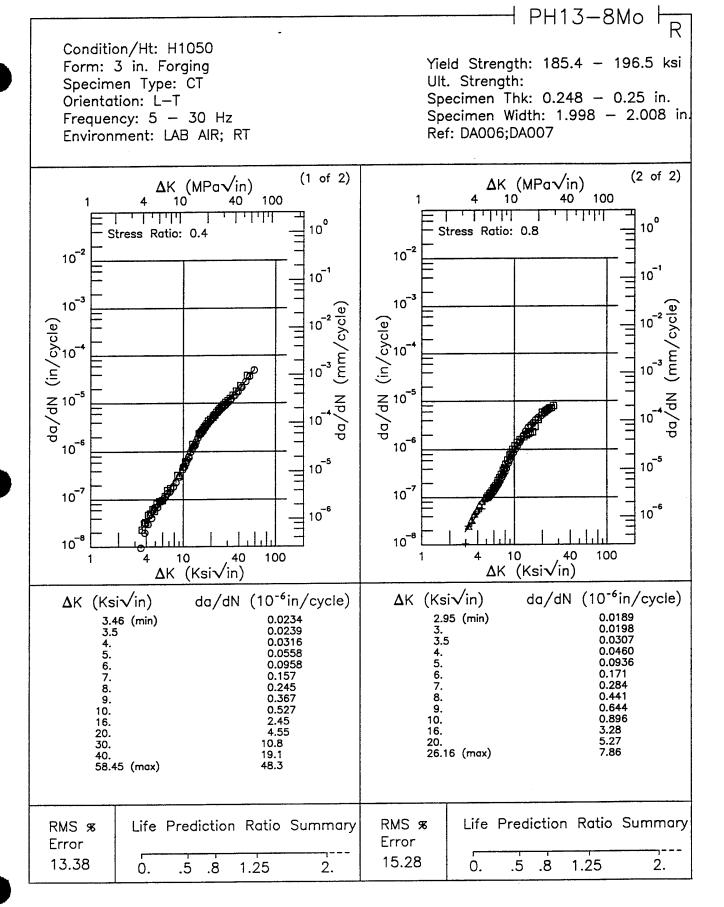


Figure 4.17.3.1.36

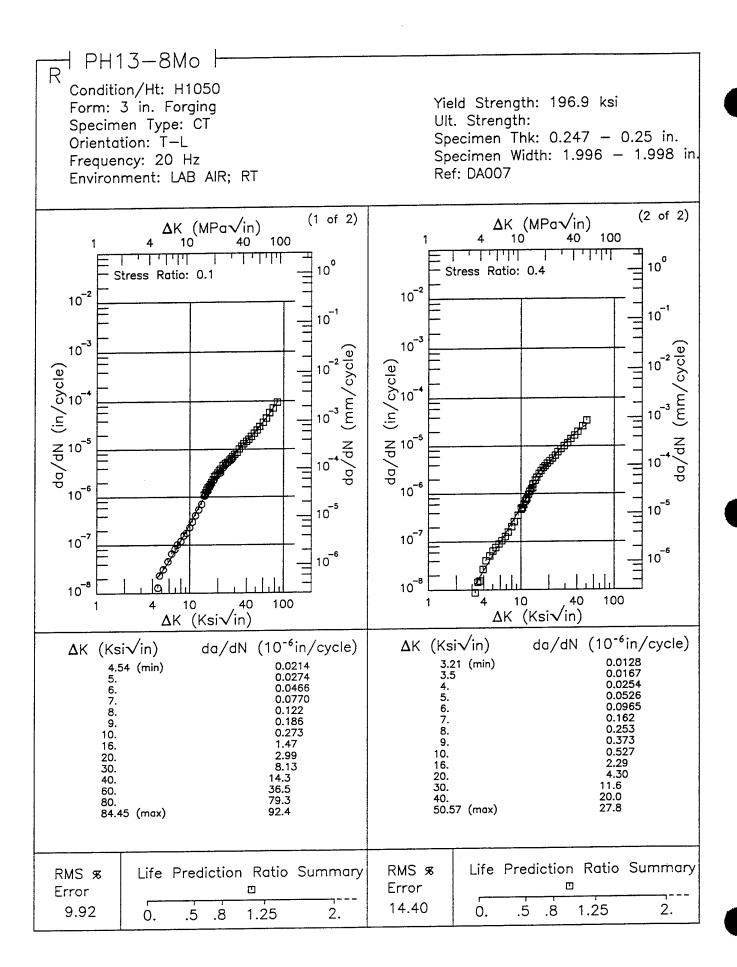


Figure 4.17.3.1.37

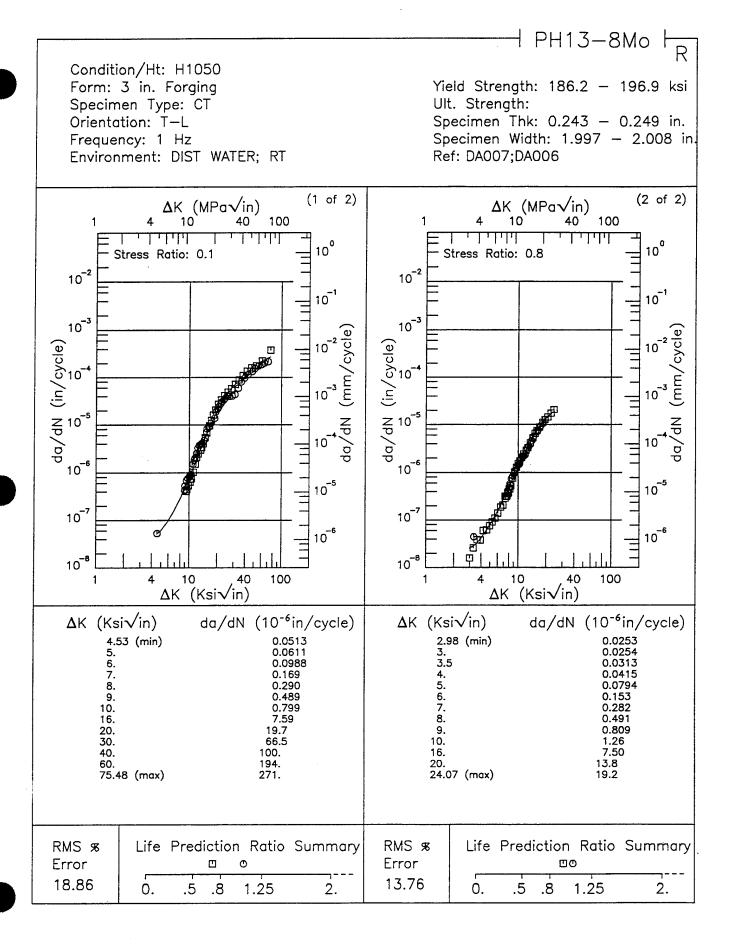


Figure 4.17.3.1.38

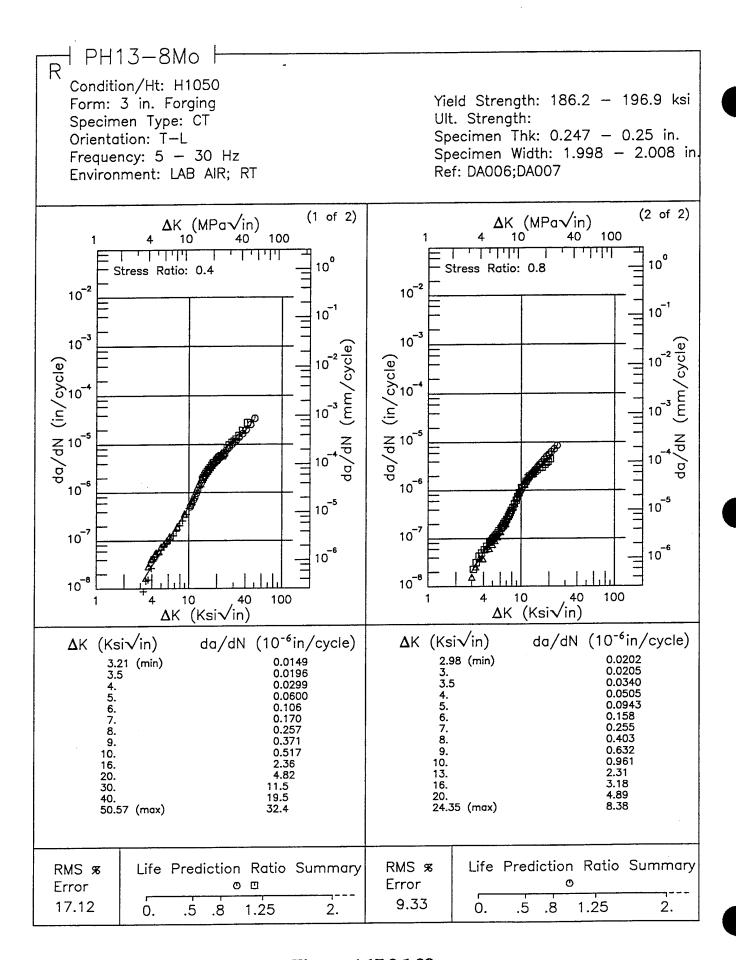


Figure 4.17.3.1.39

Condition/Ht: H1050 Form: 3 in. Forging Yield Strength: 186.2 - 196.9 ksi Specimen Type: CT Ult. Strength: Orientation: T-L Specimen Thk: 0.243 - 0.25 in. Stress Ratio: 0.1 Specimen Width: 1.996 - 2.008 in Ref: DA006; DA007 Frequency: 1 - 20 Hz (1 of 2)(2 of 2) Δ K (MPa \sqrt{in}) Δ K (MPa \sqrt{in}) 10 100 10 100 40 40 1111 1 1 1 1 1 1 1 1 11111 10° 10° Environment: LAB AIR; R.T. Environment: DIST WATER; R.T 10-2 10-2 10-1 10-1 10⁻³ 10⁻³ 10-2 da/dN (in/cycle) da/dN (in/cycle) 10 10-6 10⁻⁶ 10 -5 10⁻⁵ 10⁻⁷ 10⁻⁷ 10 6 10⁻⁶ 10 8 10⁻⁸ 40 10 40 100 10 100 ΔK (Ksi√in) ΔK (Ksi√in) da/dN ($10^{-6}in/cycle$) da/dN (10⁻⁶in/cycle) **Δ**K (Ksi√in) ΔK (Ksi√in) 4.53 (min) 5. 6. 7. 8. 4.29 (min) 5. 6. 0.0513 0.0611 0.0246 0.0353 0.0988 0.0585 7. 8. 0.0938 0.169 9. 10. 10. 0.799 16. 16. 20. 20. 19.7 30. 66.5 100. 60. 194. 75.48 (max) 84.45 (max) Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error 18.05 18.86 Ō. .5 1.25 0. .5 .8 1.25 2. .8 2.

1 PH13−8Mo | F

Figure 4.17.3.1.40

PH13-8Mo Condition/Ht: H1050 Yield Strength: 196.5 ksi Form: 3 in. Forging Specimen Type: CCP (max load specified) Ult. Strength: Specimen Thk: 0.196 in. Orientation: L-T Specimen Width: 4.009 in. Frequency: 5 Hz Ref: DA006 Environment: LAB AIR; RT (1 of 1) ΔK (MPa√in) Δ K (MPa \sqrt{in}) 100 10 40 100 10° 10° Stress Ratio: -1. 10-2 10 -2 10-1 10 10⁻³ 10 -3 da/dN (in/cycle) da/dN (in/cycle) 10 10⁻⁶ 10⁻⁶ 10 -5 10⁻⁵ 10⁻⁷ 10⁻⁷ 10 -6 10 -6 10⁻⁸ 40 100 10 40 100 10 ΔK (Ksi√in) ΔK (Ksi√in) Δ K (Ksi \sqrt{in}) $da/dN (10^{-6}in/cycle)$ da/dN (10⁻⁶in/cycle) ΔK (Ksi√in) 0.0676 0.0796 5.37 (min) 6. 7. 8. 9. 0.110 13. 16. 20. 25. 30. 14.6 26.6 53.32 (max) 35.6 Life Prediction Ratio Summary RMS % Life Prediction Ratio Summary RMS % Error Error .5 1.25 2. 9.70 .8 Ò. 1.25 2. 0. .5 .8

Figure 4.17.3.1.41

TABLE 4.17.3.3

K_{Isco} SUMMARY FOR STAINLESS STEEL PH13-8MO

	Refer	84333	R1006	RI006	RI006	R1006	RI006	RI006	R1006	RI006	RI006	RI006	86688	86688	86688	RI006	RI006	RI006	RI006
-																			
	Test Date	1971	1976	1976	1976	1976	1976	1976	1976	1976	1976	9261	1973	1973	1973	1976	1976	1976	1976
	Test Time (min)	00009	83520	83580	51720	48780	51720	86280	83520	86280	48780	51720	1			116820	120840	120840	86280
	K _{Loo} (Ksi√in)	73.9	50	>48	>46	>49	>48	>40	46	>50	>48	>46	46	69	16	>53	55	>52	<54
	Ko (Ksi√in)	73.9	130	131	131	130	130	131	130	131	130	131	62.6	62.6	9'89	132	132	132	132
	Crack (in)		÷	1		i	:	ŀ	ì		:	ì	-1	1	-	ł	i	1	:
	Prod Thk (in)	‡	4	4	4	4	4	4	4	4	4	4	2.25	2.25	2.25	1.5	1.5	1.5	1.5
	Thick (in)	0.48		1	1	1	1	1		1	1	1	1	1	1	1	1	1	ī
Snecimen	Width (in)	1.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	63	2	2	5.5	5.5	5.5	5.5
Į Ū.	Design	CANT	DCB	DCB	DCB	DCB	DCB	DCB	DCB	DCB	DCB	DCB	ŧ	CT	ಕ	DCB	DCB	DCB	DCB
	Envir.	3.5% NaCl					W E S	S.L.W.					20% NaCl	Industrial Atm	Seacoast Atm		III E S	о.т.w.	
	Yield Str (Ksi)	207.5					700	¥07						196.7			5	417	
	Spec Or.	T-T					E	5						T-T			E	;	
	rest Temp (°F)	R.T.					£ Q	i i						R.T.			Ē	1.1.	
	Prod Form	F					Q	Q 4						В			ß	4	
	Condition/ Heat Treat							TOEO	00611								111000	000111	

(2 of 4)

TABLE 4.17.3.3 (CONTINUED)

Kisce SUMMARY FOR STAINLESS STEEL PH13-8MO

Condition/	Dund	Test		Yield		0 2	Specimen		Prod				T. 420.T.		
Heat Treat		Temp (°F)	Or.	Str (Ksi)	Envir.	Design	Width (in)	Thick (in)	Thk (in)	Crack (in)	Kai√in)	K _{lace} (Ksi√in)	Time (min)	Test Date	Refer
			L-T	214	S.T.W.	DCB	5.5	1	1.5	;	132	<53	116820	1976	RI006
	臼	R.T.				DCB	5.5	1	1.5	1	781	<53	116820	1976	RIOOG
	(cont'd)	(cont'd)	T.L	213	S,T,W.	DCB	5.5	-	1.5		781	>53	116820	1976	Rioos
						DCB	5.5	1	1.5	1	132	×54	116820	1976	RIOOG
				201	M E &	DCB	5.5	1	4	-	127	>80	83520	1976	R1006
						DCB	5.5	1	4		127	>74	51720	1976	RI006
			T-T		9 K# NT-CH	WOL	2549	966'0	1	1.11	ŧ	94.8	60420	1978	GD009
				215		WOL	2.548	9660	1	1.25	ŧ	82.3	60420	1978	GD009
H1000					S.T.W.	WOL	2.544	966.0	1	1.21	ł	88.1	60420	1978	GD009
(cont'd)						DCB	5.5	1	7		125	571	61720	1976	Riod
	яВ	T.				DCB	5.5	1	4	1	125	>49	83520	1976	Rioos
				198	STW	DCB	99	-	4	1	125	49	83520	1976	Rioos
						DCB	20	-	¥	1	125	>46	83520	9261	RIOGE
			T-L			DCB	5.5	-	4	1	125	89≪	51720	1976	RIOG
					3.5% NaCl	MOL	2.545	0.998	1	1.88	***	63.2	60420	1978	GD009
				916	O.S./O MAOI	MOL	2.547	0.999	1	1.25		85.5	60420	1978	GD009
					MER	MOL	2.549	666.0	-	1.05		9.66	60420	1978	GD009
						WOL	2.544	0.999	1	1.05	•••	5.66	60420	1978	GD009

TABLE 4.17.3.3 (CONTINUED)

K_{lscc} SUMMARY FOR STAINLESS STEEL PH13-8MO

		_					_	_		00000000	00002000	000000000		Юпропрост		XXXXXX	XXXXXXXX		
	Refer	R1006	RIOGE	RIOOG	RI006	RI006	R1006	R1006	R1006	Rioos	Rioos	Rioos	86688	86688	86688	RIOG	Riode	R1006	RI006
	Test Date	1976	1976	1976	1976	1976	1976	1976	1976	1976	1976	1976	1973	1973	1973	1976	1976	1976	1976
Test	Time (min)	75180	75240	60180	116820	116820	116820	86280	116820	116820	116820	86280	:		i	120980	120960	120960	120960
	K _{lace} (Ksi√in)	>75	>70	>87	>73	70	>73	>73	>63	>63	263	>63	65	83	44	>56	>54	>50	>51
ì	Ko (Ksi√in)	132	132	182	132	132	132	132	133	133	133	133	87.8	87.8	87.8	97	97	86	86
,	Crack (in)	•••	ı		ì					-	-		ì	-	***	-		•	-
Prod	Thk (in)	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	91	1.5	1.5	2.25	2.25	2.25	9'1	97	1.5	1.5
	Thick (in)	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
Specimen	Width (in)	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	2	2	2	5.5	5.5	5.5	5.5
S	Design	DCB	DCB	DCB	DCB	DCB	DCB	DCB	DCB	DCB	DCB	DCB	CT	CT	\mathbf{CT}	CI	CT	CT	CT
	Envir.	F.C.S.	200	a Ca		E	S.I.w.				S. T.		20% NaCl	Industrial Atm	Seacoast Atm	222.00	B. I. W.	i i	S.T.W.
II	Str (Ksi)				208					Š	210			178.5		į	217	5	219
	Spec Or.				L-T					E	7-1			T-T				ار ت	
Test	Temp (°F)						R.T.							R.T.			£	ж. т.	
r £	Form						RB							В			ţ	BK	
7	Condition/ Heat Treat						H1000 (cont'd)							H1050			010110	KHS90	

TABLE 4.17.3.3 (CONCLUDED)

Kisce SUMMARY FOR STAINLESS STEEL PH13-8MO

7-0345-0	r d	Test	2	Yield		S	Specimen		Prod			ì	Test		
Condition From Heat Treat Form		Temp (°F)	Spec Or.		Envir.	Design	Width (in)	Thick (in)	Thk (in)	Crack (in)	Ro (Ksi√in)	K _{leo} (Ksivin)	Time (min)	Test Date	Refer
				010	TI WWW	L)	5.5	1	1,5		97	>67	120960	1976	RIOGE
RH975	BR	R.T.	L-S	210	3 i.m.	Ð	5.5	1	1.5		- 20	29<	120960	1976	RIOG
				219	S.T.W.	\mathbf{cr}	5.5	1	1.5	•••	86	>58	120960	1976	RI006
				, a		CJ	5.5	1	1.5		96	>92	120960	1976	RIOOG
RH1000	BR	R.T.	r-S	215	3.4.W.	CT	5.5	1	1.5	**	96	101	120960	1976	Ricos
		مانون. مانون		218	S.T.W.	CT	5.5	1	1.5	1	26	>85	120960	1976	R1006
TYS=140Ksi	Ъ	R.T.	T-T	140	3.5% NaCl	CANT.	***	1	1		180	170.	•••	1972	83613
TYS=180Ksi	Ь	R.T.	T-L	180	3.5% NaCl	CANT.	:	1	-1	:	190	160⁺	***	1972	83613
TYS=190Ksi	P	R.T.	T-T	190	3.5% NaCl	CANT		1	1		180	130*		1972	83613
TYS=200Ksi	Ъ	R.T.	T-L	200	3.5% NaCl	CANT.	i	-	1	:	190	155+	-	1972	83613
TYS=210Ksi	P	R.T.	T-T	210	3.5% NaCl	CANT.		1	1	-	135	120		1972	83613

 $^{+}$ specimen thickness does not meet minimum requirements of $2.5~\left(rac{K_{Loc}}{\sigma_{_{\mathcal{P}}}}
ight)$

^{*} asterisk in specimen design column indicates that specimens are side-grooved

TABLE 4.18.2.2

						Sc	TAINE	ESS	STAINLESS STEEL		PH14-8Mo	Кc							
	PROI	PRODUCT	Į.		1	SPECIMEN	MEN	CRACK	CRACK	GROSS	88		Kapp			Кc			
CONDITION HEAT TREAT	FORM	THICK (in.)	TEMP (°F)	SPEC	STR (Kel)	WIDTH (in.) W	THICK (in.) B	INIT (in.) %a.	FINAL (in.) Sa,	ONSET (Kei) 0.	MAX (Kei)	K (Ketvin)	K.	STAN	K. (Kaivin)	K, MBAN	STAN DEV	DATE	REFER
							BUCH	TING O	P CRACK	BUCKLING OF CHACK KINGES HESTHAINED	STRAIN	e							
		0.03	63	I.T	174.5	24.040	0.025	2.990	ı	1	72.60	231.63		ı	ı	1	!	1964	67673
		0.03			174.5	7.990	0.025	2.010	!	!	118.10	218.44*	ı	ı		ï		1964	57573
		0.03			174.6	24.020	0.025	3.000	:	ı	96.90	210.21			1	ï		1964	67673
SRH1060	SHEET	0.03	E D	E +	174.6	24.030	0.025	9.000	:	ı	72.40	231.22	223.7	11.7	1	1	•••	1964	67573
		0.03			174.5	24.040	0.025	9.000	i	;	71.90	229.61				ı	ì	1964	67573
		90.0			196.6	24.010	0900	9.000	i	ı	92.10	294.15	ı	::	1	ı		1964	67929
		60.0			197.4	24.100	0.093	6.000	ï		115.70	369.42	1	ł	ı	i	i	1964	57573

* NOTE: NET SECTION STRESS EXCREDS 80% OF YIELD STRENGTH. VALUE NOT INCLUDED IN MEAN OR STANDARD DEVIATION.

TABLE 4.19.1.1

MEAN PLANE STRAIN FRACTURE TOUGHNESS FOR STAINLESS STEEL ALLOY PH15-7Mo AT ROOM TEMPERATURE

Product Condition/Heat Treatment Specimen Orientation Rolled Bar RH1950 40.2 1.5 30.6 0.1 2						K_{Ic}	$K_{lc}~(ksi\sqrt{in})$	<u>1</u>			
Mean KH950 Std hosy n hosy hosy Std hosy n hosy hosy n hosy hosy n hosy hosy std hosy n hosy hosy RH1050 40.2 1.5 3	Product Form				01	pecime	n Orier	ıtation			
Mean Std n Mean Std n Mean Std n KI _c Dev n KI _c Dev n KI _c Dev n KI _c Dev n RI Dev n <th></th> <th></th> <th></th> <th>L-T</th> <th></th> <th></th> <th>T-L</th> <th></th> <th></th> <th>\mathbf{S}-\mathbf{F}</th> <th></th>				L-T			T-L			\mathbf{S} - \mathbf{F}	
RH1050 30.6 0.1 2 RH1050 40.2 1.5 3			Mean K _{Ie}	Std Dev	đ	Mean K _{Ic}	Std Dev	и	Mean K _{le}	Std Dev	u
RH1050 40.2 1.5 3		RH950	:		•	30.6	0.1	2	i	1	;
	Kolled Bar	RH1050	:		i	40.2	1.5	အ	i	1	:

				ST	AINLES	STAINLESS STEEL	H	PH15-7MO	K _I						
	PRODUCT	ucr					SPECIMEN	z	CRACK			K			
CONDITION	PORM	THICK (in.)	TEST TEMP (°F)	SPEC	YIBLD STR (Ket)	WIDTH (a)	THICK (in.) B	DESIGN	LENGTH (In.)	(Kr. TYS)* (in.)	K (Rei •	K. MBAN	STAN	DATE	REFER
Se na	Dellad Des	1.26	E	Ė	204.0	2.000	1.000	CT	1.025	90:0	30.50			1973	86688
OGE IN	Molled Dar	1.25	į	1:	204.0	2.000	1.000	CT	1.007	90:0	30.70	30.6	0.1	1973	86688
		1.26			195.0	2.000	1.000	CT.	1.006	0.11	41.30			1973	86688
RH1050	Rolled Bar	1.26	R.T.	Ţ.	195.0	2.000	1.000	cr	1.010	0.11	40.70	40.2	7	1973	86688
		1.25			195.0	2.000	1.000	CT	1.019	01.0	38.50			1973	86688

K_{Isco} SUMMARY FOR STAINLESS STEEL PH15-7MO

/	P	Test	7	Yield		S	Specimen		Prod	7	1		Test		
Condition/ Heat Treat	Form	Temp (°F)	opec Or.	Or. (Ksi)	Envir.	Design	Width T (in)	Thick (in)	Thk (in)	(in)	Crack no (in) (Ksivin)	R _{loc} (Ksi√in)	Time (min)	rest Date	Reference
RH950	В	B R.T.	-	196.5 3.5	% NaC	I CANT	1.5	0.48	1.75		31.5	14	30000	1971	84333
TH1050	В	B R.T.	;	167.8	167.8 3.5% NaCl CANT	CANT	1.5	1.5 0.48 1.75	1.75		33.6	18.5	60000 1971	1971	84333

TABLE 4.20

REFERENCES FOR THE STAINLESS STEEL DATA

74720

AFC 77

Kr.; Kree

Webster, D., "The Use of Deformation Voids to Refine the Austenitic Grain Size and Improve the Mechanical Properties of AFC 77," Research Report D6-23870, The Boeing Co., Renton, WA., ARPA Contract N00014-66-C-0365, February 1969.

76136

AFC 77

Kic; Kisce

Webster, D., "The Stress Corrosion Resistance and Fatigue Crack Growth Rate of a High Strength Martensitic Stainless Steel, AFC 77, "Research Report D6-23973, The Boeing Co., Renton, WA., ARPA Contract N00014-66-C-0365, June 1969.

77934

CUSTOM 455

K_{Ic}; K_{Isco}

Uchida, J. M., "Evaluation of Carpenter Custom 455," Research Report D6-23928, The Boeing Co., Renton, WA., November 18, 1969.

80685

AFC 260

Kisco

Webster, D., "Optimization of Strength and Toughness in Two High Strength Stainless Steels," Metallurgical Transactions, 2, (7), pp. 1857-1862, July 1971.

83613

PH13-8Mo

Kisce

Sandoz, G., "The Resistance of Some High Strength Steels to Slow Crack Growth in Salt Water," NRL Memorandum Report 2454, Naval Research Laboratory, Washington, D.C., February 1972.

84212

15-5PH

 K_{Ic}

17-4PH

 K_{Ic}

Takacs, E. G., "Fracture Toughness Tests, Data on Armco 17-4PH and 15-5 PH Alloys," letter to J.E. Campbell, Battelle Columbus, October 18, 1972.

84302

AFC 77

 K_{te}

Webster, D., "Increasing the Toughness of Martensitic Stainless Steel AFC 77 By Control of Retained Austenite Content, Ausforming and Strain Aging," Transactions of the ASM, 61, (4) pp. 816-838, December 1968.

REFERENCES FOR THE STAINLESS STEEL DATA

84306	PH13-8Mo	K_{ic}
		1 Fracture Mechanics Data for Air Force Handbook Usage," North American Rockwell, Los Angeles Division, Los Angeles, CA.,
84333	15-5PH(AM) 15-5PH(VM) 17-4PH 17-7PH AM 355 AM 362 AM 364 CUSTOM 455 PH13-8Mo PH15-7Mo Carter, C. S., Farwick of High Strength Pre pp. 190-197, May 197	K _{Iscc} K _{Iscc}
84365	PH13-8Mo	K_{ic}
	Takacs, E. G., "Plane Armco Steel Corporat	Strain Fracture Toughness - PH 13-8 Mo," Tabulated Data from tion, Advanced Materials Division, Baltimore, Md., July 11, 1972.
85034	PH13-8Mo	$\mathbf{K}_{\mathtt{ic}}$
	Mitchell, John, "Labo Cawthorne of Februa	ratory Reports on Fracture Toughness Tests," per memo from Edary 5, 1973; data sheets from Schultz Steel Co., South Gate, CA.
85544	AFC 77	da/dt
	Speidel, M. O., "Dyna preprint from L' Hydr France (no date).	mic and Static Embrittlement of a High Strength Steel in Water," rogen Dans Les Metaux, 1, Editions Science et Industries, Paris,
85836	РН13-8Мо	K_{ic}
	"B-1 Fracture Tought Corp., Los Angeles, C	ness Data (K_{Ic}) - Rockwell International", Rockwell International CA., April 24, 1973.

REFERENCES FOR THE STAINLESS STEEL DATA

85837

PH13-8Mo

a-vs-N; da/dN

"Fracture Toughness Data Collection, Rockwell International Corporation, from B-1 Program," Rockwell International Corporation, Los Angeles, CA., April 1973.

85857

PH13-8Mo

 K_{ic}

Shultz Steel Company - Fracture Toughness Data - May 10, 1973, per memo from Ed Cawthorne of May 10, 1973.

86688

15-5PH

 $\begin{array}{c} K_{\rm Ic};\; K_{\rm Iscc} \\ K_{\rm Ic};\; K_{\rm Iscc} \end{array}$

17-7PH

AM 355

K_{Isce} K_{Ic}; K_{Isce} K_{Ic}

PH13-8Mo PH15-7Mo

Sprowls, D. O., et al., "Evaluation of Stress Corrosion Cracking Susceptibility Using Fracture Mechanics Techniques," Final Report Part I, Aluminum Co. of America, Alcoa Technical Center, Alcoa, Pa., Contract NASA-21487, May 31, 1973.

87360

AFC 77

 $\begin{matrix} K_{Isce} \\ K_{Ic} \end{matrix}$

AFC 77 (VAR)

Caton, R. G., and Carter, C. S., "Evaluation of AFC 77 Martensitic Stainless Steel for Airframe Structural Applications," Report AFML-TR-73-182, Boeing Commercial Airplane Co., Seattle, WA., Contract F33615-71-C-1550, September 1973.

88136

PH13-8Mo

K_{1c}; a-vs-N; da/dN

Dill, H. D., "Evaluation of Steel Alloys 300M, HP-9Ni-4Co-20, HP-9Ni-4Co-30, and PH 13-8Mo", Report MDC-A2639, McDonnell Aircraft Company, McDonnell Douglas Corporation, St. Louis, MO, December 21, 1973, with data supplements received May 2, 1974.

88579

PH13-8Mo

a-vs-N; da/dN

"B-1 Program da/dN Data for Aluminum Alloys," Rockwell International Corporation, Memorandum to H. D. Moran from E. W. Cawthorne, Battelle Columbus Laboratories, April 3, 1974.

REFERENCES FOR THE STAINLESS STEEL DATA

90011

PH13-8Mo

K_{ic}

"Rockwell International, B-1 Program Fracture Toughness Data of August 5, 1974," with memorandum from E. W. Cawthorne to H. D. Moran of Battelle Columbus Laboratories, August 5, 1974.

92270

15-5PH

a-vs-N; da/dN

Rice, R. L., "Fracture Toughness and Fatigue Crack Propagation in 15-5 PH Stainless Steel Bar," memorandum to J. E. Campbell, Battelle Columbus Laboratories, Columbus, Ohio, January 31, 1975.

AM001

347

da/dN

"Fatigue Crack Propagation in a 347 Stainless Steel Weld," Prepared for Airesearch Manufacturing Co., by Del West Associates, Inc., July 29, 1975.

BW004

15-5PH

da/dN

Watson, K. R., "Pylon Durability and Damage Tolerance Analysis," The Boeing Co., Wichita, KA., Contract No. F33657-78-C-0108-PZ0036, Document No. D361-400 41-2, September 1980.

BW005

15-5PH

da/dN

Watson, K. R., "Weapons Bay Durability and Damage Tolerance Analysis," The Boeing Co., Wichita, KA., Contract No. F33657-78-C-0108-PZ0036, Document No. D361-40041-1, September 1980.

BW007

15-5PH

K_{Ic}

Hananel, A., Watson, K., Knoff, K., and Sherrich, G., "Fracture Mechanics Testing of B-52/CMI Materials," Final Test Report, The Boeing Co., Wichita, KA., Contract No. F33657-78-C00108-PZ0036, Document No. D361-11197-1, December 1978.

DA001

17-4PH

K_{Ic}; a-vs-N; da/dN

17-7PH

a-vs-N; da/dN

Fatigue Crack Growth Rate Data Sheets on Aluminum Alloys 2024, 7010, 7050, 7075 and 7475, Stainless Steel Alloys 17-4PH and 17-7PH, and Alloy Steels 4340, A286, H-11, HY-180 and 12-9-2, Sent from Mr. Paul Abelkis, Douglas Aircraft Company, McDonnell Douglas Corporation, Long Beach, CA, March 1982.

REFERENCES FOR THE STAINLESS STEEL DATA

GD009

PH13-8Mo

K_{Ic}; a-vs-N; da/dN; K_{Isce}

Margolis, W. S., "F-16 Material Allowables Evaluation of PH 13-8Mo Steel Alloy, H1000 Temper," General Dynamics, Fort Worth Division, Report No. 16PR1084, October 1978.

GD010

17-4PH

a-vs-N; da/dN

Margolis, W. S., "Constant Amplitude Fatigue Crack Growth Rate of 17-4 PH Steel Alloy Casting, H1025, Repair Welded and Stress Relieved at 90F," General Dynamics, Fort Worth Division, Report No. 16PR1195, May 1979.

HD007

304

a-vs-N; da/dN

James, L. A., Schwenk, E. B., "Fatigue-Crack Propagation Behavior of Type 304 Stainless Steel at Elevated Temperatures," Metallurgical Transactions, Vol. 2, pp. 491-496, (1971).

HD008

304

a-vs-N; da/dN

James, L. A., "Effect of Thermal Aging Upon the Fatigue-Crack Propagation of Austenitic Stainless Steels," Metallurgical Transactions, Vol. 5, pp. 831-838, (1974).

HD009

304

a-vs-N; da/dN

James, L. A., Staalsund, J. L., Bauer, R. E., "Optimization of Fatigue Crack Growth Testing for First Wall Materials Development Evaluations," Journal of Nuclear Materials, Vol. 85-86, Part B, pp. 851-854, (1979).

HD010

304

a-vs-N; da/dN

James, L. A., "Specimen Size Considerations in Fatigue Crack Growth Rate Testing in Fatigue Crack Growth Measurement in Data Analysis," STD-738, pp. 45-47, ASTM, (1981).

HD011

304

a-vs-N; da/dN

James, L. A., "Frequency Effects in the Elevated Temperature Crack Behavior of Austenitic Stainless Steels-A Design Approach," Journal of Pressure Vessel Technology, Vol. 101, pp. 171-176, (1979).

TABLE 4.20 (CONCLUDED)

REFERENCES FOR THE STAINLESS STEEL DATA

HD012

304

a-vs-N; da/dN

316

a-vs-N; da/dN

James, L. A., "Some Observations Regarding Specimen Size Criteria for Fatigue-Crack Growth Rate Testing," Report HEDL-TME 77-87, Westinghouse Hanford Co., Richland, WA., August 1977.

HD013

316

a-vs-N; da/dN

James, L. A, "The Effect of Elevated Temperature Upon the Fatigue-Crack Propagation Behavior of Two Austenitic Stainless Steels," Mechanical Properties of Materials, Vol. III, pp. 341-352, Society of Materials Science, Japan, 1972.

HD014

316

a-vs-N; da/dN

James, L. A., "A Survey of the Effect of Heat-to-Heat Variations Upon the Fatigue-Crack Propagation Behavior of Types 304 and 316 Stainless Steels," Report HEDL-TME 75-37, Westinghouse Hanford Co., Richland, WA., May 1975.

NC001

PH13-8Mo

 K_{lc}

"Plane Strain Fracture Toughness Data Sets on Aluminum, Steel, and Titanium Alloys", Data sent from P. G. Porter of Northrop Corp., Hawthorne, CA, March 1, 1982.

NC002

PH13-8Mo

a-vs-N; da/dN

Fatigue Crack Growth Rate Data on Aluminum, Steel, and Titanium Alloys, Data sent from P. G. Porter of Northrop Corp., Hawthorne, CA, March 1, 1982.

RI004

CUSTOM 455

a-vs-N; da/dN

Mines, R. G., "Fracture Mechanics Evaluation of Custom 455 Stainless Steel," Rockwell International, Shuttle Orbiter Division, Laboratory Test Report No. 2761-41-33, May 1980.

RI006

PH13-8Mo

 K_{Iscc}

Ferguson, R. R., Berryman, R. C., "Fracture Mechanics Evaluation of B-1 Materials", Rockwell International, B-1 Division, Los Angeles, CA, Contract No. F33657-70-C-0800, Report No. AFML-TR-76-137, October 1976.